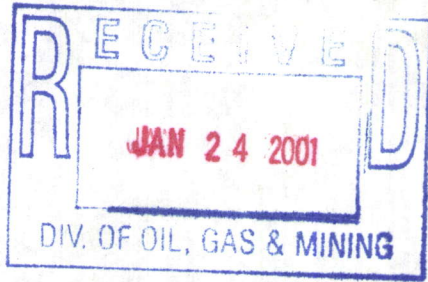


m/045/022



## MagCorp (Knolls Facility) Bond Calculation

January 22, 2001 (11:54am)

## Table of Contents

Table 1, Total Length of Ditches (feet)

Table 2, Total Cubic Yards of material in Ditches

Table 3, Reclamation Costs for Ditches

Table 4, Total Length of Dikes (feet)

Table 5, Total Cubic Yards of material in Exterior Dikes

Table 6, Reclamation Costs for Exterior Dikes

Table 7, Total Length of Interior Dikes

Table 8, Total Cubic Yards of Interior Dikes

Table 9, Interior Dike Reclamation Costs

Table 10, Road Reclamation

Table 11, Facility Removal

Table 12, BLM Contracted Oversight Costs

Table 13, Total Reclamation Costs



## MagCorp (Knolls Facility) Reclamation Bonding Requirements

### SUMMARY:

It has been determined by the State Office Minerals Staff that it is necessary for a bond to be placed by MagCorp. This bond is to insure reclamation of disturbed areas within their Right of Way for a Magnesium processing facility at Knolls Utah. ***Stipulation 17 states. "Prior to abandonment of the grant, the holder shall contact the Authorized Officer to arrange a joint inspection of the grant area. The inspection will be held to agree on an acceptable abandonment and rehabilitation plan. The Authorized Officer must approve the plan in writing prior to the holder commencing any abandonment and rehabilitation activities."*** The reclamation requirements are that ditches will be backfilled, baffle walls will be pushed into adjacent borrows and dikes are reclaimed by flattening them out and contouring. A cost estimate for reclamation has been performed by the Minerals Staff and resulted in the following.

### INTRODUCTION:

The MagCorp (Knolls Facility) operation is located in the western portion of Tooele County, Utah, approximately 30 miles east of the community of Wendover Utah. This area is extremely flat with a nominal elevation of 4,212 feet above sea level. The production of Magnesium Chloride brines are derived from the solar evaporation. The operation consists of four basic steps:

1. Brine collection
2. Concentration of brine through evaporation
3. Precipitation of sodium and potassium
4. Concentration of the Mag Chloride brine.

In order to perform these basic steps MagCorp collects mineral laden brines through a collection system. Please see Appendix 17 for photographs of the operation. The collection system consists of approximately 6 miles of a main collection ditch and approximately 11.7 miles of a collection ditch interior to Pond 0. The P1 pump station can pull brines either from the main collection ditch (6 miles) or from the main collection ditch and the interior Pond 0 (11.7 miles) ditch via a gate system at Pond 0. The brines are pumped through the P1 pump station which delivers about 50,000 gallons per minute. The brine from this pump can be diverted through a system of gates to either Pond 0 or Pond 1. Once in Pond 1, the brine is sent through a transfer ditch of about 3 miles which then flow into the P2 feed ditch. Once the brine reaches the P2 feed ditch they can be pumped from the P2 pump into the P7 ditch. The P7 ditch diverts the brine into Pond 7A. From Pond 7A the brine can be diverted into Pond 5 or Pond 7B. If the brine is diverted into Pond 5, they can be moved back into Pond 7B. From Pond 7B the brine is diverted to Pond's 7C and 7D. In Pond 7D the brine is essentially magnesium chloride brine. The brine can then be pumped from the 7D pump into one of two finished brine storage ponds. These ponds have pumps to move brines from one pond to another pond and to a sump. Once the brine is in the sump they are then sent to the Rowley facility via a pipe line for further processing.

The reclamation of the Knolls facility consists of the following:

1. Ditches and berms from ditches.
2. Exterior Dikes of the pond structures
3. Interior Dikes of the pond structures (including finish brine storage ponds)
4. Reclamation and removal of facilities



5. Reclamation of roads
6. Reestablishment of survey monuments

### **DITCH RECLAMATION**

The ditches will be required to be filled in. This will alleviate any physical safety hazards for the public due to the berms and ground water remaining in the ditch. This will help to return the area back to a flat vista.

**Ditch(es) Earthwork:** Main Collection Ditch, Pond1 Bypass Ditch and P2 Feed Ditch.

The total length of ditches and baffles were approximated from the map at Appendix 1. The resulting lengths are as listed in Table 1.

**TABLE 1.**

<b>Total Length of Ditches (feet)</b>	
Facility Type	
Pond 1 Bypass Ditch	18,480*
Main Intake Ditch	31,000
No 2 Pump Feed Ditch	12,000
Pond 1 - Pond 2 and Pond 0 - Pond 2	1,500
Grand Total	62,980

\*1990 Annual report states the ditch was dug 3.5 miles long. 3.5 miles \* 5280 feet per mile = 18,480 feet.

The volume of the main collection ditch and P2 Feed Ditch was estimated by using the Dames & Moore "New Solar Pond Facilities located on West Desert for AMAX Magnesium, Inc., dated December 8, 1986" (Appendix 2). The volume of the material was taken and divided by the length of the ditch. In the case of the Main Intake ditch the estimated quantity of 550,000 yd<sup>3</sup> was divided by the length of 7.12 miles to determine the average cross sectional area. This was done because the ditch lengths were changed from the design in the Dames & Moore report versus the "As built" configuration.

$$A = (V * 27) / L$$

A = Area of the Ditch (ft<sup>2</sup>)

V = Volume of the Ditch (sq feet) \* 27 ft<sup>2</sup> per yd<sup>3</sup>

L = Length of Ditch (miles) \* 5280 feet per mile

A = Area of the Main Intake Ditch

V = 550,000 yd<sup>3</sup> (Appendix 2)

L = 7.12 Miles (Appendix 2)

$$A = (550,000 \text{ yd}^3 * 27 \text{ ft}^3 \text{ per yd}^3) / 7.12 \text{ miles} * 5280 \text{ feet per mile}$$

**Area of the Main Intake Ditch is = 395 ft<sup>2</sup>**

### No 2 Pump Feed Ditch

A = Area of the Main Intake Ditch

V = 38,000 yd<sup>3</sup> (Appendix 2)

L = 1.53 Miles (Appendix 2)

$$A = (38,000 \text{ yd}^3 * 27 \text{ ft}^3 \text{ per yd}^3) / 1.55 \text{ miles} * 5280 \text{ feet per mile}$$

**Area of the Main Intake Ditch is = 125 ft<sup>2</sup>** (see Table 5 for the 40,000 yds cast up material)

The Pond 1 Bypass ditch was taken from the 1990 Annual Report of Mining Operations for Knolls Solar Ponds (See Appendix 2)

The Pond 2 - Pond 0 was estimated

1. Main Collection ditch = 395 sq. ft.
2. No. 2 Pump Feed ditch = 125 sq. ft. ditch only (38,000 yd<sup>3</sup>)
3. Pond 1 Bypass ditch = 240 sq. ft.
4. Pond 2 - Pond 0 By ditch = 150sq. ft. (Estimate)

Once this calculation is carried out, the resulting figure is the cubic feet of material that must be relocated. This figure was then converted into cubic yards using the following equation:

$$\text{ft}^3 / 27 = \text{yd}^3$$

where:

yd<sup>3</sup> = Cubic Yards of material

ft<sup>3</sup> = Cubic feet of material

The cubic yardage of material to be moved is summarized in Table 2.

The length of each ditch was then multiplied by their average cross sectional area to determine the volume.

**TABLE 2.**

<b>Cubic Yards of material to be removed for Ditches (yd<sup>3</sup>)</b>			
<b>Facility Type</b>	<b>Area (ft<sup>2</sup>)</b>	<b>Length (ft)</b>	<b>(yd)<sup>3</sup></b>
Main Collection*	395	31,400	459,370
No 2 Pump Feed Ditch	125	12,000	55,556
Pond 1 Bypass ditch**	240	18,480	164,267
Pond 1 - Pond 2 and Pond 0 - Pond 2	150	1,500	8,333
Grand Total		63,380	687,526
Numbers may not add because of rounding			

\* Back Calculated from the Dames & Moore report on the New Solar Pond Facilities, 1986

\*\* MagCorp 1990 Annual Report to the Division of Oil Gas and Mining

Pond 1 ditch was not figured here but was figured in the with the dike calculations



**Ditch Reclamation Plan:**

A detailed equipment survey was not conducted on filling the ditches. In lieu of this approach BLM relied on the Preliminary Cost Estimate West Desert Solar Ponds for AMAX Magnesium, Inc., Appendix C construction cost estimate. This is found in the Dames & Moore Geotechnical and Construction Cost Studies for the New Solar Pond Facilities located on the West Desert for AMAX Magnesium, Inc. dated 1986, which the pertinent portions can be viewed in Appendix 2 of this document. All of the excavator or track hoe work was costed at \$1.50 per yard except for the P1 ditch which was costed at \$2.25 per yard. The P1 ditch had to have the material double handled and this is the reason why the cost was escalated. In the other ditches the material did not have to be double handled with two excavators.

The reclamation work on the P1 ditch will have to be handled by a large excavator due to the fact that the material cannot be doubled handled to fill the ditch back to its original level. The actual excavator that was used was a CAT 245 hoe. This machine will be able to accomplish the work in an efficient manner. The boom on the excavator will have to be approximately 50 feet long. It would be best if the ditches were pumped down and both sides were filled at the same time. This would require two excavators to work at the same time.

The costs were estimated using the \$1.50 as a base cost for the excavator work. From the \$1.50 per yard the costs will be adjusted for construction labor. This was an increase of 34% from 1986 to present.

The costs were reduced by a factor of 30% because this estimates the best cycle time of CAT 325B and CAT 330B which are similar to a CAT 245. The hoes can operate at an average of 12-13 seconds at the best cycle time versus 18-19 seconds on average cycle time. (See Appendix 3, Cost Reduction). This would be approximately a 30% increase in productivity. BLM applied a 10% contingency for items missed in the cost estimate based on the Means Estimating Guide. If BLM were to contract this out it would require an 18% administrative charge to be withheld. The following shows a breakdown of all the costs.

**Description of Costs:**

The following is a summary of all the costs included in the bond calculation:

**Operating Costs**

The base cost of \$1.50 per yd<sup>3</sup> is taken from the preliminary cost estimate from the preliminary design of the facility (Appendix C, Preliminary Cost Estimate, West Desert Solar Ponds, Dames & Moore New Solar Pond Facilities for AMAX Magnesium, Inc., Dec. 8, 1986.). The reference page of cost data can be viewed in Appendix 2. It is understood that this cost includes overhead and profit.

**Cost Reduction**

The cost reduction of 30% was derived from page 5-146 of the Caterpillar Performance Book. It was based on the fact that to place the material back into the ditch would be easier than excavating the material. The 30% was based on the fact that under average operating conditions the cycle time would be 23 seconds and under easy conditions the cycle time would be 16 seconds. This can be viewed in Appendix 3.

**Cost Index**

Western Mine Engineering, Mining Cost Service page CL-2 shows a cost index of Construction Labor at 12.48 in 1986 and in March 1999 the index was 16.77. This equates to 34% increase in Construction Labor. Equipment and Machinery increased by 37% over the same period of time. The

reference page of cost data can be viewed in Appendix 4.

### **Contingencies**

Means Facilities Construction cost Data recommends a 10% increase to the total cost for the contingencies. The reference page of cost data can be viewed in Appendix 5.

### **Administrative Costs**

The Washington Office guidance is to apply 18% overhead on all reimbursable (5XXX) projects. For the reference pages see Appendix 6.

**TABLE 3.**

<b>Summary of Costs for Reclamation of Ditches</b>			
<b>Type</b>	<b>Cost Cumulative (\$/yd)</b>	<b>Yds</b>	<b>Total Cost</b>
Operating	\$1.50	687,526	\$1,031,289
Reduced Costs for ease of job (-30%)	\$1.05	687,526	\$721,902
Cost Index from 1986 to 1999 Construction Labor Costs (34%)	\$1.41	687,526	\$967,349
Subtotal Direct costs			<b><u>\$967,349</u></b>
Contingency (10%)	\$1.55	687,526	\$1,064,084
Subtotal (all costs)			<b><u>\$1,064,084</u></b>
Administrative (18%)	\$1.83	687,526	\$1,255,619
<b>Total Cost (\$2000)</b> <small>Numbers may not add because of rounding</small>			<b><u>\$1,255,619</u></b>

Numbers are assumed to have overhead and profit included

### **EXTERIOR DIKES:**

The BLM has chosen as a minimum to grade all exterior dikes to a maximum of a 4 to 1 slope from the level of the existing pond out. This will get rid of physical hazards of steep slopes and areas where deep ponds would be and help return the area back to a more natural looking area.

#### **Exterior Dike Earthwork:**

The total length of ditches and baffles were approximated from the map at Appendix 1 and verified with the map dated 1994 submitted from the company to BLM. The resulting lengths are as listed in Table 4. The lengths for DWG.'s 1,2 and 4 were measured by vehicle mileage at 0.1 miles, 0.2 miles and 1.65 miles respectively.

**TABLE 4.**

<b>Total Length of Dikes (feet)</b>		
<b>Type</b>		<b>Dikes</b>
Entering Dunes	(DWG #1)	530
Between Dunes	(DWG #2)	1,060
Pond 5 North Dike	(DWG #3)	5,000
E. end Dunes	(DWG #4)	6,400
N. Dike Pond 0	(DWG #5)	21,000
W. Dike Pond 0	(DWG #6)	40,000
Pond 0 Sep.	(DWG #7)	2,500
Pond 1 W. Dike	(DWG #8)	7,500
Pond 1 S. Dike	(DWG #9)	13,700
Finished Brine North	(DWG #10)	4,900
Pond 7D,C & B S Dike	(DWG #11)	7,500
Pond 7D W Dike	(DWG #12)	13,500
Pond 7D N Dike	(DWG #13)	7,500
Pond 7D NE Dike	(DWG #13)	4,000
Pond 5 SW Dike	(DWG #16)	1,300
<b>Total</b>		<b>136,390</b>

The length of each dike was then multiplied by their average cross sectional area. These areas for the dikes were measured and the following area were derived based upon actual field calculations. The cross-sectional diagrams are in Appendix 7.

Once this calculation is carried out, the resulting figure is the cubic feet of material that must be relocated. This figure was then converted into cubic yards using the following equation:

$$\text{ft}^3/27 = \text{yd}^3$$

where:

$\text{yd}^3$  = Cubic Yards of material

$\text{ft}^3$  = Cubic feet of material

The cubic yardage of material to be moved is summarized in Table 5.



**TABLE 5.**

<b>Cubic yards of Exterior Dikes to be graded by a dozer (yd<sup>3</sup>)</b>			
<b>Type</b>	<b>Area (ft<sup>2</sup>)</b>	<b>Length (ft)</b>	<b>(yd<sup>3</sup>)</b>
Entering Dunes (DWG #1)	102	530	2,002
Between Dunes (DWG #2)	73	1,060	2,866
Pond 5 North Dike (DWG #3)	476	5,000	88,148
E. end Dunes (DWG #4)	265	6,400	62,815
N. Dike Pond 0 (DWG #5)	222	21,000	172,667
W. Dike Pond 0 (DWG #6)	240	40,000	355,556
Pond 0 Separation (DWG #7)	218	2,500	20,185
Pond 1 W. Dike (DWG #8)	327	7,500	90,833
Pond 1 S. Dike (DWG #9)	189	13,700	95,900
Finished Brine North (DWG #10)	220	4,900	39,926
Pond 7D,C & B S Dike (DWG #11)	929	7,500	258,056
Pond 7D,C & B W Dike (DWG #12)	348	13,500	174,000
Pond 7D N Dike (DWG #13)	175	7,500	48,611
Pond 7A & B NE Dike (DWG #13)	73	4,000	10,815
Pond 5 SW Dike (DWG #16)	333	1,300	16,033
P2 Cast up material*			40,000
<b>Grand Total</b> <small>Numbers may not add because of rounding</small>		136,390	1,478,413

\*See Appendix 2

#### **Equipment Selection (Exterior Dike):**

Equipment selection is limited by the load bearing capacity of the material surface. In a study performed by the Utah State Department of Highway in cooperation with the Bureau of Public Roads on the immediate surroundings, unconfined compression tests determined the load bearing capacity of the material to be 10 psi. The reference page from the report can be viewed in Appendix 19. John Condas at Gilbert & Western [the company that constructed the facility] was contacted by J. Kohler of this office on 9 November 1999 and he stated that they used 8 psi for equipment loading considerations. Referencing to Caterpillar's Performance Handbook (30th Anniversary Edition), it was determined that the D7R-LGP is the highest production dozer that could be used. This dozer has an applied stress of less than 7 psi on the material, which is a reasonable 3 psi less than the suggested limit. The D8, D9N, D10N and the D11N dozers all apply loads of 14.3 psi or higher which eliminates them from consideration. A D8LGP was reviewed and with a universal blade the dozer applied a load of 9.03 psi which is above the 8 psi used by Gilbert and Western in

the original construction. Contact was made with Wheeler Machinery (4901 West 2100 South, Salt Lake City, Utah, 801-908-8900) and they stated that they did not have a D8LGP in the rental fleet and that it was only available for purchase. For these two reasons the D8LGP was removed from consideration and a D7RLGP was chosen.

In this section the overall weight of the dozer and the ground contact area of the dozer shoe were given and can be viewed in Appendix 8 page 1-11 and 1-46. Using these two parameters, the load per square inch applied by the dozer on the material was calculated by using the relationship:

#### **D7R-LGP**

$$\sigma'_d = W_d / A_d$$

where:

$\sigma'_d$  = Stress applied by the dozer on the material (psi) 7.69

$W_d$  = Weight of the dozer plus the blade (lbs)

$A_d$  = Dozer shoe ground contact area (sq. in.)

$$\sigma'_d = 60,300 \text{ lbs.} + 8624 \text{ lbs.} / 8624 \text{ in}^2 = 7.69 \text{ psi}$$

#### **Production Rate of the Equipment:**

The production rate of the D7R LGP was calculated using the Caterpillar Performance Handbook, Bulldozer Section, page 1-52. Page 1-52 shows the graph of the production using a universal blade vs. dozing distance and page 1-55 is a step by step explanation on how to use the graph to estimate the actual production of the dozer, taking into account site specific factors. Both of these pages can be inspected in Appendix 9.

The average push is understood to be 213 feet derived from a weighted average of push distance and volumes based on drawings completed for the reclamation of the dikes (See Appendix 18)

The following is a direct accounting for each correction factor used in the production rate calculation.

#### **Correction Factors:**

1. Operator (**O**): Assuming that the operator will be average, the suggested correction factor is 0.75
2. Material (**M**): The material should be easy to cut but the ground is questionable. A correction factor is 0.8 has been applied
3. Job Efficiency (**E<sub>j</sub>**): The operator will be in charge of general maintenance of the dozer (lube, oil, filter). Taking this factor into account, along with startup time, breaks and miscellaneous delays, an efficiency of 50 min/hr is estimated. The suggested correction factor is 0.83
4. Material density (**D<sub>m</sub>**): The material to be moved can be characterized about half dirt and half rock. Generally, 50% rock and 50% dirt has a density of 2900 lbs/yd<sup>3</sup> which is found in Appendix 6. The suggested correction factor is 2700 lb./LCY/2900 lb./LCY for a factor of 0.93.
5. The uncorrected Hourly Production (**P<sub>u</sub>**): (graph in Appendix 5, Item E) = 380 LCY/Hr for a D7R series.

Using these correction factors, the actual production is calculated as follows:

$$\text{Production Rate} = (\text{O}) * (\text{M}) * (\text{E}_j) * (\text{D}_m) * (\text{P}_u) = (.75) * (.80) * (.83) * (.93) * (380 \text{ yd}^3/\text{hr})$$

The resulting site specific **Production Rate** is 176 yd<sup>3</sup> per hr.

**Exterior Dike Reclamation Time:**

Due too extremely wet conditions during late fall, early spring and winter, six months will be considered the number of working months per year. This affects the number of mobilizations that will take place and will directly affect the cost as will be shown later. The operator will not work Saturday or Sunday. He will be paid for The shifts will be 8 hour shifts, 5 days per week or on a monthly basis it will be 173 hrs per month. This is calculated using the following relationship:

$$T = (D - W/12) * 8$$

where

T = Total Hours per month

D = Days per year (364)

W = Days in weekends per year (104)

12 = Months per year

8 = Working hours per day

$$T = ((364 \text{ days per year} - 104 \text{ weekend days per year}) / 12 \text{ months per year}) * 8 \text{ hours per day}$$

$$T = 173 \text{ hrs per month}$$

The operators will be paid 60 hrs per month at 1.5 times the pay rate to compensate for the 10 holidays and 10 days of paid vacation. (This would equate to 1.7 days per month).

$$Otd = (10 + 10) / 12$$

Otd = Overtime Days

10 = 10 holidays

10 = 10 vacation days

12 = months per year

$$Otd = (10 \text{ holidays per year} + 10 \text{ vacation days per year} / 12 \text{ months per year})$$

$$Otd = 1.7 \text{ days per year}$$

Knowing the production rate per working hour, the monthly production rate of the dozer can be calculated. This was accomplished by using the relationship:

$$P_m = H_w * P_h$$

where:

P<sub>m</sub> = Monthly Production rates

H<sub>w</sub> = Working Hours per Month

P<sub>h</sub> = Hourly Production rates

$$P_m = 173 \text{ hr/month} * 176 \text{ yd}^3/\text{hr}$$

This calculation results in a monthly production rate of P<sub>m</sub> = 30,447 yd<sup>3</sup>per month.

Next, the total number of working months to complete the job can be calculated using the relationship:

$$M_t = Y_t / P_m$$

where:



$M_t$  = Total Number of Months to Complete the Job

$Y_t$  = Total cubic Yardage to be Moved

$P_m$  = Monthly Production Rate

$$M_t = 1,478,413 \text{ yd}^3 / 30,447 \text{ yd}^3 \text{ per month}$$

The total number of months it will take to complete the job will approximate  $M_t = 48.6$  months on the property for the D7R LGP dozer to complete the work required for reclamation.

### **Exterior Dike Reclamation Costs:**

#### **Operating Costs**

The operating costs were taken from the Machinery Information Division of PRIMEDIA Information Inc. Rental rate Blue Book Volume I page 9-45. They are \$33.50 times a Utah factor of 0.865 which equates to \$28.98 per hour. This can be viewed in Appendix 10.

The resulting costs are as follows:

$$O_{tc} = (173 * E_j) * O_c$$

where:

$O_{tc}$  = Total Monthly Operating Costs

$E_j$  = Operator Efficiency that was calculated in the Production Rate calculation above. In other words this is the only amount of time that the equipment will be operating. This is 0.83 or 50 minutes out of one hour.

173 = Number of work hours in a work month

$O_c$  = Operating Costs (\$28.98 per hour)

$$O_{tc} = (173 \text{ hrs. per month} * .83) * \$28.98 \text{ per hour}$$

This results in an operating cost for the dozer of  $O_{tc} = \$4,161$  per month.

#### **Equipment Rental Rates, Mobilization and Insurance:**

The local Caterpillar distributor, Wheeler Machinery, was consulted for rental rates. They are located at 4901 West 2100 South, West Valley City. Their rental rate as per 2 Jan 2001 was \$10,800 per month. This rate includes discounts for long term rental. Anything more than 176 hours is an additional cost but currently this project is estimated at 173 working hours per month so the regular rate with the discount will be employed for cost purposes. Insurance is \$928 per month. Wheeler Machinery charges a \$336 mobilization fee for projects located within a 2-hour drive of their office. This mobilization fee will apply over 6 months.

The equipment cost for this project is derived as follows:

$$E_r = (D_r) + ((M_r * 2)/6) + I_r$$

where:

$E_r$  is the monthly Equipment rate

$D_r$  = D7 Dozer Rate: \$10,800/month

$M_r$  = Mobilization Rate per event: \$336

$I_r$  = Insurance Rate: \$928/month

2 = Number of times per year that mobilization will occur

6 = Number of actual work months

$$E_r = (\$10,800/\text{month}) + ((\$336 * 2)/6) + \$928/\text{month}$$

This results in a monthly equipment rental rate of  $E_r = \$11,840$  per month.

This concurs well with the figure in the Machinery Information Division of PRIMEDIA Information Inc. For 3Q 2000, Rental Rate Blue Book Volume I, P. 9-45. Which lists the D7R-LGP for \$12,790 per month times the Utah Factor of 0.865 = \$11,063 per month not including mobilization and insurance.

#### **Operators' wages (including fringes)**

If the government was to contract out this effort, Davis-Bacon Act wages would have to be used. These wages for a dozer operator in Tooele County for 9/29/00 are found in Appendix 11. These include fringe benefits. The cost was formalized by the following correlation:

$$O_w = O_r * 173 + 1.7 * \$27.23 * 1.5$$

where:

$O_r$  = Operator wage rates of  $\$20.15 + 7.08 = \$27.23$  (Appendix 8)

173 = Number of work hours per month

$1.65 * \$27.23 * 1.5$  = Holiday and Vacation pay

$$O_w = \$27.23 \text{ per hour} * 173 \text{ hrs per month} + 1.7 \text{ days per month} * \$27.23 \text{ per hour} * 1.5$$

This results in a monthly Operator rate of  $O_w = \$4780$  per month.

#### **Travel Cost**

Because of the remoteness of the project location, travel compensation will be necessary. This rate is set \$0.30 per mile. The weekly travel estimates for the operator will ( $\$0.30/\text{mile} * 5 \text{ days per week} * 180 \text{ miles per day}$ ) for traveling on the weekdays. There will also be an allowance for travel of a supervisor to inspect the job progress once every two weeks. The traveling distance covered will be 180 miles round trip. This is sufficient for travel to and from Salt Lake City, Utah. All federal documents related to the per diem can be viewed in Appendix 12.

The overall amount for travel will be calculated using the following relations:

1 month =  $9\frac{1}{3}$  weekend days

1 month =  $21\frac{2}{3}$  working days (173 hrs per month)

This was calculated as follows:

$$T_c = O_t + S_t + O_p + S_p + T_p$$

$$O_t = (M_r * O_m) * 4.3$$

$$S_t = (M_r * S_m) * 4.3$$

where:

$O_t$  = Operator Travel Costs

$S_t$  = Supervisor Travel Costs

$O_p$  = Operator Perdiem Costs = \$0.00 because mileage is paid on a daily basis

$S_p$  = Supervisor Perdiem Costs = \$0.00 because mileage is paid on a daily basis

$M_r$  = Mileage Rate of \$0.30 per mile

$O_m$  = Operator weekly mileage of 900

$S_m$  = Supervisor weekly mileage of 90 (or 360 for the month)

$D_r$  = Perdiem Rate of \$00 per day

21.67 = Number of working days per month

2 = Number of supervisor days per month

**T<sub>p</sub>** = Travel pay 4 hrs/day times 21.67 days/Mo times \$27.23/ hr = \$2360/ mo. The 4 hrs per day is for travel 2 hours each way to the site. In other words the operator will be paid for 12 hours per day. The mileage rate for the vehicle is for the amortization for the vehicle only.

**T<sub>c</sub>** = (\$.30 \* 900)\* 4.3 + (\$.30 \* 90)\*4.3 + 0 + 0 + \$2360 =  
The monthly travel costs equated to **T<sub>c</sub>** = **\$3637** per month.

#### **Summary of Exterior Dike Reclamation Costs:**

The following is a summary of all the costs included in the bond calculation:

#### **Contractor Overhead and Profit**

Means Facilities Construction Cost Data (1998) recommends a 20% increase to the total cost for the contractors overhead and profit. The reference page of cost data can be viewed in Appendix 13.

#### **Contingencies**

Means Facilities Construction cost Data (1998) recommends a 10% increase to the total cost for the contingencies in final working drawing stage. The reference page of cost data can be viewed in Appendix 5.

#### **Administrative Costs**

The Washington Office guidance is to apply 18%overhead on all projects dealing with 5XXX category. This project will be considered a 5XXX project. For the reference pages see Appendix 6.

**TABLE 6.**

<b>Summary of Exterior Dike Reclamation Costs</b>		
<b>Type</b>	<b>Cost (\$/Month)</b>	<b>Cost Cumm (\$/Month)</b>
Operating	\$4,161	\$4,161
Equipment	\$11,840	\$16,001
Operator	\$4,780	\$20,781
Travel	\$3,637	\$24,418
Subtotal direct costs	\$24,418	<b><u>\$24,418</u></b>
Contractor Overhead & Profit (20%)	\$4,884	\$29,302
Contingency (10%)	\$2,442	\$31,743
Subtotal of all costs		\$31,743
Administrative (18% of all costs)	\$5,714	<b><u>\$37,457</u></b>
Months	48.60	\$1,820,421
<b>Total Cost (\$2000)</b> <small>Numbers may not add because of rounding</small>	1.00	<b><u>\$1,820,421</u></b>



## **7 SYSTEM POND INTERIOR DIKES AND MAGNESIUM CHLORIDE STORAGE PONDS:**

The standard for the salt industry for maintaining the salt in a form that contains the least amount of contaminants is that the ponds are lined with salt. This ensures the fact that erosion of the dikes in the ponds does not bring foreign material into the salt. This also demands a maintenance procedure be put in place to keep the salt liner in-tact during operations. In order to keep the amount of dirt, clay and other foreign material to a minimum and to maintain the salt in the ponds as potentially extractable, BLM has chosen to require the operator to remove the interior dikes in the Pond 7 system. This will help keep the contamination of the salt to a minimum. The excess material will be removed to Pond 1 and spread on top of the salt in this pond which may not be extractable because of salt thickness necessary to support equipment. The Magnesium Chloride Storage Ponds are actually used as salt precipitation ponds rather than storage ponds. Because the South Pond has been compromised, the best recommendation is to remove the pond contents and the dike to the area of Pond 1. This will allow the salts in pond 1 to return back to the ground water more easily, where they may be recovered at a later time. The north storage pond can be covered with material from the Pond 7 system dikes and berms to stabilize the surface. Physical safety, preservation of the resource and long-term stability are key to this effort.

The total length of ditches and baffles were approximated from the map at Appendix 1 and verified with the map dated 1994 submitted from the company to BLM. Volumes were estimated using the resulting lengths which are as listed in Table 7.

**TABLE 7.**

<b>Total Length of Dikes (feet)</b>		
<b>Type</b>		<b>Dikes</b>
Pond 7a-7b and 7b-7c	(DOG #15)	51,000
Finished Brine South	(DOG #14)	2,400
Grand Total		53,400
Numbers may not add because of rounding		

The length of each ditch was then multiplied by the average cross sectional area. These areas for the berms were measured and the following areas were derived based upon actual field calculations . . . The diagrams are in Appendix 2.

Once this calculation is carried out, the resulting figure is the cubic feet of material that must be relocated. This figure was then converted into cubic yards using the following equation:

$$\text{ft}^3/27 = \text{yd}^3$$

where:

yd<sup>3</sup> = Cubic Yards of material

ft<sup>3</sup> = Cubic feet of material

The cubic yardage of material to be moved is summarized in Table 8.

**TABLE 8.**

<b>Cubic yards of material to be moved by a Wheeled Tractor (yd<sup>3</sup>)</b>			
<b>Type</b>	<b>Area (ft<sup>2</sup>)</b>	<b>Length (ft)</b>	<b>(yd<sup>3</sup>)</b>
Pond 7a-7b and 7b-7c (DWG #15)	50	51,000	94,444
Finished Brine South (DWG #2)	7,200	2,400	640,000
Grand Total			734,444
Numbers may not add because of rounding			

**Equipment Selection:**

Equipment selection was a CAT 631E or equivalent. This is a self loading scraper. Again the Caterpillar Handbook 30<sup>th</sup> edition (October 1999) was used for cost estimation purposes. The haul distance would be approximately 4,800 feet to Pond 1. This number was derived from taking the weighted average of 94,444 yd<sup>3</sup> at 17,000 feet and 640,000 yd<sup>3</sup> at 3,000 feet which are the approximate haul distances. From page 9-42 and 9-43 the haul time for approximately 4,800 feet is 1.8 minutes loaded and about 1.8 minutes empty. In addition to the scraper a dozer would be necessary. We will plan on using the D7RLGP dozer for pushing the material around and ensuring proper distribution.

From page 9-11, Appendix 14, the cycle time is estimated by  $C_t = L_t + H_t + S_t + R_t$ .

$C_t$  = Cycle Time

$L_t$  = The fixed load time for a 631E with Auger is 1.8 minutes. See page 9-42, Appendix 14.

$H_t$  = Haul time

$S_t$  = The spread and maneuver time is 0.7 minutes. It is understood that the grade is 0% and the rolling resistance is minimal. See page 9-11, Appendix 14.

$R_t$  = Return time unloaded for a 631E with Auger is 1.8 minutes. See page 9-43, Appendix 14.

$$C_t = 0.9 \text{ min} + 1.8 \text{ min} + 0.7 \text{ min} + 1.8 \text{ min.}$$

$C_t = 5.0$  minutes

In this case the total cycle time would be 12 trips per hour.

The machine is limited to 31 yd<sup>3</sup> heaped at 100% efficiency. The operation is expected to operate at 83% efficiency (50 minutes per hour) because the operator will have to take breaks, and maintain the equipment which will reduce the tonnage to 23.25 yd<sup>3</sup>. The total time that is necessary to move 734,444 yd<sup>3</sup> at 31 yd<sup>3</sup>/trip and 12 trips per hour at 83% efficiency is 2379 hrs. The number of months that it would take to do this job is estimated by dividing 2379 hrs by 173 hrs per month. This equates to 13.7 months.

A wheel scraper in a moderate to average work conditions has a life of 22,000 to 17,000 hours (Appendix 14, P. 22-71), therefore only requiring the equipment for approximately 10% of that time for this estimate we will rent the equipment. We contacted Wheeler Machinery on 3 January 2001 and they quoted an equipment rental for this piece of equipment of \$17,000 per month and an additional \$1635 per month for insurance. The operating cost was estimated from the Machinery Information Division of PRIMEDIA Information Inc. Rental rate Blue Book, Vol. I, P. 9-39 (Appendix 14) at \$72.35 per hour times the Utah factor of 0.865 which equates too \$62.58 per hour.

**Production Rate of the Equipment:**

The production rate of the Wheeled Tractor 631E series is taken from Appendix 15, page 9-5. The

machine is limited to 31 yd<sup>3</sup> when it is heaped.

The uncorrected Hourly Production ( $P_u$ ) = 12 Trips per hour \* 31 yds. per trip

$P_u = 372$  yd<sup>3</sup> per hr at 100% efficiency.

**Correction Factors:**

Job Efficiency ( $E_j$ ): The operator will be in charge of general maintenance of the equipment (lube, oil, filter). Taking this factor into account, along with startup time, breaks and miscellaneous delays, the efficiency of 50 min/hr is estimated. The suggested correction factor is 0.83.

Using these correction factors, the actual production is calculated as follows:

$$\text{Production Rate} = (E_j) * (P_u) = (.83) * (372) \text{ yd}^3 \text{ per hour}$$

The resulting site specific **Production Rate** is 309 yd<sup>3</sup> per hr.

**Reclamation Time:** This affects the number of mobilizations that will take place and will directly affect the cost as will be shown later. The operator will not work Saturday or Sunday. The shifts will be 8 hours shifts, 5 days per week. Taking into account, these constraints, there will be 173 working hours per month. Knowing the production rate per working hour, the monthly production rate of the scraper can be calculated.

$$P_m = H_w * P_h$$

where:

$P_m$  = Monthly Production rate

$H_w$  = Working Hours per Month

$P_h$  = Hourly Production rates

$$P_m = 173 \text{ hrs per month} * 309 \text{ yd}^3 \text{ per hr.}$$

This calculation results in a monthly production rate of  $P_m = 53,457$  yd<sup>3</sup> per month.

Next, the total number of working months to complete the job can be calculated using the relationship:

$$M_t = Y_t / P_m$$

where:

$M_t$  = Total Number of Months to Complete the Job

$Y_t$  = Total cubic Yardage to be Moved

$P_m$  = Monthly Production Rate

$$M_t = 734,444 \text{ yd}^3 / 53,457 \text{ yd}^3 \text{ per month}$$

The total number of months it will take to complete the job will approximate  $M_t = 13.7$  months on the MagCorp Knolls Facility for the Wheel Tractor-Scraper to complete the work required for reclamation.

**Reclamation costs:**

**Operating Costs**

The operating cost was taken from the Machinery Information Division of Prime MEDIA Information Inc. Rental rate Blue Book Volume I page 9-45. They are \$72.35 times a Utah factor of 0.865 which equates too \$62.58 per hour. This can be viewed in Appendix 10.

The resulting costs are as follows:

$$O_{tc} = (173 * E_j) * \text{where:}$$

$O_{tc}$  = Total Monthly Operating Costs

$E_j$  = Operator Efficiency that was calculated in the Production Rate calculation above. In other words this is the only amount of time that the equipment will be operating. This is equal to 0.83

173 = Number of work hours in a work month

$O_c$  = Operating Costs (\$62.58 per hour)

$$O_{tc} = (173 \text{ hrs. per month} * .83) * \$62.58 \text{ per hour}$$

This results in an operating cost for the dozer of  $O_{tc} = \$8986$  per month.

### Operator's wages (including fringes)

If the government was to contract out this effort, Davis-Bacon Act wages would have to be used. These wages for a dozer operator in Tooele County for 1996 are found in Appendix 11. These include fringe benefits. The cost was formalized by the following correlation:

$$O_w = O_r * 173 + 1.7 * \$27.23 * 1.5$$

where:

$O_r$  = Operator wage rates of  $\$20.15 + 7.08 = \$27.23$  (Appendix 8)

173 = Number of work hours per month

$1.65 * \$27.23 * 1.5$  = Holiday and Vacation pay per month

$$O_w = \$27.23 \text{ per hour} * 173 \text{ hrs per month} + 1.7 \text{ days per month} * \$27.23 \text{ per hour} * 1.5$$

This results in a monthly Operator rate of  $O_w = \$4778$  per month.

### Travel Cost

Because of the remoteness of the project location, travel compensation will be necessary. This rate is set \$0.30 per mile. The weekly travel estimate for the operator will (\$0.30/mile \* 900 miles) for traveling on the weekends. There will also be an allowance for travel of a supervisor to inspect the job progress once every two weeks. The traveling distance covered will be 180 miles round trip. This is sufficient for travel to and from Salt Lake City, Utah. All federal documents related to the per diem can be viewed in Appendix 12.

The overall amount for travel will be calculated using the following relations:

1 month =  $8\frac{1}{3}$  weekend days

1 month =  $21\frac{2}{3}$  working days (173 hrs per month)

This was calculated as follows:

$$T_c = O_t + S_t + O_p + S_p + T_p$$

$$O_t = (M_r * O_m) * 4.3$$

$$S_t = (M_r * S_m) * 4.3$$

where:

$O_t$  = Operator Travel Costs

$S_t$  = Supervisor Travel Costs

$O_p$  = Operator per diem Costs

$S_p$  = Supervisor per diem Costs

$M_r$  = Mileage Rate of \$0.30 per mile

$O_m$  = Operator weekly mileage of 900

$S_m$  = Supervisor weekly mileage of 90 (or 360 for the month)

$D_r$  = per diem Rate of \$00 per day

$21.67$  = Number of working days per month

$0$  = Number of supervisor days per month. Supervisors cost has been charged to the Dozer Cost.

$T_p$  = Travel pay 4 hrs/day times 21.67 days/Mo times \$25.75/ hr = \$2232/ mo

$T_c$  =  $(\$0.30 * 900) * 4.3 + 0 + 0 + 0 + \$2232 =$

The monthly travel costs equated to  $T_c = \$3393$  per month.

### **Summary of Interior Dike and Brine Storage Reclamation Costs:**

The following is a summary of all the costs included in the bond calculation:

#### **Contractor Overhead and Profit**

Means Facilities Construction Cost Data recommends a 20% increase to the total cost for the contractors overhead and profit. The reference page of cost data can be viewed in Appendix 13.

#### **Contingencies**

Means Facilities Construction cost Data recommends a 10% increase to the total cost for the contingencies in final working drawing stage. The reference pate of cost data can be viewed in Appendix 5.

#### **Administrative Costs**

The Washington Office guidance is to apply 18%overhead on all projects dealing with 5XXX category. This project will be considered a 5XXX project. For the reference pages see Appendix 6.

**TABLE 9.**

<b>Summary of Interior Dike and South Brine Storage Reclamation Costs</b>		
<b>Type</b>	<b>Cost (\$/Month)</b>	<b>Cost Cummm (\$/Month)</b>
Operating	\$8,986	\$8,986
Equipment	\$18,635	\$27,621
Operator	\$4,780	\$32,401
Travel	\$3,393	\$35,794
Subtotal Direct Costs	\$35,794	<b><u>\$35,794</u></b>
Overhead & Profit (20%)	\$7,159	\$42,953
Contingency (10%)	\$3,579	\$46,532
Subtotal all costs		<b><u>\$46,532</u></b>
Administrative (18%) of all costs	\$8,376	\$54,908
Months	13.70	\$752,240
<b>Total Scraper Cost</b>	1.00	<b>\$752,240</b>
Dozer Cost D7RLGP (\$37,454/mo)	13.70	\$513,120
<b>Grand Total Interior Dike Reclamation (\$2000)</b>		<b><u>\$1,265,359</u></b>
Numbers may not add because of rounding		

**Road Reclamation.**

Rational. Because of the small amount of annual rain fall 6.44" (Averaged from Weather Station, Knolls 10NE from 1986 to 1995) it will be necessary to rip and plant the areas that have been disturbed in the dune area because the area will have a difficult time reestablishing the plant growth. It has been determined that a polypropylene mesh would be necessary in order to stabilize the ground so the seeds and the material would not blow away.

There are numerous roads that will require reclamation. The summation is contained in Table 10.

The cost was determined by using \$160 per acre for mulch, \$170 per acre for re-seeding and \$220 per acre for ripping. This totals \$550 per acre. These costs were obtained from the Utah Division of Oil, Gas and Mining and found in Appendix 20. A stabilizer from the Means Cost Estimating Guide 1998, page 57, Appendix 16 Item 704-0200, polypropylene mesh at \$1.96 per square yard was used.



**TABLE 10.**

<b>Road Reclamation (ft)</b>			
Type	Width (ft)	Length (ft)	(ft <sup>2</sup> )
Dunes	15	20,000	300,000
North Dike Roads	15	16,000	240,000
Roads to the Facility	15	6,000	90,000
Grand Total			630,000
Acres		14.5	
	<b>Cost/Unit</b>	<b>Acres</b>	<b>Total cost</b>
Cost of Ripping and re-seeding per acre	\$550	14.5	\$7,975
Cost of Stabilizer and installation per yd <sup>2</sup>	\$1.96	14.5	\$137,553
Subtotal Direct Costs			<b><u>\$145,528</u></b>
		<b>Cost</b>	<b>Cost Cumm</b>
OH & Profit 20%		\$29,106	\$174,633
Contingency 10%		\$14,553	\$189,186
Subtotal All Costs			<b><u>\$189,186</u></b>
Administrative 18% of all costs		\$34,054	\$223,240
<b>Total Cost</b>			<b><u>\$223,240</u></b>
Numbers may not add because of rounding			

Calculation for cost of stabilizer and installation per yd<sup>2</sup>

9 ft<sup>2</sup> per yd<sup>2</sup>

43,560 ft<sup>2</sup> per acre

43,560 ft<sup>2</sup> per acre / 9 ft<sup>2</sup> per yd<sup>2</sup> = 4840 yd<sup>2</sup> per acre

4840 yd<sup>2</sup> per acre \* 14.5 acres \* \$1.96 per yd<sup>2</sup> = \$137,553

### **Facilities and Pump Stations**

Rational: The facilities and pump stations and man-made structures will be required to be removed in order to remove physical safety hazards and to return the area back to a more natural condition.

The facilities and pump stations that will be included in this analysis will consist of the following items:

1. P1 Pump station, outlet structure, diesel tank and aqueduct.
2. P2 Pump station and outlet structure
3. Gate structure at Pond 0
4. Warehouse building
5. P7 Pump Station

6. Pump stations at brine storage facilities
7. Final Brine pump station and sump
8. Wells
9. Pipe at P2 feed ditch
10. Gates in the Pond 7 system

**TABLE 11.**

<b>Facility Reclamation</b>				
Type	Sq ft	Cost/ ft <sup>2</sup>	Total Cost	Estimation
P1 Pump Station (Concrete)	384	\$20.54	\$7,887	Note 1
P1, P2, P3, P4 & P5 Pump Stations P2 Feed Ditch pipe Building (steel)	6	\$4,800.00	\$28,800	Note 2
P1 Diesel Tank and Diesel Tank @ Building, and large tank at building	3	\$899.00	\$2,697	Note 3
P1 Outlet Structure (Concrete)	400	\$20.54	\$8,216	Note 4
P2 Outlet Structure (Concrete)	200	\$20.54	\$4,108	Note 5
Gates: Pond 5A, 5B, 7B, 7C, 7D	1,000	\$20.54	\$20,540	Note 6
Pond 0 Gate	1,080	\$20.54	\$22,183	Note 7
Finished Brine Sump	1,350	\$20.54	\$27,729	Note 8
Building (Concrete)	1,000	\$8.07	\$8,070	Note 9
Warehouse	1	\$8,400.00	\$8,400	Note 10
Well	1	\$500.00	\$500	Note 11
Total			\$139,131	
OH & Profit 0% Included in costs from Means Estimating Guide			\$139,131	
Contingency 10%			\$153,044	
Administrative 18%			\$180,591	
<b>Total Cost</b> <small>Numbers may not add because of rounding</small>			<b>\$180,591</b>	

The \$20.54 per square foot was derived using the Means Cost Estimating Guide for 1998 (page 39, Appendix 16) Concrete Removal. Plain concrete is figured at \$12.80 per ft<sup>2</sup> (Item 754-2440) and then add 20% (Item 754-2620) for heavy reinforcing. This brings the cost to \$15.30. Then haulage disposal was calculated at \$0.37 per sq ft @ 10 inches thick per 5 miles.

\$0.37 per sq ft haulage cost was determined as follows:

$\$12.10/\text{yd}^3 = \$12.10 \text{ per } 46,656 \text{ in}^3$  (Appendix 16, page 39, Item 754-4250)

$\$12.1 / 46,656 \text{ in}^3 = \$0.000259 \text{ per in}^3 = \$0.00259 \text{ per in}^2 \text{ per } 10" \text{ thick piece}$

$\$0.00259 \text{ per in}^2 \text{ per } 10" \text{ thick piece} * 144 \text{ in}^2 \text{ per ft}^2 = \$0.37 \text{ per ft}^2 \text{ per } 10" \text{ thick}$

A round trip to USPCI site and back would be about 30 miles (or 6 times \$0.37 would be \$2.24).

Disposal costs would be \$60 per ton (page 30, Item 612-0100) That equates to \$3.75 per sq ft @ 10" thick.  
Concrete weight 120 lbs/ft<sup>3</sup>

$2000 \text{ lbs per ton} / 120 \text{ lbs per ft}^3 = 16.66 \text{ ft}^3 \text{ per ton}$

$\$60 \text{ per ton} / 16.66 \text{ ft}^3 \text{ per ton} = \$4.50 \text{ per ft}^3$

$\$3.60 \text{ per ft}^3 / 1728 \text{ ft}^3 \text{ per in}^3 = \$0.002084 \text{ per in}^3$

$\$0.002605 \text{ per in}^3 * 10 = \$0.02084 \text{ per in}^2 \text{ per } 10\text{in thick}$

$\$0.02084 \text{ per in}^2 * 144 \text{ in}^2 \text{ per ft}^2 = \$3.00 \text{ per ft}^2 \text{ per } 10\text{in thick}$

Therefore the total cost would be  $\$15.30 + \$2.24 = \$17.54 + \$3.00 = \$20.54$

Company would not provide drawings.

Note 1. 384 sq ft was estimated using 24 columns times 4 sq ft at 10 inches thick

Note 2. Would be similar to Single family wood house demolition (Maximum \$4800 each, times 6 sites. See 604-1020 on page 30, Appendix 16)

Note 3. These would be equivalent to underground petroleum storage tank removal item 880-0110 page 43 Appendix 16. These tanks are not underground but footings and foundations would have to be removed therefore it is assumed to be an equivalent cost because we have no drawings. There are 3 tanks. Item 880-1023 for moving the tank is \$600 for 100 miles or \$6.00 per mile. At 30 miles this would be \$180 per tank. For 3 tanks this would be \$540. Item 880-0300 demands a cost to remove sludge and water remaining in the bottom of the tank. This would be \$179 per tank. Total Cost per tank would be \$480 for removal plus \$180 for haulage and \$179 for product removal and an estimated \$60 each for disposal costs. This would total \$899 for each tank.

Note 4. Estimated to be 20' by 20'

Note 5. Estimated to be 20' X 10'

Note 6. Each gate was estimated to be 10' X 5' and there are 4 sides which equals 200 sq ft each, There are 5 gates for a total of 1000 sq ft at 10" thick.

Note 7. The gate was estimated to be 20' X 15' top and bottom for a sq footage of 600 sq ft. There are 2 sides and 2 supports both estimated at 15' X 8' for a total of 480 sq ft. Grand total is 1080 sq ft at 10" thick.

Note 8. The sump is estimated at 15' X 15' for a total of 225 sq ft. There are 5 sides and a top for a total of 6 sides. This equates to 1350 sq ft

Note 9. The concrete for the building and the pad was estimated at 100' X 100' by 6" thick Slab on grade, reinforced with wire mesh was \$4.51 per sq ft. (Item 754-0420 page 39, Appendix 16). The cost for disposal

is \$4.50 per ft<sup>3</sup> or \$1.80 per ft<sup>2</sup> per 6 inches thick.(see calculation above for disposal cost)

Haul cost would be

\$0.22 per sq ft haulage cost was determined as follows:

$\$12.10/\text{yd}^3 = \$12.10 \text{ per } 46,656 \text{ in}^3$  (Appendix 16, page 39, element code 754-4250)

$\$12.1 / 46,656 \text{ in}^3 = \$0.000259 \text{ per in}^3 = \$0.001554 \text{ per in}^2 \text{ per 6" thick piece}$

$\$0.00154 \text{ per in}^2 \text{ per 6" thick piece} * 144 \text{ in}^2 \text{ per ft}^2 = \$0.22 \text{ per ft}^2 \text{ per 6" thick}$

A round trip to USPCI site and back would be about 30 miles (or 6 times \$0.22 would be \$1.32.

Total cost would be  $\$4.50 + \$1.80 + \$1.32 = \$8.07 \text{ per sq ft per 6 inches thick}$

Note 10. Warehouse was estimated as a three family, three story house at a maximum rate of \$8400. See Item 604-1320, page 30, Appendix 16.

Note 11. Estimate to plug, and remove casing on the well. No depth known

**Survey Monuments.** The Right-of-way specifically states that all survey monuments shall be re-established. It is unknown how many this may include. Because the ponds are now filled with salt in many of the areas, the survey monuments will have to be re-established in these areas. After consulting with the surveyors in the Utah State Office it was felt that between \$80,000 and \$100,000 would be adequate to cover the costs. The 2% of the total cost was then back calculated to arrive at this number. This is assumed to be accomplished by the Government surveyors and therefore there would be no indirect costs (Overhead and Profit, Contingency and Administrative Costs).

## BLM Contracted Oversight Costs

**TABLE 12**

BLM Contracted Oversight Costs			
Type	Cost	Number	Cost Cumulative
Government Technical GS-12 Equivalent	\$60,000	3	\$180,000
Government Administrative GS - 9 Equivalent	\$40,000	4	\$160,000
Vehicle	\$30,000	1	\$30,000
Subtotal Direct Costs			<b><u>\$370,000</u></b>
Over head and Profit (20%)	\$74,000		\$444,000
Contingency (10%)	\$37,000		\$481,000
Subtotal All Costs			<b><u>\$481,000</u></b>
Administrative Cost (18%) all costs	\$86,580		\$567,580
<b>Total Cost (\$2000)</b> <small>Numbers may not add because of rounding</small>			<b><u>\$567,580</u></b>

1 Technical person full time for 3 years similar to GS-12, \$60,000 per person per year

1 Administrative Person full time for 3 years plus one year at a GS-9, \$40,000 per person per year

Many different types of positions could qualify for this work. Pay rate is for expertise level.

## TOTAL BONDING REQUIREMENTS:

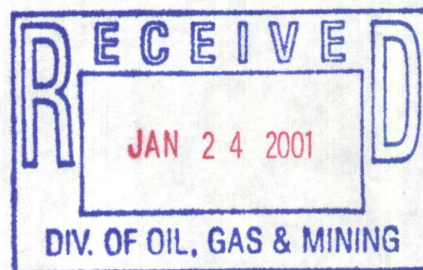
TABLE 13

Grand Total of MagCorp Reclamation Costs		
Type	Cost	Cost Cumulative
Ditches and Ditches	\$1,255,619	\$1,255,619
Exterior Dikes	\$1,820,421	\$3,076,040
Interior Dikes and South Brine Storage	\$1,265,359	\$4,341,399
Facilities and Pumps	\$180,591	\$4,521,990
Survey monuments 2% of the cost	\$90,440	\$4,612,430
Road Ripping and Re-seeding	\$223,240	\$4,835,670
Contract Oversight Cost	\$567,580	\$5,403,250
Total Cost (\$2000)		\$5,403,250
Grand Total With Escalation Factor for 5 Years into the future <small>Numbers may not add because of rounding</small>	1.12	<b>\$6,051,640</b>

### Escalation Factor for 5 Years

Western Mine Engineering, Mining Cost Service page CL-2 shows a cost index of Construction Labor at 14.73 in 1994 and in March 1999 the index was 16.77. This equates to 14% increase in Construction Labor. Equipment and Machinery increased by 10% over the same period of time. Therefore, we will average them at 12%. The reference page of cost data can be viewed in Appendix 4.

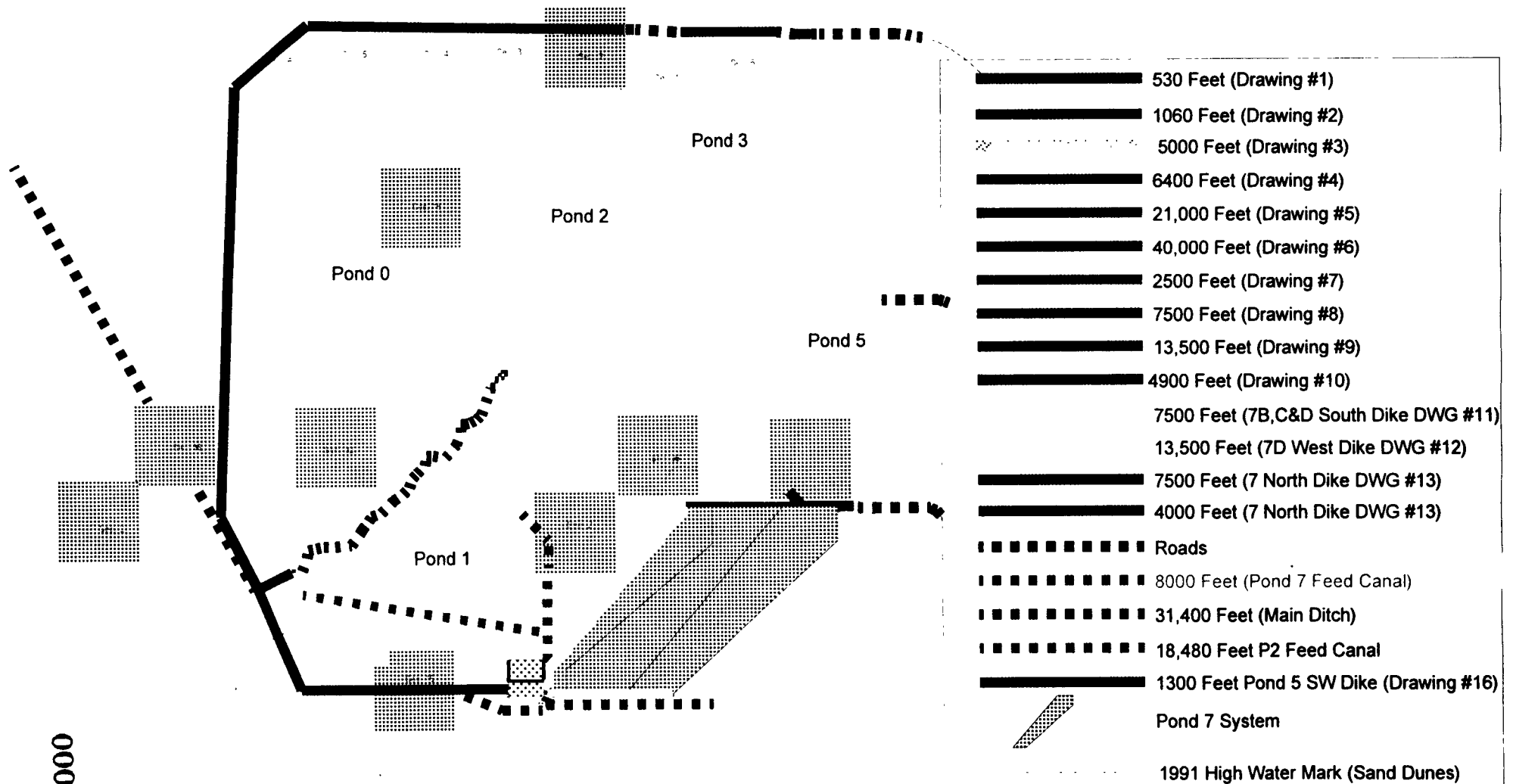
m/045/022



**APPENDIX 1**

(Map)

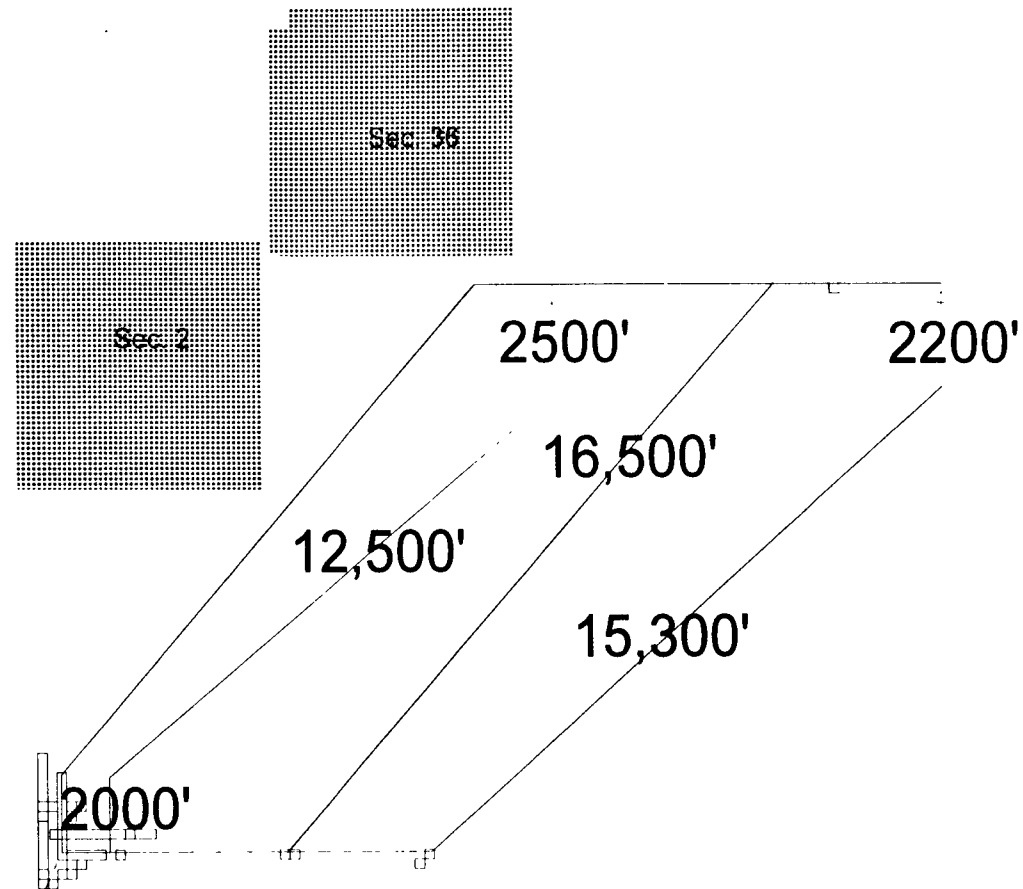
# Mag Corp Reclamation Requirements Map



000373

# Mag Corp Reclamation Requirements Map

## Pond System 7 Length Requirements



000374



## **APPENDIX 2**

(Ditches, Dames and Moore Estimate & UDOGM 1991 Report)

---

GEOTECHNICAL AND CONSTRUCTION COST  
STUDIES

**NEW SOLAR POND FACILITIES**

LOCATED ON  
WEST DESERT

FOR  
AMAX MAGNESIUM, INC.

---

**Dames & Moore**



ITEMIZED COST ESTIMATE

<u>ITEM</u>	<u>QUANTITY</u>	<u>UNIT COST</u>	<u>AMOUNT</u>
1. Canals			
a. Intake canal - cut	550,000cy	\$2.25/cy*	\$1,238,000 7.12 miles
b. P2 feed canal - cut	38,000cy	1.50/cy	57,000 1.553 miles
- fill (cast-up)	40,000cy	1.50/cy	60,000
c. 7E feed canal - fill (cast-up)	117,000cy	1.50/cy	176,000
			-----
Subtotal			\$1,531,000 =====
2. Pond Dikes			
a. Pond 1 - South Dike (15,000 LF)			
- sand dune fill	280,000cy		
- imported fill	70,000cy		
b. Pond 1 - Northwest Dike (2,500 LF)			
- cast-up fill	28,000cy		
- imported fill	10,000cy		
c. Pond 3 & 4 - Separation Dike (6,000 LF)			
- sand dune fill	66,000cy		
- imported fill	22,000cy		
d. Pond 3 - North Dike (8,000 LF)			
- cast-up fill	190,000cy		
- imported fill	50,000cy		
e. Pond 7E - West Dike (11,000 LF)			
- cast-up fill	75,000cy		

\* Higher unit cost reflects double handling required to pile all excavated material on east side of canal, as a foundation lift for inlet canal dike.

000377

APPENDIX C

PRELIMINARY\* COST ESTIMATE

WEST DESERT SOLAR PONDS

FOR AMAX MAGNESIUM, INC.

SUMMARY OF TOTAL COSTS

1. Direct costs	\$12,922,600
2. Indirect costs	850,000
3. Engineering design	478,000
4. Construction management	620,000
	=====

Project Total  
(installed cost)\*

\$14,870,600  
=====

SUMMARY OF DIRECT COSTS

1. Canals	\$ 1,531,000
2. Pond dikes and gates	3,577,000
3. Reservoirs	2,626,000
4. Buildings	618,500
5. Pumps and pump stations	1,234,400
6. Electrical	2,905,300
7. Miscellaneous construction	430,400
	=====

Total Direct Costs      \$12,922,600

\* This preliminary level estimate should not be construed to have an accuracy greater than  $\pm$  20 percent. It should be noted that unit costs quoted herein (particularly those related to earthwork operations) may be reduced 10% to 15% if work is initiated in 1987. This is primarily due to the existing favorable economic climate, expected to last through 1987.

:11- 97 : 13:11 :

TrustLandsAdmin-

SW  
FORM BY: TrustLandsAdminFORM MR-AR  
(Revised 12/90)RECEIVED  
JAN 22 1991DIVISION OF  
OIL, GAS & MINING

STATE OF UTAH  
DEPARTMENT OF NATURAL RESOURCES  
DIVISION OF OIL, GAS AND MINING  
355 West North Temple  
3 Triad Center, Suite 350  
Salt Lake City, Utah 84180-1203  
Telephone: (801) 538-5340  
Fax: (801) 359-3940

## ANNUAL REPORT OF MINING OPERATIONS

The informational requirements of this form are based on provisions of the Mined Land Reclamation Act, Title 40-8, Utah Code Annotated 1953, as amended, and the General Rules as promulgated under the Utah Minerals Regulatory Program. An operator conducting mining operations under a Notice of Intention must file an annual operations and progress report (FORM MR-AR) with the Division.

I. GENERAL INFORMATION

1. Report Time Period: From (mo./yr.) 1/90 To (mo./yr.) 17/90
2. DOGM File Number (original notice): M / 045 / 022
3. Mine Name: Knolls Solar Ponds
4. Legal Description (Location of Lands Affected):
 

Sections	<u>5-8, 17-21, 28-33</u>	Township <u>1N</u> , Range <u>12W</u>
Sections	<u>1-36</u>	Township <u>1N</u> , Range <u>13W</u>
Sections	<u>14, 23, 25, 26, 36</u>	Township <u>1N</u> , Range <u>14W</u>
Sections	<u>4-6, 7-9, 18, 19</u>	Township <u>1S</u> , Range <u>12W</u>
Sections	<u>1-18</u>	Township <u>1S</u> , Range <u>13W</u>

SLBM, Tooele County, UT
5. Mineral(s) Mined: Magnesium Chloride Brine
6. Name of Operator or Company: Magnesium Corporation of America
7. Permanent Address: 238 North 2200 West  
Salt Lake City, Utah 84116

## 8. Company Representative (or designated operator):

Name: D.H. WilkinsonTitle: PresidentAddress: 238 North 2200 West, Salt Lake City, UT 84116Phone: (801) 532-2043

- ☐ Please check if any of the above information has changed since previous year.

II. MINING AND RECLAMATION

1. Was the mine active during the past year? Yes ☒ No ☐
2. If active, how much ore or mineral was mined? 206 million gallons MgCl<sub>2</sub> brine.
3. Briefly describe any new or additional surface disturbances that occurred during the past year. This description should include the type of work performed, volume of material moved, and the acreage affected.  
A canal was dug to connect P1 pump to P2 canal. The new canal is  
about 3-1/2 miles long, 30 feet wide and 8 feet deep. Excavated  
material was used for side-sills.
4. Briefly describe the reclamation work performed during the past year. This description should include acreage reclaimed, methods employed, and an evaluation of the results.  
None
5. What was the total unreclaimed acreage at years end? N/A



6. Briefly summarize mining and reclamation planned for the upcoming year.  
Plan to mine 200 million gallons brine during the year. No  
reclamation is required.

NOTE: Section III., "Additional Information" applies only to large mining operations.

### III. ADDITIONAL INFORMATION

1. An updated surface facilities map should be attached if there have been significant changes since the previous map was submitted.
2. Any monitoring results or other reports that are required under the terms of the approved notice of intention should also be attached.

### IV. SIGNATURE REQUIREMENT

I hereby certify that the foregoing is true and correct.

Name (Typed or Print):

Don H. Wilkinson

Title of Operator:

President, Magnesium Corporation of America

Signature of Operator:

*D. Wilkinson*

Date:

January 21, 1991

jb  
MNMR-AR

Cycle Time Estimating Chart

Model	307B	311B	312B, 312B L	315B, 315B L	317B L, 317B LN	318B L, 318B LN	320B	322B	325B	330B	345B*	360
Bucket Size L (yd³)	280	450	520	520	520	800	800	1000	1100	1400		1900
Soil Type	0.37	0.59	0.68	0.68	0.68	1.05	1.05	1.31	1.44	1.83		2.5
Digging Depth (m)	1.5	1.5	1.8	3.0	3.0	3.0	2.3	3.2	3.2	3.4		4.2
Digging Depth (ft)	5	5	6	10	10	10	8	10	10	11		14
Load Bucket (min)	0.08	0.07	0.07	0.10	0.10	0.09	0.09	0.09	0.09	0.09		0.10
Swing Loaded (min)	0.05	0.06	0.06	0.04	0.04	0.06	0.06	0.06	0.06	0.07		0.09
Dump Bucket (min)	0.03	0.03	0.03	0.02	0.02	0.04	0.03	0.04	0.04	0.04		0.04
Swing Empty (min)	0.06	0.05	0.05	0.05	0.05	0.06	0.05	0.06	0.06	0.07		0.07
Total Cycle Time (min)	0.22	0.21	0.21	0.21	0.21	0.25	0.23	0.25	0.25	0.27		0.30

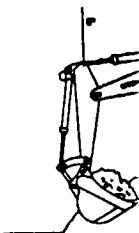
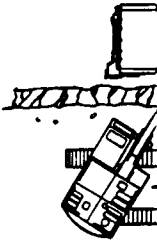
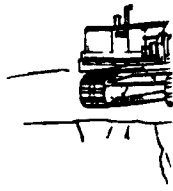
\*Information not available at time of printing.

CYCLE TIME ESTIMATING CHART													
CYCLE TIME	MACHINE SIZE CLASS												CYCLE TIME
	307	311B	312B	315B	318B L	320B	322B	325B	330B	345B*	350	375	
10 SEC.													
15													0.17 min.
20 SEC.													0.25 min.
25													0.33 min.
30 SEC.													0.42 min.
35													0.50 min.
40 SEC.													0.58 min.
45													0.67 min.
50 SEC.													0.75 min.
55													0.83 min.
60 SEC.													0.92 min.
													1.0 min.

\*Information not available at time of printing.

Caterpillar 300 Series  
move material faster a  
bucket, shortest stick  
longer stick and stand  
tion jobs.

MAXIMIZING PROD



**TABLE 2. Mining and Milling Cost Indexes**  
Source U.S. Department of Labor, Bureau of Labor Statistics

Note: All indexes are subject to revision four months after original publication.

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P
Year/ Month	Mine Labor	Construction Labor	Machinery & Equipment	Iron & Steel	Timber	Petroleum Products	Explosives	Tires	Industrial Commodities	RR. Transp. Metallic Ores	RR. Transp. Coal	RR. Transp. Non-Metallic Minerals	Electric Power	Industrial Chemicals	Coal	Natural Gas
1985	2.92	3.70	27.2	28.9	28.9	12.3	33.3	36.4	30.9				21.2	27.7	17.5	
1986	3.05	3.89	28.1	29.1	30.4	12.8	32.8	37.3	31.5				21.1	27.9	17.9	
1987	3.19	4.11	29.1	29.5	31.1	13.1	33.5	36.8	32.0				21.1	28.4	18.7	
1988	3.35	4.41	30.7	30.1	37.5	12.9	34.2	37.8	32.8				21.3	28.6	19.4	7.8
1989	3.60	4.79	32.1	31.6	41.8	13.1	35.0	36.2	33.9	24.2	24.8	23.5	21.6	28.4	21.1	7.7
1970	3.85	5.24	33.7	34.0	35.2	13.3	35.7	38.8	35.2	26.4	26.9	25.4	22.5	28.6	28.1	7.9
1971	4.06	5.69	35.4	35.9	44.0	14.1	37.9	40.6	36.5	29.9	30.7	28.4	24.8	28.9	34.0	8.4
1972	4.44	6.06	36.6	37.9	52.1	14.3	38.5	41.0	37.8	31.0	31.9	29.5	26.2	28.7	36.2	8
1973	4.75	6.41	38.0	40.2	66.6	16.9	40.2	42.6	40.3	32.2	32.8	30.5	28.0	29.3	40.8	
1974	5.23	6.81	44.3	52.7	65.7	29.3	50.2	52.1	49.2	37.5	38.3	35.4	36.4	43.0	62.2	11...
1975	5.95	7.31	53.9	59.3	62.4	33.8	59.5	57.2	54.9	43.2	44.0	40.5	44.3	58.7	71.2	16.1
1976	6.46	7.71	57.8	63.7	77.1	36.3	62.6	63.6	58.4	47.9	49.4	45.0	47.9	62.2	68.9	21.8
1977	6.94	8.10	62.1	68.0	92.5	40.5	64.9	66.9	62.5	51.2	52.4	48.3	54.3	63.5	72.8	30.8
1978	7.67	8.66	67.7	74.8	107.6	42.2	69.8	70.7	67.1	55.1	56.5	52.0	59.1	64.0	80.4	36.5
1979	8.49	9.27	74.5	83.6	118.1	58.4	75.5	80.9	75.7	63.8	65.9	60.6	64.5	74.9	84.3	47.6
1980	9.17	9.94	84.2	90.0	107.3	88.6	84.0	92.1	88.0	74.5	75.8	72.2	77.8	91.9	87.4	63.3
1981	10.04	10.82	93.3	98.5	106.6	105.9	96.7	99.5	97.4	86.1	86.9	86.4	89.2	103.1	93.0	82.1
1982	10.77	11.63	100.0	100.0	100.0	100.0	100.0	100.0	100.0	93.9	95.4	93.3	100.0	100.0	100.0	100.0
1983	11.28	11.94	102.3	101.3	115.0	89.9	101.1	95.7	101.1	95.9	96.5	94.6	103.1	97.3	100.5	106.6
1984	11.63	12.13	103.8	105.3	110.0	87.4	103.6	93.4	103.3	99.4	99.9	98.9	108.4	96.8	102.2	106.1
1985	11.98	12.32	105.4	104.8	107.4	83.2	105.0	90.5	103.7	100.2	100.0	100.1	112.8	96.0	102.2	102.9
1986	12.46	12.46	106.7	101.1	108.4	53.2	103.6	88.0	100.0	100.5	100.7	101.6	114.5	91.5	100.8	99.6
1987	12.54	12.71	108.9	104.6	116.1	56.8	107.3	87.7	102.6	99.0	100.1	101.1	111.9	95.5	97.1	79.5
1988	12.80	13.08	111.8	115.7	112.4	53.9	109.0	92.5	106.3	103.9	104.3	106.1	112.6	106.8	95.4	77.4
1989	13.26	13.54	117.2	119.1	127.1	61.2	117.6	96.3	111.6	105.8	105.3	108.3	116.2	114.8	95.5	82.0
1990	13.68	13.77	121.6	117.2	123.8	74.8	125.6	93.8	115.8	108.5	104.2	111.7	119.6	113.2	97.5	80.4
1991	14.19	14.00	125.2	114.1	125.7	67.2	132.1	95.7	116.5	108.7	105.2	115.9	128.1	111.8	97.2	79.1
1992	14.54	14.15	128.7	111.5	148.6	64.7	132.0	96.3	117.4	106.6	105.9	117.6	129.6	109.3	95.0	80.6
1993	14.60	14.38	132.0	116.0	183.4	62.0	132.6	95.3	118.9	106.7	106.6	119.3	130.6	110.4	96.1	8
1994	14.88	14.73	133.7	122.0	198.1	59.1	139.5	93.8	120.7	104.6	107.5	119.7	129.2	114.3	96.7	
1995	15.30	15.08	136.7	128.8	178.5	60.8	144.2	93.0	125.5	101.9	107.3	119.5	130.8	128.4	95.0	66.6
1996	15.61	15.46	139.8	125.8	189.5	70.1	146.4	90.6	127.3	103.5	106.7	119.2	131.6	126.7	94.5	91.2
1997	16.17	16.03	142.2	126.5	206.5	68.0	149.1	89.0	127.7	103.4	107.0	120.6	130.8	126.4	96.3	101.7
1998	16.95	16.56	145.1	122.6	182.4	51.3	147.3	89.6	124.8	104.2	109.0	120.9	130.0	121.6	93.1	83.7
1998-Jan.	16.85	16.25	144.8	127.0	190.9	57.4	149.2	89.3	125.9	105.1	110.6	121.2	127.4	125.8	91.7	90.9
1998-Feb.	16.89	16.21	144.9	126.6	192.9	54.4	149.5	90.2	125.3	105.8	110.3	121.4	127.2	124.1	94.5	81.9
1998-Mar.	16.89	16.29	145.0	125.7	193.7	50.6	148.6	90.2	125.0	105.6	109.0	121.4	126.7	123.1	93.5	86.4
1998-Apr.	16.84	16.34	145.0	125.5	193.4	52.7	148.3	90.0	125.3	106.2	109.0	121.5	126.4	122.3	95.2	90.1
1998-May	16.73	16.42	145.2	125.3	187.0	54.9	146.4	89.1	125.5	106.2	109.0	121.5	129.2	121.9	94.5	90.5
1998-June	16.73	16.44	145.3	125.0	177.1	53.2	146.5	89.7	125.1	106.2	108.7	121.5	133.8	121.4	94.7	81.9
1998-July	16.81	16.63	145.3	124.2	181.6	52.1	146.5	89.0	125.3	103.7	108.3	121.5	134.8	121.1	94.3	89.0
1998-Aug	16.94	16.74	145.4	122.6	183.4	49.1	146.6	88.8	124.5	103.7	108.3	121.7	135.2	120.4	90.7	82.1
1998-Sept	17.16	16.76	145.3	120.5	175.2	49.7	146.6	89.9	124.1	103.7	108.3	121.7	135.4	119.5	91.0	69.8
1998-Oct.	17.13	16.86	145.2	117.6	171.9	51.0	146.9	89.8	124.2	102.5	108.4	121.7	130.4	119.2	92.8	77.6
1998-Nov	17.34	16.79	145.3	115.6	170.3	48.8	146.8	89.8	123.8	102.1	107.4	121.7	127.6	119.4	94.2	83.1
1998-Dec.	17.35	16.84	145.4	115.0	174.2	41.8	146.4	89.8	123.1	101.2	108.2	**	127.5	119.8	92.1	80.3
1999-Jan.	17.28	16.72	146.2	114.6	181.3	44.6	145.8	89.4	123.4	100.8	107.3	121.7	127.4	118.9	94.7	74.7
1999-Feb.	17.21	16.65	146.5	114.0	186.8	42.5	146.5	89.4	122.8	100.9	**	121.7	126.6	118.0	90.2	71.0
1999-Mar.	17.32	16.77	146.7	112.8	193.7	45.7	147.1	89.0	123.3	105.0	107.1	121.8	126.5	117.4	92.4	69.8

\*\* not available

# 010 | Overhead & Miscellaneous Data

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

010

## 010 000 | Overhead

			CREW	DAILY OUTPUT	LABOR HOURS	UNIT	1998 BARE COSTS				TOTAL INCL O&P
							MAT.	LABOR	EQUIP.	TOTAL	
004	0011	ARCHITECTURAL FEES									
	0020	For new construction									
	0060	Minimum				Project					4.90%
	0090	Maximum									16%
	0100	For alteration work, to \$500,000, add to fee									50%
	0150	Over \$500,000, add to fee									25%
012	0012	CONSTRUCTION COST INDEX (Appendix) for 67 major U.S. and									
	0021	Canadian cities, total cost, min. (Rock Springs, WY)				%					79.40%
	0050	Average									100%
	0101	Maximum (Anchorage, AK)									125.20%
014	0010	CONSTRUCTION ECONOMIES For bricklaying									
016	0010	CONSTRUCTION MANAGEMENT FEES \$1,000,000 job, minimum				Project					4.50%
	0050	Maximum									7.50%
	0300	\$5,000,000 job, minimum									2.50%
	0350	Maximum									4%
018	0010	CONSTRUCTION TIME Requirements									
020	0010	CONTINGENCIES Allowance to add at conceptual stage				Project					15%
	0050	Schematic stage									10%
	0100	Preliminary working drawing stage									7%
	0150	Final working drawing stage									2%
022	0010	CONTRACTOR EQUIPMENT See division 016									
024	0010	CREWS For building construction, see How To Use This Book									
028	0010	ENGINEERING FEES									
	0020	Educational planning consultant, minimum				Project					50%
	0100	Maximum									2.50%
	0200	Electrical, minimum				Contract					4.10%
	0300	Maximum									10.10%
	0400	Elevator & conveying systems, minimum									2.50%
	0500	Maximum									5%
	0600	Food service & kitchen equipment, minimum									8%
	0700	Maximum									12%
	0800	Landscaping & site development, minimum									2.50%
	0900	Maximum									6%
	1000	Mechanical (plumbing & HVAC), minimum									4.10%
	1100	Maximum									10.10%
	1200	Structural, minimum				Project					1%
	1300	Maximum									2.50%
034	0010	FIELD OFFICE EXPENSE									
	0100	Field office expense, office equipment rental average				Month	130			130	143
	0120	Office supplies, average					84			84	92.50
	0125	Office trailer rental, see division 015-904									
	0140	Telephone bill; avg. bill/month incl. long dist.				Month	230			230	253
	0160	Field office lights & HVAC					86			86	94.50
036	0010	FIELD PERSONNEL Clerk average				Week		255		255	405
	0100	Field engineer, minimum						610		610	965
	0120	Average						795		795	1,255
	0140	Maximum						910		910	1,405
	0160	General purpose laborer, average						840		840	1,325
	0180	Project manager, minimum						1,150		1,150	1,815
	0200	Average						1,285		1,285	2,030
	0220	Maximum						1,450		1,450	2,290

GENERAL REQUIREMENTS

042

0010	JO
0020	
0100	
0200	
0300	
0400	
0500	
0600	
0700	
0800	
0900	
1000	
1100	
1200	
1300	
1400	
0012	IF
0021	
0050	
0101	

046

United States Department of the Interior  
BUREAU OF LAND MANAGEMENT  
WASHINGTON, D.C. 20240

IN REPLY REFER TO:  
1681/1323 (880)

December 10, 1992

EMS Transmission 12/14/92  
Instruction Memorandum No. 93-84  
Expires 9/30/94

To: All WO and Field Officials

From: Director

Subject: Recovery of Indirect Administrative Costs

This instruction memorandum explains Bureau of Land Management (BLM) policy for the recovery of indirect costs associated with work done for non-BLM entities through reimbursements, service charges, road maintenance fee, and contributed funds accounts.

*Application of the Indirect Administrative Cost Rate*

The BLM is obligated by law and Governmentwide policy to collect indirect administrative costs when performing work for other entities, whether Federal, Non-Federal, or private. The indirect administrative cost rate generally applicable to all work is 18 percent of the total project cost, unless specifically exempted or reduced by other sections of this directive. All reimbursable projects in the Construction and Access (29XX), Management of Lands and Resources (49XX), and Oregon & California Grant Lands (69XX) appropriations, Service Charges (5XXX), and non-exempted Contributed Fund (71XX) projects are subject to the 18 percent indirect administrative cost rate. The indirect administrative rate for Road Maintenance Fee work in subactivities 9110 and 9120 remains at 5 percent of collections.

Also, reimbursable projects conducted for other Federal agencies with which the BLM has a National-level Memorandum of Understanding (MOU) which dictates a different administrative rate, such as the National MOU with the Forest Service which establishes a mutual indirect cost rate of 20 percent, and those projects covered by other MOUs with mutually adopted variable rates, are charged indirect administrative costs at the rate established by the appropriate MOU.

The indirect cost amounts collected by BLM will continue to be applied to a Bureauwide credit account and allocated on a Bureauwide basis as part of the 4830 (General Administration) cost targets to provide for the cost of supporting reimbursable, cost recoverable, and contributed fund projects.

000389



### ***Exceptions to the Indirect Administrative Cost Rate for Contributed Fund projects***

Projects in the Contributions Account (71XX) that the cognizant BLM State Director determines are of primary benefit to the general public and further Bureau management objectives may be exempted from application of any indirect administrative cost charges or may be given reduced indirect administrative cost rates. The State Director is responsible for making the determination of exemption and calculating the new rate. If two or more States are involved in the contributed funds project, the cognizant State Directors are responsible for assuring that similar rates are applied. For 71XX projects determined to be exempt or having a reduced rate, the cognizant State Director is responsible for submitting the waiver form (BLM Form 1681-3a) to the BLM Service Center Division of Finance.

The BLM California State Director is authorized to set the indirect administrative rate for the California Off-Highway Vehicle (OHV) contribution (7123) projects. The rates should reflect the actual support required for each project.

### ***Indirect Costs Associated with Fire Protection Reimbursements***

Fire protection and presuppression reimbursable work performed under subactivity 1590 (Fire Reimbursements) for National Agreement Cooperating agencies and presuppression work for State agencies covered by formal agreements are exempt from the indirect administrative cost rate. This category of exempt activities includes: dispatch and logistical support services; prevention and detection services; crews and personnel, telecommunication support services; smokejumper operations, fire suppression training and support and training materials necessary for fire preparedness. Participating agencies which provide similar and like services in presuppression activities are the following: USDA-Forest Service, NPS, BIA, and FWS, and State Forestry agencies engaged in wildfire suppression. The indirect administrative charge also does not apply to 1590 interagency core funding for BIFC under Interagency Agreement No. 18.

Functions such as management type work, fire planning, indirect office space charges and prescribed fire activities are *not* exempt from the indirect administrative charges. All project costs (i.e., personnel time, leave surcharge, travel, materials, equipment, facilities, and utility charges) for subactivity 1590 fire presuppression work, will continue to be recovered via the reimbursable process, and recorded on BLM Form 1681-3, Reimbursable Work Project Authorization, a copy of which should be sent to the BLM Service Center Division of Finance (SC-615).

### ***Review of the applicability of the full rate to certain reimbursable work***

The application of the full indirect administrative cost rate to certain types of reimbursable projects, such as tying other Federal agencies into existing third-party contracts, has been identified in some cases as not equitable. The concern is that a large contract or a pass-thru project does not necessarily cost the BLM as much in administrative support as projects with

a large proportion of direct labor intensive work, yet the same rate is charged. Based on requests from the cognizant State Director, the Headquarters Office will consider applying lower rates, such as 10 percent, for such projects. Such requests are to be sent to the Headquarters Office Division of Budget (WO-880) for review and approval.

***Waivers and Exceptions for other special projects***

There may be some rare instances where a reduction or waiver of the indirect administrative cost rate for a certain Reimbursable (49XX, 29XX, 69XX) project may facilitate the BLM's work. If the cognizant State Director believes that there is a project warranting such an exception, a waiver/reduction of the indirect administrative cost rate can be requested from the Headquarters Office Division of Budget (WO-880) by the State Director in writing. Requests will be reviewed and, if justified, approved for a waiver. However, the BLM incurs administrative costs with all projects. These indirect support costs must be funded either through the application of the indirect rate or by a subsidy from appropriated General Administration (4830) or other program dollars.

In no case will waivers or reductions in the indirect administrative cost rate for cost recoverable projects under the Service Charges, Deposits and Forfeitures account (5XXX) for otherwise non-exempt programs be considered. Since these projects are being accomplished for the benefit of non-governmental agencies or private entities, the BLM must recover the full indirect administrative cost rate under the law.

Any questions regarding this instruction memorandum may be referred to Harold Grayson, Division of Budget (WO-880), on (202) 208-4168.

Signed	Authenticated
Roger Hildebeidel	Georgette A. Fogle
Acting Assistant Director, Management Services	Directives (WO 855)

T1N R13W Section 1, 0 1 miles (528 ft)

Drawing #1 Entering Dunes

Volume approx 2000 yds

Area 101 73 ft<sup>2</sup> (Blue) CUT

Area 51.7 (Red) FILL

Area 4 70 ft<sup>2</sup>

Area 47 0 ft<sup>2</sup>

2.00 ft

Total Area 179.23 ft<sup>2</sup> (Blue)

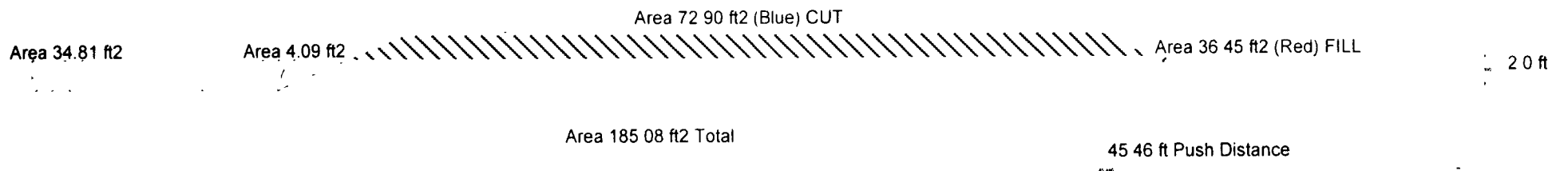
45.196 ft Push Distance

000393

T1N R12W Section 5, 0.2 miles (1056 ft)

Drawing #2 Between Dunes

Volume 2866 yds

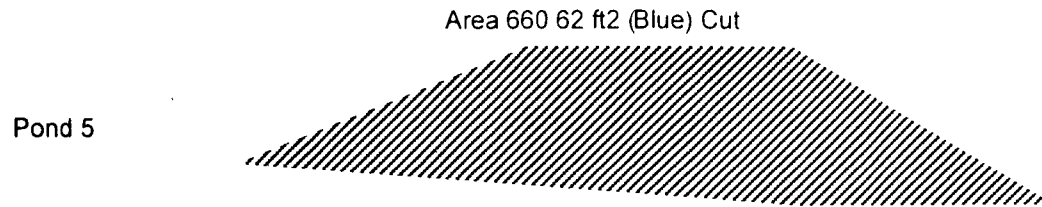


000394

T. 1 N., R. 12 W. Section 20 & 21, (5000 Feet distance)

Drawing #3 Pond 5 North Dike

Volume approx. 88,150 yds



Estimated from Pond 5 SW Dike + 5 feet Elevation

312 Feet PUSH Distance

Average 475.55 ft2

Pond 5 SW Dike

Area 290 5 ft2 (Blue) Cut



145 Feet PUSH Distance

000395

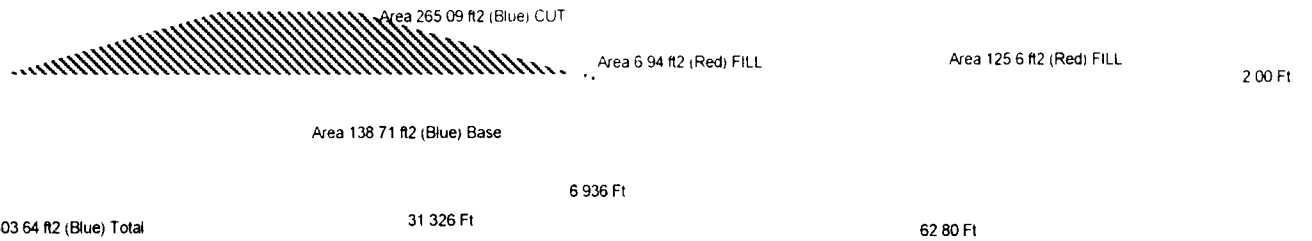


T1N R12W Section 6, 6400 ft.

Drawing #4 East end of Dune Field

Volume Approx. 62,815 yds.

101 074 Ft PUSH DISTANCE

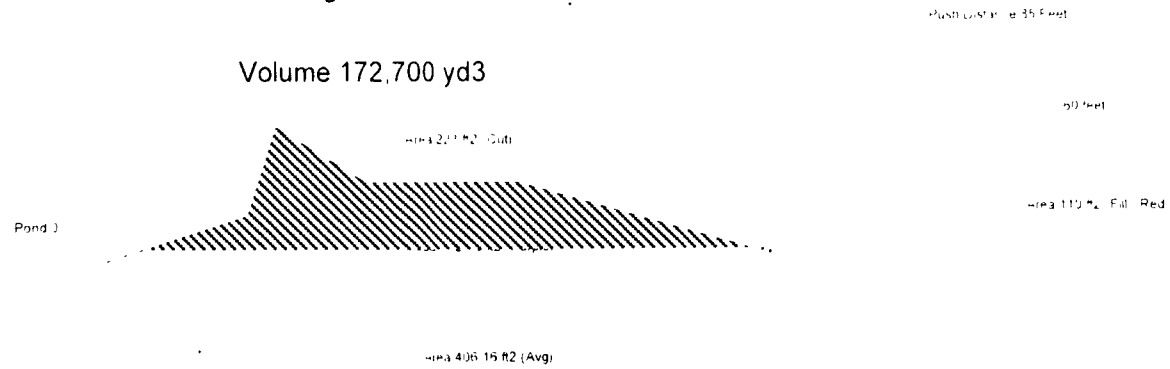


000396

T1N R13W Section 2, 3, 4, 5 (21,000 Feet)

Drawing #5 North Dike Pond 0

Volume 172,700 yd3



000397

T1NR13V/ Section 18 (40 000 Feet distance)

Drawing #6 West Lake

Volume approx 356 600 yds

1250 ft

Area 28 172 141 144

20 ft

1000

Area 11 971 144

1000

Area 11 971 144

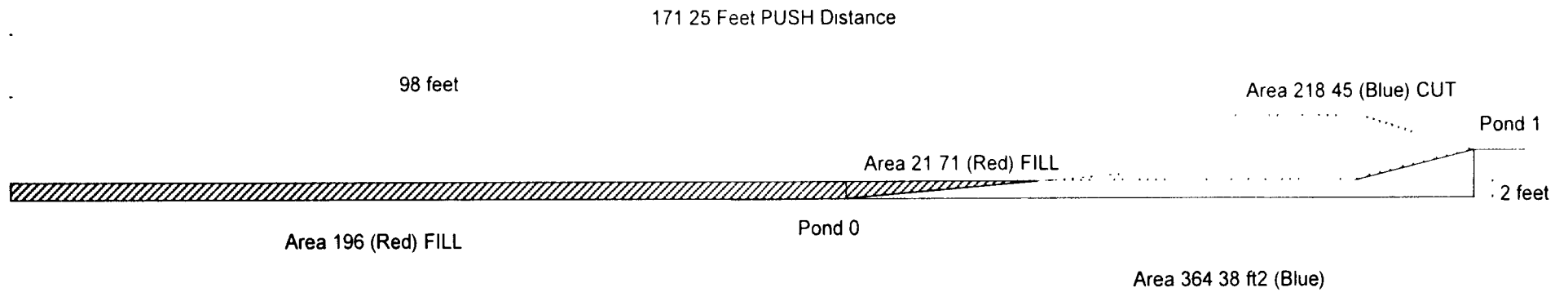
1000

000398

T. 1 S., R. 13 W. Section 7, (2500 Feet distance)

Drawing #7 Pond 0 - Pond1 Seperation

Volume approx. 21,000 yds



000399

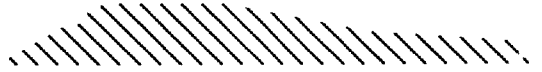
T 1 S , R 13 W Section 7 & 18, (7500 Feet distance)

Drawing #8 Pond1 West Dike

Volume approx 90.833 yds

Area 163.53 ft<sup>2</sup> (Red) FILL

Area 327.06 ft<sup>2</sup> (Blue) CUT



Area 11.0 ft<sup>2</sup> (Red) FILL

Area 152.5 ft<sup>2</sup> (Red) FILL

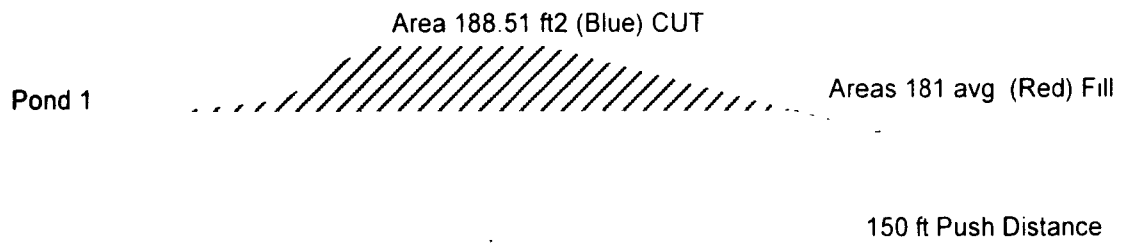
121.52 Feet Push Distance

000400

T. 1 S., R. 13 W. Section 15 & 17, (13,700 Feet distance)

Drawing #9 Pond1 South Dike

Volume approx. 95,900 yds



000401



T. 1 S., R. 13 W. Section 15, (4900 Feet distance)

Drawing #10 North Brine Storage Pond

Volume approx. 40,000 yds

147 Feet PUSH Distance

Area 220 ft<sup>2</sup> (Red) FILL

Plya Floor

4 1 Slope

Area 220 ft<sup>2</sup> (Blue) Cut

2 feet

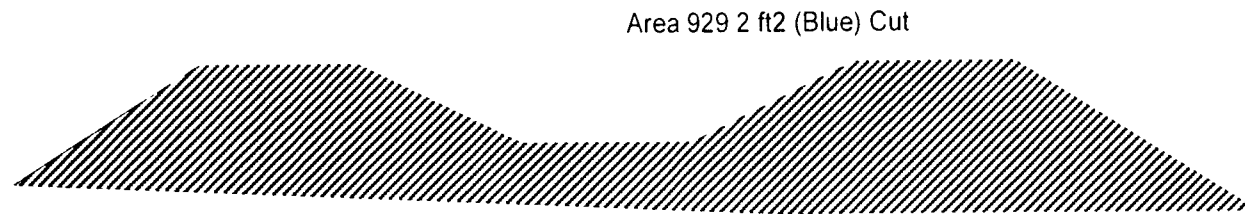
West End MgCl<sub>2</sub> Pond (North)

000402

T. 1 S., R. 13 W. Section 13 & 14, (7500 Feet distance)

Drawing #11 South Dike Pond 7 System

Volume approx. 258,000 yds



7 System Ponds

466 Feet PUSH Distance

000403

T1S R12W Secs 6,5,4 (7,500 Feet)

Drawing #13 7D North Dike

Volume 50,000 yds

Area 180 ft2 (Avg)

Pond 7D

Area 175 ft2 (Avg)

Plya Floor

Push Distance Approx 138 feet

T1S R12W Secs 6,5,4 (4,000 Feet)

Drawing #13 7D North Dike

Volume 11,000 yds

Area 73 ft2 (Avg)

Pond 5

Pond 7D

Push Distance Approx. 138 feet

Note Reference Drawing 14 for Notes.

000405

T1S R12W Secs. 5 (85,000 Feet)

Drawing # 15 & 17 Interior 7 System Dikes

Volume 158,000 yds

Average Area 50 ft<sup>2</sup>

Area 81.7 ft<sup>2</sup> (Avg)

Pond 7a

Pond 7b

Area 22.75 ft<sup>2</sup> (Avg)

Pond 7c

Pond 7c

000406

# **Caterpillar Performance Handbook**

---

**CATERPILLAR®**

000409



D7R XR

171 kW	230 hp
25 193 kg	55,600 lb
—	—
25 492 kg	56,200 lb
3306TA	
2100	
6	
121 mm	4.75"
152 mm	6"
10.5 L	638 in <sup>3</sup>
8	
610 mm	2'0"
3.05 m	10'0"
3.72 m <sup>2</sup>	5760 in <sup>2</sup>
1.98 m	6'6"
2.56 m	8'5"
3.35 m	10'11"
3.43 m	11'2"
—	—
5.81 mm	19'1"
4.67 m	15'4"
2.87 m	9'5"
2.59 m	8'6"
416 mm	16.4"
3.32 m	11'7"
4.50 m	14'9"
—	—
3.98 m	13'1"
3.69 m	12'2"
479 L	127 U.S. gal

it, horn, back-up alarm, retrieval



D7R LGP



D8R



D8R LGP



D9R

MODEL

	179 kW	240 hp	228 kW	305 hp	228 kW	305 hp	302 kW	405 hp
Flywheel Power								
Operating Weight: <sup>*</sup>								
Power Shift	27 065 kg	59,700 lb	—	—	—	—	48 440 kg	106,790 lb
Power Shift Differential Steer	27 364 kg	60,300 lb	37 580 kg	82,850 lb	33 730 kg	74,360 lb	48 840 kg	107,670 lb
Engine Model	3306TA		3406CTA		3406CTA		3408ETA	
Rated Engine RPM	2100		2100		2100		1900	
No. of Cylinders	6		6		6		8	
Bore	121 mm	4.75"	137 mm	5.4"	137 mm	5.4"	137 mm	5.4"
Stroke	152 mm	6"	165 mm	6.5"	165 mm	6.5"	152 mm	6"
Displacement	10.5 L	638 in <sup>3</sup>	14.6 L	893 in <sup>3</sup>	14.6 L	893 in <sup>3</sup>	18 L	1099 in <sup>3</sup>
Track Rollers (Each Side)	7		8		8		8	
ERF†	9		—		—		—	
Width of Standard Track Shoe	914 mm	3'0"	560 mm	1'10"	965 mm	3'2"	610 mm	2'0"
Length of Track on Ground	3.16 m	10'5"	3.21 m	10'6"	3.20 m	10'6"	3.47 m	11'5"
Ground Contact Area (W/Std. Shoe)	5.78 m <sup>2</sup>	8960 in <sup>2</sup>	3.57 m <sup>2</sup>	5544 in <sup>2</sup>	6.2 m <sup>2</sup>	9576 in <sup>2</sup>	4.24 m <sup>2</sup>	6569 in <sup>2</sup>
Track Gauge	2.24 m	7'4"	2.08 m	6'10"	2.34 m	7'8"	2.25 m	7'5"
GENERAL DIMENSIONS:								
Height (Stripped Top)**	2.74 m	9'0"	2.67 m	8'9"	2.67 m	8'9"	3.00 m	9'10"
Height (To Top of ROPS)	3.43 m	11'3"	3.51 m	11'6"	3.51 m	11'6"	3.99 m	13'1"
Height (To Top of ROPS Canopy)	3.52 m	11'6"	3.51 m	11'6"	3.51 m	11'6"	3.99 m	13'1"
Height (To Top of Cab ROPS)	3.58 m	11'9"	3.45 m	11'3"	3.45 m	11'3"	—	—
Overall Length (With SU Blade)***	—	—	6.39 m	21'0"	6.39 m	21'0"	6.84 m	22'5"
(Without Blade)	—	—	4.93 m	16'2"	4.93 m	16'2"	5.18 m	17'0"
Overall Length (With S Blade)	5.78 m	19'0"	—	—	—	—	—	—
(Without Blade)	4.67 m	15'4"	—	—	—	—	—	—
Width (Over Trunnions)	3.37 m	11'1"	3.05 m	10'0"	3.55 m	11'7"	3.30 m	10'10"
Width (W/O Trunnions — Std. Shoe)	3.15 m	10'4"	2.7 m	8'8"	—	—	2.93 m	9'8"
Width (With Standard Shoe)	—	—	—	—	3.37 m	10'10"	—	—
Ground Clearance	496 mm	17.5"	606 mm	1'11"	574 mm	1'10.6"	591 mm	1'11"■
Blade Types and Widths:								
Straight	4.50 m	14'9"	—	—	—	—	—	—
Angle Straight	—	—	4.99 m	16'4"	—	—	—	—
Universal	—	—	4.26 m	14'0"	3.94 m	12'11"	4.65 m	15'3"
Semi-U	—	—	3.94 m	12'11"	4.52 m	14'10"	4.32 m	14'2"
Fuel Tank Refill Capacity	479 L	127 U.S. gal	625 L	165 U.S. gal	625 L	165 U.S. gal	818 L	216 U.S. gal

\* Operating Weight includes ROPS canopy, operator, lubricants, coolant, full fuel tank, hydraulic controls and fluids, semi universal blade with tilt, back-up alarm, seat belts, lights, rigid drawbar and front towing device.

— D8R and D9R equipped with track guides, ROPS/FOPS cab, single shank ripper and SU blade.

\*\* Height (stripped top) — without ROPS canopy, exhaust, seat back or other easily removed encumbrances.

\*\*\* Includes drawbar.

■ SAE J1234.

† ERF — Extended Track Roller Frame. Extends frame 366 mm (14.4"). adds 3 track sections and 2 rollers/side.

000410



# Bulldozers

## Blade Specificati

- D6R • D6R XL • D6R LGP
- D7R • D7R LGP

MODEL	D6R, D6R XL & D6R LGP *					
	6S LGP		6A (IG)		6SU (IG)	
Type	Straight		Angling		Semi Universal	
Blade Capacities*	3.70 m <sup>3</sup>	4.83 yd <sup>3</sup>	4.3 m <sup>3</sup>	5.63 yd <sup>3</sup>	5.62 m <sup>3</sup>	7.4 yd <sup>3</sup>
Weight, Shipping** (Dozer)	2801 kg	6162 lb	3260 kg	7180 lb	2950 kg	6500 lb
Tractor & Dozer Dimensions:						
A Length (Blade Straight)	5.71 m	18'9"	—		—	
Blade Dimensions:						
B Width (including std. end bits)	3.99 m	13'1"	4.20 m	13'9"	3.56 m	11'8"
C Height	1101 mm	3'7.3"	1169 mm	3'10"	1412 mm	4'8"
D Max. Digging Depth	655 mm	2'1.2"	500 mm	1'7.7"	459 mm	18.1"
E Ground Clearance @ Full Lift	1083 mm	3'6.6"	1242 mm	4'1"	1195 mm	3'11"
F Manual Tilt	632 mm	2'0.9"	408 mm	16.1"	670 mm	2'2.4"
G Max. Pitch	+5.3°-4.8°		+5.3°-4.8°		+5.3°-4.8°	
H Max. Hydraulic Tilt	701 mm	2'3.6"	408 mm	16.1"	743 mm	2'5.3"
J Hydraulic Tilt (Manual Brace Centered)	385 mm	15.2"	408 mm	16.1"	743 mm	2'5.3"

\* Blade capacities as determined by SAE J1265.

Notice that the capacity of the U-blade is the volume carried by a straight blade of the same dimensions plus the volume included in the "cup" of the U-blade. It is intended for **relative comparisons of dozer sizes**, and not for predicting capacities or productivities in actual field conditions.

\*\* Shipping Weight — Total Bulldozer Arrangement includes: Blade, push arms or C-frame, braces, cylinders, lines, trunnions and lift cylinder mountings.

MODEL	D7R & D7R LGP									
	7A		7S		7SU		7U		7S LGP ERF†	
Type	Angling		Straight		Semi Universal		Universal		Straight	
Blade Capacities*	3.89 m <sup>3</sup>	5.08 yd <sup>3</sup>	5.16 m <sup>3</sup>	6.75 yd <sup>3</sup>	6.86 m <sup>3</sup>	8.98 yd <sup>3</sup>	8.34 m <sup>3</sup>	10.91 yd <sup>3</sup>	5.89 m <sup>3</sup>	7.7 yd <sup>3</sup>
Weight, Shipping** (Dozer)	3527 kg	7750 lb	3500 kg	7716 lb	3593 kg	7904 lb	3920 kg	8624 lb	3732 kg	8210 lb
General Dimensions (Tractor & Dozer)										
A Length (Blade Straight)	6.10 m	20'0"	5.81 m	19'1"	6.03 m	19'9"	6.27 m	20'7"	5.81 m	19'1"
Length (Blade Angled)	6.98 m	22'11"	—		—		—		—	
Width (Blade Angled)	4.12 m	13'6"	—		—		—		—	
Width (with C-Frame only)	3.09 m	10'1"	—		—		—		—	
Blade Dimensions:										
B Width (including std. end bits)	4.50 m	14'9"	3.90 m	12'10"	3.69 m	12'1"	3.98 m	13'1"	4.50 m	14'9"
C Height	1111 mm	3'7.7"	1363 mm	4'5.7"	1524 mm	5'0"	1553 mm	5'1.1"	1343 mm	4'4.9"
D Max. Digging Depth	669 mm	2'2.3"	527 mm	1'8.7"	527 mm	1'8.7"	527 mm	1'8.7"	668 mm	2'2.3"
E Ground Clearance @ Full Lift	1115 mm	3'7.9"	1145 mm	3'9.1"	1145 mm	3'9.1"	1145 mm	3'9.1"	1153 mm	3'9.4"
F Manual Tilt	466 mm	18.3"	—		—		—		—	
G Max. Pitch Adjustment	—		+3.1°-3.9°		+3.1°-3.9°		+3.1°-3.9°		+3.0°-3.9°	
Blade Angle (either side)	25°		—		—		—		—	
H Max. Hydraulic Tilt	627 mm	2'0.7"◀	845 mm	2'9.3"	799 mm	2'7.4"	861 mm	2'9.9"	686 mm	2'3"
J Hydraulic Tilt (Manual Brace Centered)	—		501 mm	1'7.7"	474 mm	18.6"	511 mm	1'8.1"	426 mm	16.8"

\* Blade capacities as determined by SAE J1265.

Notice that the capacity of the U-blade is the volume carried by a straight blade of the same dimensions plus the volume included in the "cup" of the U-blade. It is intended for **relative comparisons of dozer sizes**, and not for predicting capacities or productivities in actual field conditions.

\*\* Shipping Weight — Total Bulldozer Arrangement includes: Blade, push arms or C-frame, braces, cylinders, lines, trunnions and lift cylinder mountings.

† Extended track roller frame.

◀ Attachment includes two cylinders.

## MODEL

- Type
- Blade Capacities\*
- Weight, Shipping\*\*  
(Dozer)
- General Dimensions  
(Tractor & Dozer)
- A Length (Blade Straight)
- Length (Blade Angled)
- Width (Blade Angled)
- Width (with C-Frame only)
- Blade Dimensions:
- B Width (including std. end bits)
- C Height
- D Max. Digging Depth
- E Ground Clearance @ Full Lift
- G Max. Pitch Adjustment
- Blade Angle (either side)
- H Max. Hydraulic Tilt
- J Hydraulic Tilt (Manual Brace Center)
- K Pusharm Trunnion Width (to Ball Centers)
- Maximum Track Width Permitted

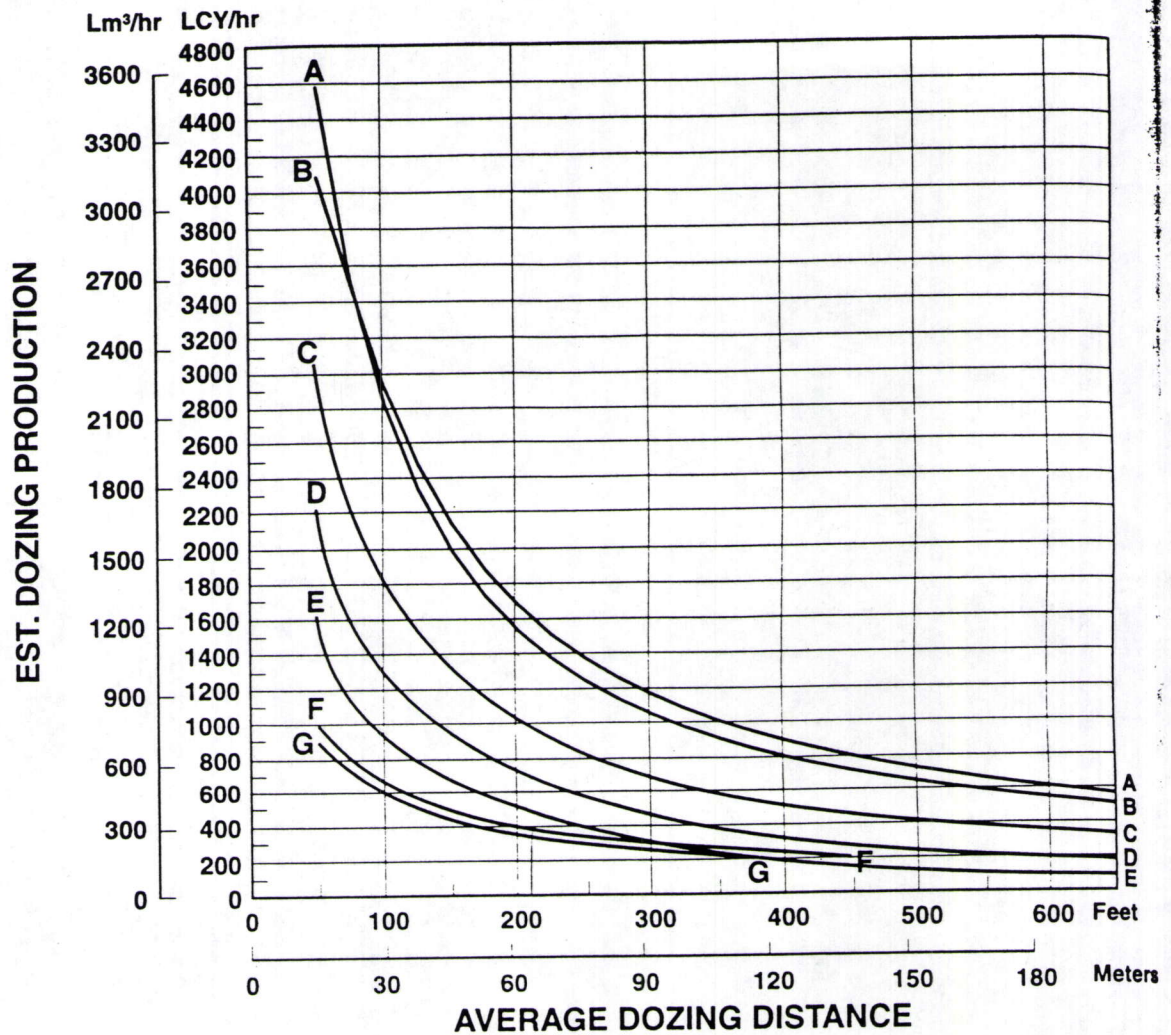
- Dual Tilt Option
- G Dual Pitch Adj.
- H Dual Max. Hyd. Tilt

\* Blade capacities as determined by SAE J1265.  
Notice that the capacity of the U-blade is the volume carried by a straight blade of the same dimensions plus the volume included in the "cup" of the U-blade. It is intended for **relative comparisons of dozer sizes**, and not for predicting capacities or productivities in actual field conditions.  
\*\* Shipping Weight — Total Bulldozer Arrangement includes: Blade, push arms or C-frame, braces, cylinders, lines, trunnions and lift cylinder mountings.  
◀ Attachment includes two cylinders

000411



## ESTIMATED DOZING PRODUCTION • Universal Blades • D7G through D11R



## KEY

- A — D11R-11U
- B — D11R CD
- C — D10R-10U
- D — D9R-9U
- E — D8R-8U
- F — D7R-7U
- G — D7G-7U

NOTE: This chart is based on numerous field studies made under varying job conditions. Refer to correction factors following these charts.



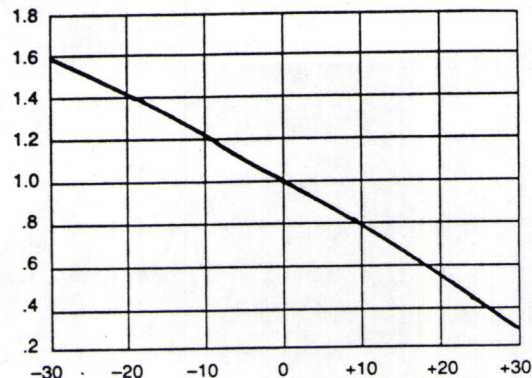
# JOB CONDITION CORRECTION FACTORS

	TRACK- TYPE TRACTOR	WHEEL- TYPE TRACTOR
<b>OPERATOR —</b>		
Excellent	1.00	1.00
Average	0.75	0.60
Poor	0.60	0.50
<b>MATERIAL —</b>		
Loose stockpile	1.20	1.20
Hard to cut; frozen —		
with tilt cylinder	0.80	0.75
without tilt cylinder	0.70	—
cable controlled blade	0.60	—
Hard to drift; "dead" (dry, non-cohesive material) or very sticky material	0.80	0.80
Rock, ripped or blasted	0.60-0.80	—
<b>SLOT DOZING</b>	1.20	1.20
<b>SIDE BY SIDE DOZING</b>	1.15-1.25	1.15-1.25
<b>VISIBILITY —</b>		
Dust, rain, snow, fog or darkness	0.80	0.70
<b>JOB EFFICIENCY —</b>		
50 min/hr	0.83	0.83
40 min/hr	0.67	0.67
<b>BULLDOZER*</b>		
Adjust based on SAE capacity relative to the base blade used in the Estimated Dozing Production graphs.		
<b>GRADES —</b> See following graph.		

\*NOTE: Angling blades and cushion blades are not considered production dozing tools. Depending on job conditions, the A-blade and C-blade will average 50-75% of straight blade production.

## % Grade vs. Dozing Factor

(-) Downhill  
(+) Uphill



## ESTIMATING DOZER PRODUCTION OFF-THE-JOB

### Example problem:

Determine average hourly production of a D8R/8SU (with tilt cylinder) moving hard-packed clay an average distance of 45 m (150 feet) down a 15% grade, using a slot dozing technique.

Estimated material weight is 1600 kg/Lm<sup>3</sup> (2650 lb/LCY). Operator is average. Job efficiency is estimated at 50 min/hr.

Uncorrected Maximum Production — 458 Lm<sup>3</sup>/h (600 LCY/hr) (example only)

Applicable Correction Factors:

Hard-packed clay is "hard to cut" material -0.80  
 Grade correction (from graph) .....-1.30  
 Slot dozing .....-1.20  
 Average operator .....-0.75  
 Job efficiency (50 min/hr) .....-0.83  
 Weight correction .....(2300/2650)-0.87

Production = Maximum Production × Correction Factors

$$= (600 \text{ LCY/hr}) (0.80) (1.30) (1.20) (0.75) (0.83) (0.87) = 405.5 \text{ LCY/hr}$$

To obtain production in metric units, the same procedure is used substituting maximum uncorrected production in Lm<sup>3</sup>.

$$= 458 \text{ Lm}^3/\text{h} \times \text{Factors} = 309.6 \text{ Lm}^3/\text{h}$$

000414

1-55



# TRACTORS & EARTHMOVING

## LGP CRAWLER DOZERS (cont.)

Model (Yr./Disc.)	Dozer Type	Operator Protection	HP	Monthly \$	Weekly \$	Daily \$	Hourly \$	Estimated Operating Cost \$/hr.
<b>DIESEL POWERED (CONT.)</b>								
<b>CATERPILLAR (cont.)</b>								
D5C III LGP HYSTAT	VPAT	ROPS	90.0	4,330.00	1,210.00	305.00	46.00	13.75
D5C SERIES III LGP	Power Angle Tilt	EROPS	91.0	4,480.00	1,255.00	315.00	47.00	14.05
D5C SERIES III LGP	Power Angle Tilt	ROPS	91.0	4,165.00	1,165.00	290.00	44.00	13.65
D5H LGP SERIES II (1996)	Power Angle Tilt	EROPS	130.0	6,485.00	1,815.00	455.00	68.00	19.40
D5H LGP SERIES II (1996)	Power Angle Tilt	ROPS	130.0	6,195.00	1,735.00	435.00	65.00	19.00
D5M LGP	Power Angle Tilt	EROPS	110.0	5,315.00	1,490.00	375.00	56.00	16.20
D5M LGP	Power Angle Tilt	ROPS	110.0	5,135.00	1,440.00	360.00	54.00	15.95
D6H DS LGP SERIES II (1997)	Straight	EROPS	165.0	7,815.00	2,190.00	550.00	83.00	23.45
D6H DS LGP SERIES II (1997)	Straight	ROPS	165.0	7,500.00	2,100.00	525.00	79.00	23.00
D6H LGP SERIES II (1997)	Straight	EROPS	165.0	7,550.00	2,115.00	530.00	80.00	23.05
D6H LGP SERIES II (1997)	Straight	ROPS	165.0	7,235.00	2,025.00	505.00	76.00	22.55
D6M LGP	Power Angle Tilt	EROPS	140.0	6,745.00	1,890.00	475.00	71.00	20.00
D6M LGP	Power Angle Tilt	ROPS	140.0	6,485.00	1,815.00	455.00	68.00	19.65
D6R DS LGP	Straight	EROPS	185.0	8,300.00	2,325.00	580.00	87.00	24.80
D6R DS LGP	Straight	ROPS	185.0	7,990.00	2,235.00	560.00	84.00	24.35
D6R LGP	Straight	EROPS	185.0	8,245.00	2,310.00	580.00	87.00	24.75
D6R LGP	Straight	ROPS	185.0	7,935.00	2,220.00	555.00	83.00	24.30
D7H DS LGP SERIES II (1996)	Straight	EROPS	215.0	11,830.00	3,310.00	830.00	125.00	32.00
D7H DS LGP SERIES II (1996)	Straight	ROPS	215.0	11,420.00	3,200.00	800.00	120.00	31.40
D7H LGP SERIES II (1996)	Straight	EROPS	215.0	11,380.00	3,185.00	795.00	120.00	31.50
D7H LGP SERIES II (1996)	Straight	ROPS	215.0	10,970.00	3,070.00	770.00	115.00	30.90
D7R DS LGP	Straight	EROPS	240.0	13,105.00	3,670.00	920.00	140.00	33.85
D7R DS LGP	Straight	ROPS	240.0	12,720.00	3,560.00	890.00	135.00	33.30
D7R LGP	Straight	EROPS	240.0	12,790.00	3,580.00	895.00	135.00	33.50
D7R LGP	Straight	ROPS	240.0	12,410.00	3,475.00	870.00	130.00	32.95
<b>DEERE</b>								
450H LGP	Power Angle Tilt	EROPS	74.0	3,780.00	1,060.00	265.00	40.00	12.05
450H LGP	Power Angle Tilt	ROPS	74.0	3,505.00	980.00	245.00	37.00	11.75
550H LGP	Power Angle Tilt	EROPS	84.0	4,290.00	1,200.00	300.00	45.00	13.30
550H LGP	Power Angle Tilt	ROPS	84.0	4,015.00	1,125.00	280.00	42.00	13.00
650H LGP	Power Angle Tilt	EROPS	90.0	4,610.00	1,290.00	325.00	49.00	14.10
650H LGP	Power Angle Tilt	ROPS	90.0	4,335.00	1,215.00	305.00	46.00	13.80
750B LGP (1995)	Straight	EROPS	140.0	5,415.00	1,515.00	380.00	57.00	19.15
750B LGP (1995)	Straight	ROPS	140.0	5,170.00	1,450.00	365.00	55.00	18.80
750C LGP	Straight	EROPS	140.0	6,535.00	1,830.00	460.00	69.00	19.85
750C LGP	Straight	ROPS	140.0	6,245.00	1,750.00	440.00	66.00	19.45
850B LGP (1995)	Straight	EROPS	165.0	6,815.00	1,910.00	480.00	72.00	22.70
850B LGP (1995)	Straight	ROPS	165.0	6,460.00	1,810.00	455.00	68.00	22.15
850C LGP	Straight	EROPS	185.0	8,230.00	2,305.00	575.00	86.00	24.90
850C LGP	Straight	ROPS	185.0	7,905.00	2,215.00	555.00	83.00	24.40
<b>DRESSER</b>								
TD12C LGP	Straight	EROPS	125.0	6,485.00	1,815.00	455.00	68.00	18.75
TD12C LGP	Straight	ROPS	125.0	6,125.00	1,715.00	430.00	65.00	18.30
TD15E LGP	Straight	EROPS	175.0	8,805.00	2,465.00	615.00	92.00	25.05
TD15E LGP	Straight	ROPS	175.0	8,465.00	2,370.00	595.00	89.00	24.55
TD20G LGP (1998)	Straight	EROPS	225.0	12,675.00	3,550.00	890.00	135.00	33.45
TD20G LGP (1998)	Straight	ROPS	225.0	12,320.00	3,450.00	865.00	130.00	32.90
TD20H LGP	Straight	EROPS	225.0	13,210.00	3,700.00	925.00	140.00	33.35
TD20H LGP	Straight	ROPS	225.0	12,555.00	3,515.00	880.00	130.00	32.55
<b>FURUKAWA</b>								
FD45P-1	Hyd	ROPS	39.0	2,490.00	695.00	175.00	26.00	8.30
<b>KOMATSU</b>								
D21P-7	Power Angle Tilt	EROPS	40.0	3,575.00	1,000.00	250.00	38.00	9.60
D21P-7	Power Angle Tilt	ROPS	40.0	3,165.00	885.00	220.00	33.00	9.05
D31P-20A	Power Angle Tilt	EROPS	70.0	4,270.00	1,195.00	300.00	45.00	12.40

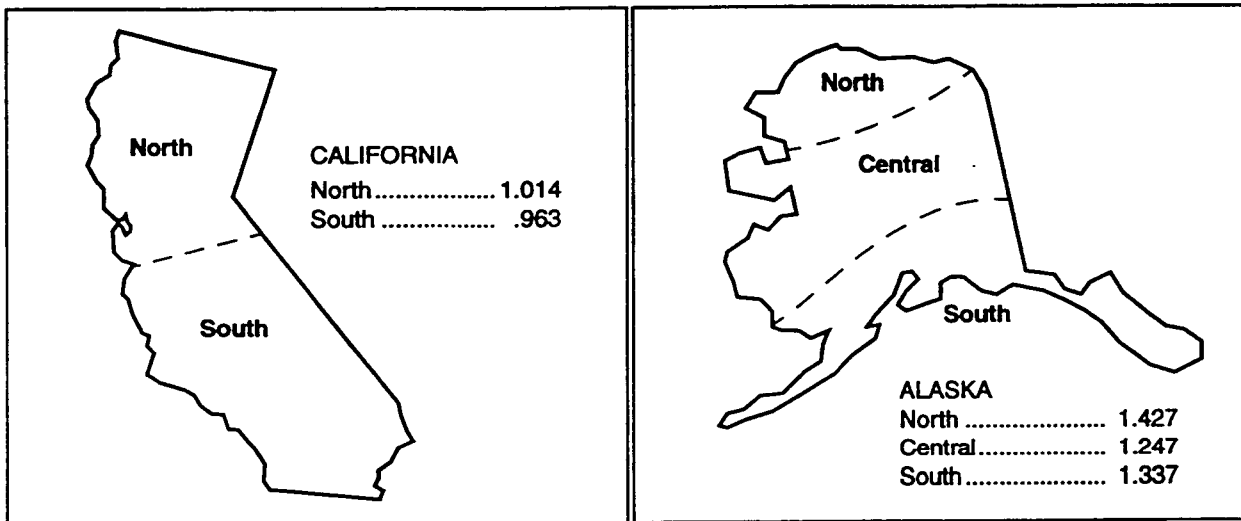
# TRACTORS & EARTHMOVING

## REGIONAL ADJUSTMENT MAPS

The following regional adjustments may be used to modify the average equipment rates shown in this section. These adjustments reflect regional variations in factors that affect equipment ownership costs. Adjustments for extreme variations within regions should be considered separately. To make regional adjustments, multiply the average rate by the factor listed for the specific region. For example:

$$\begin{array}{rcl} \text{Average Monthly Rate} & = & \$550.00 \\ \text{Regional Adjustment Factor} & = & \times 1.07 \\ \hline \text{Adjusted Monthly Rate} & = & \$588.50 \end{array}$$

Regional adjustment factors apply only to the rental rates; they are not meant to be adjustments to the "Estimated Operating Cost \$/Hr." For a complete statement on the *Regional Adjustment Maps*, see Section 1, "INTRODUCTION."



STATES		Adjustment
Alabama		.926
Alaska	North	1.427
	Central	1.247
	South	1.337
Arizona		.875
Arkansas		.918
California	North	1.014
	South	.963
Colorado		.919
Connecticut		1.037
Delaware		.952
District of Columbia		.960
Florida		.951
Georgia		.932
Hawaii		1.016
Idaho		.910
Illinois		1.014
Indiana		.985
Iowa		.951
Kansas		.937
Kentucky		.970
Louisiana		.942
Maine		.945
Maryland		.929
Massachusetts		1.031
Michigan		1.012
Minnesota		1.112
Mississippi		.919
Missouri		.978
Montana		1.012
Nebraska		.912
Nevada		.941
New Hampshire		.929
New Jersey		.962
New Mexico		.822
New York		1.079
North Carolina		.919
North Dakota		.990
Ohio		.996
Oklahoma		.918
Oregon		.938
Pennsylvania		1.040
Rhode Island		1.021
South Carolina		.909
South Dakota		1.002
Tennessee		.930
Texas		.889
Utah		.865
Vermont		.937
Virginia		.949
Washington		.978
West Virginia		.993
Wisconsin		1.080
Wyoming		1.027
ISLANDS		Adjustment
Guam		1.040
Marshall Islands		1.046
Puerto Rico		.906
Virgin Islands		.906

GENERAL DECISION UT000033 09/29/00 UT33  
General Decision Number UT000033

Superseded General Decision No. UT990033

State: Utah

Construction Type:  
HIGHWAY

County(ies):  
TOOELE

# HIGHWAY CONSTRUCTION PROJECTS

Modification Number	Publication Date
0	02/11/2000
1	09/29/2000

COUNTY(ies):  
TOOELE

\* ELEC0354C 06/01/2000

	Rates	Fringes
ELECTRICIANS	22.62	6.17+4.2%

	Rates	Fringes
SUUT3013A 03/27/1992		
CARPENTERS	16.28	2.63
CEMENT MASONS	11.00	
FLAGGERS	7.10	1.60
LABORERS:		
General Laborer, Fence Erector Laborer	12.27	2.77
Concrete Laborer (Compaction, Underground Fine Grading, Operation of Shute or Bucket)	12.27	2.77
Grade Laborer (Uses Hand Held Level To Check Grade, Inserts Grade Stakes In Concrete)	12.27	2.77
Asphalt Raker Laborer	12.70	2.64
Pipelayer (Smoothe sides and Bottoms of Trenches, Doe Rigging of Pipe, Assembles and Installs Concrete and Tile Pipe)	12.82	2.64
Laborer, Power Tools Cutting Torch, Operators of Gasoline, Electric or Pneumatic Tools, (E.G. Compressor, Compactor, Jackhammer, Vibrator, Concrete Saw, Chain Saw, and Concrete Cutting Torch)	12.82	2.64
Laborer, Sand Blaster (Surfaces That Will Not Be Repainted Exept For Highway Stripping)	12.27	2.77

000419



## POWER EQUIPMENT OPERATORS:

Backhoe/Loader Comb	21.05	7.08
Backhoe, All Sizes	17.85	6.96
Blade, Rough	21.35	7.63
Blade, Smoothe/Finish	19.72	7.22
Bulldozer, D7 or Less	20.15	7.08
Bulldozer, Over D7	21.05	7.23
Cranes, All Sizes	17.47	6.93
Heavy Duty Repairman	17.94	6.93
Loader, All Sizes	19.77	7.13
Paver, Asphalt	17.15	7.23
Roller, Asphalt	17.62	7.29
Roller Grader	17.47	6.73
Screedman	18.10	6.94
Sheepfoot Compactor	18.10	6.94
Tractor, Small rubber tire	24.20	.58
Tractor, w/Attachment	20.15	7.23

## TRUCK DRIVERS:

Dump Trucks - Water Level Capacity (Bottom, End and Side), Including Dumpster Truck, Turnawagons, Turna-rockers and Dumpcrete):

8 cu. yds. and Less than		
14 cu. yds.	15.99	5.70
14 cu. yds. and Less than		
35 cu. yds.	16.91	5.57

Water, Fuel and Oil Trucks:

1200 Gallons to less than		
2500 Gallons	17.19	5.87
2500 Gallons to less than		
4000	17.88	5.87
4000 Gallons to less than		
6000	16.29	5.52
Oiler Spreader Operator Where		
Boot Man is not required	17.72	5.90
Pickup Truck	17.21	5.70

WELDERS - Receive rate prescribed for craft performing operation to which welding is incidental.

Unlisted classifications needed for work not included within the scope of the classifications listed may be added after award only as provided in the labor standards contract clauses (29 CFR 5.5(a)(1)(v)).

In the listing above, the "SU" designation means that rates listed under that identifier do not reflect collectively bargained wage and fringe benefit rates. Other designations indicate unions whose rates have been determined to be prevailing.

## WAGE DETERMINATION APPEALS PROCESS

1.) Has there been an initial decision in the matter? This can be:

- \* an existing published wage determination
- \* a survey underlying a wage determination
- \* a Wage and Hour Division letter setting forth a position on a wage determination matter

- \* a conformance (additional classification and rate) ruling

On survey related matters, initial contact, including requests for summaries of surveys, should be with the Wage and Hour Regional Office for the area in which the survey was conducted because those Regional Offices have responsibility for the Davis-Bacon survey program. If the response from this initial contact is not satisfactory, then the process described in 2.) and 3.) should be followed.

With regard to any other matter not yet ripe for the formal process described here, initial contact should be with the Branch of Construction Wage Determinations. Write to:

Branch of Construction Wage Determinations  
Wage and Hour Division  
U. S. Department of Labor  
200 Constitution Avenue, N. W.  
Washington, D. C. 20210

- 2.) If the answer to the question in 1.) is yes, then an interested party (those affected by the action) can request review and reconsideration from the Wage and Hour Administrator (See 29 CFR Part 1.8 and 29 CFR Part 7). Write to:

Wage and Hour Administrator  
U.S. Department of Labor  
200 Constitution Avenue, N. W.  
Washington, D. C. 20210

The request should be accompanied by a full statement of the interested party's position and by any information (wage payment data, project description, area practice material, etc.) that the requestor considers relevant to the issue.

- 3.) If the decision of the Administrator is not favorable, an interested party may appeal directly to the Administrative Review Board (formerly the Wage Appeals Board). Write to:

Administrative Review Board  
U. S. Department of Labor  
200 Constitution Avenue, N. W.  
Washington, D. C. 20210

- 4.) All decisions by the Administrative Review Board are final.

END OF GENERAL DECISION

000421



## GENERAL SERVICES ADMINISTRATION

### 41 CFR Parts 301-4 and 302-2

[FTR Amendment 42]

RIN 3090-AF64

#### Federal Travel Regulation; Privately Owned Vehicle Mileage Reimbursement

AGENCY: Federal Supply Service, GSA.  
ACTION: Final rule.

**SUMMARY:** This final rule amends the Federal Travel Regulation (FTR) to implement provisions of the Treasury, Postal Service, and General Government Appropriations Act for Fiscal Year 1995 (Pub. L. 103-329, September 30, 1994). The Act eliminates the fixed statutory ceilings on mileage reimbursement rates for advantageous use of a privately owned vehicle (POV) on official business travel, and allows the Administrator of General Services to establish the rates based on cost investigations. This amendment is intended to provide equitable reimbursement to a Federal employee for advantageous use of a POV on official business travel by increasing the mileage reimbursement rates to reflect current costs per mile of operating a POV; and by increasing the mileage reimbursement rates for use of a POV in lieu of a Government-furnished vehicle (GFV) to reflect current costs to an agency of operating a GFV.

**DATES:** This final rule is effective January 1, 1995, and applies to travel performed on or after January 1, 1995.

**FOR FURTHER INFORMATION CONTACT:** Robert A. Clauson, General Services Administration, Transportation Management Division (FBX), Washington, DC 20406, telephone 703-305-5745.

**SUPPLEMENTARY INFORMATION:** This final rule amends the Federal Travel Regulation (FTR) to establish increased mileage reimbursement rates for use of a privately owned vehicle (POV) while performing official business travel.

Mileage reimbursement rates for advantageous use of a POV have been constrained by statute at 25 cents per mile for a privately owned automobile (established in June 1991), 45 cents per mile for a privately owned airplane (established in October 1980), and 20 cents per mile for a privately owned motorcycle (established in October 1980) even though cost studies have indicated that higher reimbursement

rates were necessary to adequately reimburse the cost of operating a POV.

Section 634 of the Treasury, Postal Service, and General Government Appropriations Act for Fiscal Year 1995 (Pub. L. 103-329, September 30, 1994) eliminated the fixed statutory caps and allows the Administrator of General Services to establish mileage reimbursement rates based on cost investigations which the General Services Administration (GSA) is required under 5 U.S.C. 5707(b)(1) to periodically conduct and report to Congress. Under the new law, the mileage reimbursement rate for advantageous use of a privately owned automobile may not exceed the Internal Revenue Service (IRS) business standard mileage rate in any year the IRS establishes such a single rate.

GSA has reported the results of its November 1994 cost investigation to Congress and indicated that the governing regulation would be revised to increase the mileage allowance for advantageous use of a privately owned automobile from 25 cents per mile to 30 cents per mile, for use of a privately owned airplane from 45 cents per mile to 88.5 cents per mile, and for use of a privately owned motorcycle from 20 cents per mile to 24.5 cents per mile. Additionally, based on updated data reflecting current costs to an agency of operating a GFV, GSA has increased the two-tiered reimbursement rates for use of a POV instead of a GFV from 18 cents to 23.5 cents per mile and from 9.5 cents to 10.5 cents per mile.

GSA has determined that this rule is not a significant regulatory action for the purposes of Executive Order 12866 of September 30, 1993. This final rule is not required to be published in the **FEDERAL REGISTER** for notice and comment. Therefore, the Regulatory Flexibility Act does not apply.

#### List of Subjects in 41 CFR Part 301-4

Government employees, Travel, Travel allowances, Travel and transportation expenses

#### List of Subjects in 41 CFR Part 302-2

Government employees, Relocation allowances and entitlements, Transfers

For the reasons set out in the preamble, 41 CFR parts 301-4 and 302-2 are amended to read as follows:

#### PART 301-4—REIMBURSEMENT FOR USE OF PRIVATELY OWNED CONVEYANCES

1. The authority citation for part 301-4 continues to read as follows:

Authority: 5 U.S.C. 5701-5709; E.O. 11609, 36 FR 13747, 3 CFR, 1971-1975 Comp., p. 586.

2. Section 301-4.2 is amended by revising paragraph (a); removing paragraph (b); redesignating paragraphs (c) and (d) as paragraphs (b) and (c) respectively; by removing the number "25" every place it appears in new paragraph (c), and adding in its place the number "30"; and by removing the phrase "paragraphs (d)(1) and (2)" in new paragraph (c)(3), and adding in its place the phrase "paragraphs (c) (1) and (2)", to read as follows:

#### § 301-4.2 When use of a privately owned conveyance is advantageous to the Government.

(a) *Authorized mileage reimbursement rates.* When the use of a privately owned conveyance is authorized or approved as advantageous to the Government for the performance of official travel, either within or outside the United States, as provided in § 301-2.2(d)(3) of this chapter, reimbursement to the traveler shall be at the mileage rates prescribed in this paragraph.

(1) For use of a privately owned automobile: 30 cents per mile.

(2) For use of a privately owned airplane: 88.5 cents per mile.

(3) For use of a privately owned motorcycle: 24.5 cents per mile.

#### § 301-4.4 [Amended]

3. Section 301-4.4 is amended by removing the number "18.0" wherever it appears in the section, and adding in its place the number "23.5"; and by removing the number "9.5" where it appears in paragraph (c), and adding in its place the number "10.5".

#### PART 302-2—ALLOWANCES FOR SUBSISTENCE AND TRANSPORTATION

4. The authority citation for part 302-2 continues to read as follows:

Authority: 5 U.S.C. 5721-5734; 20 U.S.C. 905(a); E.O. 11609, 36 FR 13747, 3 CFR, 1971-1975 Comp., p. 586.

#### § 302-2.3 [Amended]

5. Section 302-2.3 is amended by removing the reference "§ 301-4.2(a)(2)" where it appears in the introductory text of paragraph (c), and by adding in its place the reference "§ 301-4.2(a)(1)".

Dated: December 15, 1994.

Julia M. Stasch,

Acting Administrator of General Services.

[FR Doc. 94-31790 Filed 12-23-94; 8:45 am]

BILLING CODE 6820-24-F



**GENERAL SERVICES  
ADMINISTRATION****41 CFR Chapter 301****[FTR Amendment 41]****RIN 3090-AF55****Federal Travel Regulation; Maximum  
Per Diem Rates****AGENCY:** Federal Supply Service, GSA.  
**ACTION:** Final rule.

**SUMMARY:** An analysis of lodging and meal cost survey data reveals that the listing of maximum per diem rates for locations within the continental United States (CONUS) should be updated to provide for the reimbursement of Federal employees' expenses covered by

per diem. This final rule, among other things, increases/decreases the maximum lodging and meals and incidental expenses amounts in certain existing per diem localities, adds new per diem localities, and modifies the defined per diem area for Flagstaff and Grand Canyon, in the state of Arizona and Virginia Beach and Williamsburg, in the state of Virginia.

**DATES:** This final rule is effective on January 1, 1995, and applies for travel (including travel incident to a change of official station) performed on or after January 1, 1995.

**FOR FURTHER INFORMATION CONTACT:** Donna Cooke or Karen Kinsella, Transportation Management Division (FBX), Washington, DC 20406, telephone 703-305-5745.

**SUPPLEMENTARY INFORMATION:** The General Services Administration (GSA) has determined that this rule is not a significant regulatory action for the purposes of Executive Order 12866 of September 30, 1993. This final rule is not required to be published in the Federal Register for notice and comment. Therefore, the Regulatory Flexibility Act does not apply.

For the reasons set out in the preamble, under 5 U.S.C. 5701-5709, title 41, chapter 301 of the Code of Federal Regulations is amended by revising Appendix A to chapter 301 to read as follows:

**CHAPTER 301—TRAVEL  
ALLOWANCES****APPENDIX A TO CHAPTER 301—PRESCRIBED MAXIMUM PER DIEM RATES FOR CONUS**

The maximum rates listed below are prescribed under § 301-7.3(a) of this chapter for reimbursement of per diem expenses incurred during official travel within CONUS (the continental United States). The amount shown in column (a) is the maximum that will be reimbursed for lodging expenses including applicable taxes. The M&IE rate shown in column (b) is a fixed amount allowed for meals and incidental expenses covered by per diem. The per diem payable calculated in accordance with part 301-7 of this chapter for lodging expenses plus the M&IE rate may not exceed the maximum per diem rate shown in column (c). Seasonal rates apply during the periods indicated.

Per diem locality		Maximum lodging amount (a)	M&IE rate (b)	Maximum per diem rate (c)
Key city <sup>1</sup>	County and/or other defined location <sup>2, 3</sup>			
CONUS, Standard rate .....		\$40	\$26	
(Applies to all locations within CONUS not specifically listed below or encompassed by the boundary definition of a listed point. However, the standard CONUS rate applies to all locations within CONUS, including those defined below, for certain relocation subsistence allowances. See parts 302-2, 302-4, and 302-5 of this subtitle.)				
<b>ALABAMA</b>				
Anniston .....	Calhoun .....	42	26	
Birmingham .....	Jefferson .....	52	30	
Dothan .....	Houston .....	43	26	
Gulf Shores .....	Baldwin .....			
(April 1-September 30) .....		106	30	
(October 1-March 31) .....		52	30	
Huntsville .....	Madison .....	58	34	
Mobile .....	Mobile .....	55	34	
Montgomery .....	Montgomery .....	51	26	
Sheffield .....	Colbert .....	56	30	
<b>ARIZONA</b>				
Casa Grande .....	Pinal .....	50	30	
Chinle .....	Apache .....			
(April 1-October 31) .....		93	30	
(November 1-March 31) .....		54	30	
Flagstaff .....	All points in Coconino County not covered under Grand Canyon per diem area .....			
(April 1-October 31) .....		78	30	
(November 1-March 31) .....		58	30	
Grand Canyon .....	All points in the Grand Canyon National Park and Kaibab National Forest within Coconino County .....	104	30	
Kayenta .....	Navajo .....			
(May 1-October 14) .....		80	26	
(October 15-April 30) .....		55	26	
Phoenix/Scottsdale .....	Mancopa .....			
(December 1-April 30) .....		87	34	
(May 1-November 30) .....		61	34	
Prescott .....	Yavapai .....	50	30	
Sierra Vista .....	Cochise .....	46	30	
Tucson .....	Pima County; Davis-Monthan AFB .....			
(November 1-April 30) .....		62	30	
(May 1-October 31) .....		54	30	



# 010 | Overhead & Miscellaneous Data

1 GENERAL REQUIREMENTS

010 000   Overhead		CREW	DAILY OUTPUT	LABOR- HOURS	UNIT	1998 BARE COSTS				TOTAL INCL O&P
						MAT.	LABOR	EQUIP.	TOTAL	
048	0010 MAIN OFFICE EXPENSE Average for General Contractors	R010 -050								
	0020 As a percentage of their annual volume									
	0125 Annual volume under 1 million dollars					% Vol.				13.60%
	0145 Up to 2.5 million dollars									8%
	0150 Up to 4.0 million dollars									6.80%
	0200 Up to 7.0 million dollars									5.60%
	0250 Up to 10 million dollars									5.10%
0300 Over 10 million dollars								3.90%		
052	0010 MARK-UP For General Contractors for change	R010 -070								
	0100 of scope of job as bid									
	0200 Extra work, by subcontractors, add					%				10%
	0250 By General Contractor, add									15%
	0400 Omitted work, by subcontractors, deduct									5%
	0450 By General Contractor, deduct									7.50%
	0600 Overtime work, by subcontractors, add									15%
	0650 By General Contractor, add									10%
	1000 Installing contractors, on his own labor, minimum							49%		
1100 Maximum						105.40%				
054	0012 MATERIAL INDEX (Appendix) For 67 major U.S. and Canadian cities									
	0022 Minimum (Las Cruces, NM)				%	93.50%				
	0040 Average					100%				
	0061 Maximum (Anchorage, AK)					128.30%				
058	0010 OVERHEAD As percent of direct costs, minimum	R010 -050				%				5%
	0050 Average									12%
	0100 Maximum									30%
062	0010 OVERHEAD & PROFIT Allowance to add to items in this	R010 -070								
	0020 book that do not include Subs O&P, average					%				25%
	0100 Allowance to add to items in this book that									
	0110 do include Subs O&P, minimum					%				5%
	0150 Average									10%
	0200 Maximum									15%
	0300 Typical, by size of project, under \$100,000									30%
	0350 \$500,000 project									25%
	0400 \$2,000,000 project									20%
0450 Over \$10,000,000 project								15%		
064	0010 OVERTIME For early completion of projects or where	R010 -110								
	0020 labor shortages exist, add to usual labor, up to					Costs		100%		
068	0010 PERFORMANCE BOND For buildings, minimum	R010 -080				Job				.60%
	0100 Maximum					"				2.50%
070	0010 PERMITS Rule of thumb, most cities, minimum					Job				.50%
	0100 Maximum					"				2%
082	0010 SMALL TOOLS As % of contractor's work, minimum	R010 -050				Total				.50%
	0100 Maximum					"				2%
086	0010 TAXES Sales tax, State, average	R010 -090				%	4.78%			
	0050 Maximum						7.25%			
	0200 Social Security, on first \$65,400 of wages	R010 -100						7.65%		
	0301 Unemployment, CA, combined Federal and State, minimum						2.10%			
	0350 Average						4%			
	0400 Maximum						9.30%			



# TRACTORS & EARTHMOVING

## WHEEL LOADER GENERAL PURPOSE BUCKETS

(In lieu of standard bucket.)

Capacity	Monthly \$	Weekly \$	Daily \$	Hourly \$	Estimated Operating Cost \$/Hr.
1 CY	62.00	17.00	4.00	.60	.35
1-1/4 CY	110.00	31.00	8.00	1.00	.40
1-1/2 CY	130.00	36.00	9.00	1.00	.45
1-3/4 CY	170.00	48.00	12.00	2.00	.50
2 CY	190.00	53.00	13.00	2.00	.50
2-1/2 CY	245.00	69.00	17.00	3.00	.60
3+ CY	395.00	110.00	28.00	4.00	.75

## WHEEL LOADER MULTI-PURPOSE BUCKETS

Capacity	Monthly \$	Weekly \$	Daily \$	Hourly \$	Estimated Operating Cost \$/Hr.
1 CY	550.00	155.00	39.00	6.00	.95
1-1/4 CY	625.00	175.00	44.00	7.00	1.05
1-1/2 CY	580.00	160.00	40.00	6.00	1.00
1-3/4 CY	650.00	180.00	45.00	7.00	1.05
2 CY	690.00	195.00	49.00	7.00	1.10
2-1/2 CY	730.00	205.00	51.00	8.00	1.15
3 & Over CY	840.00	235.00	59.00	9.00	1.30

## WHEEL LOADER SIDE DUMP BUCKETS

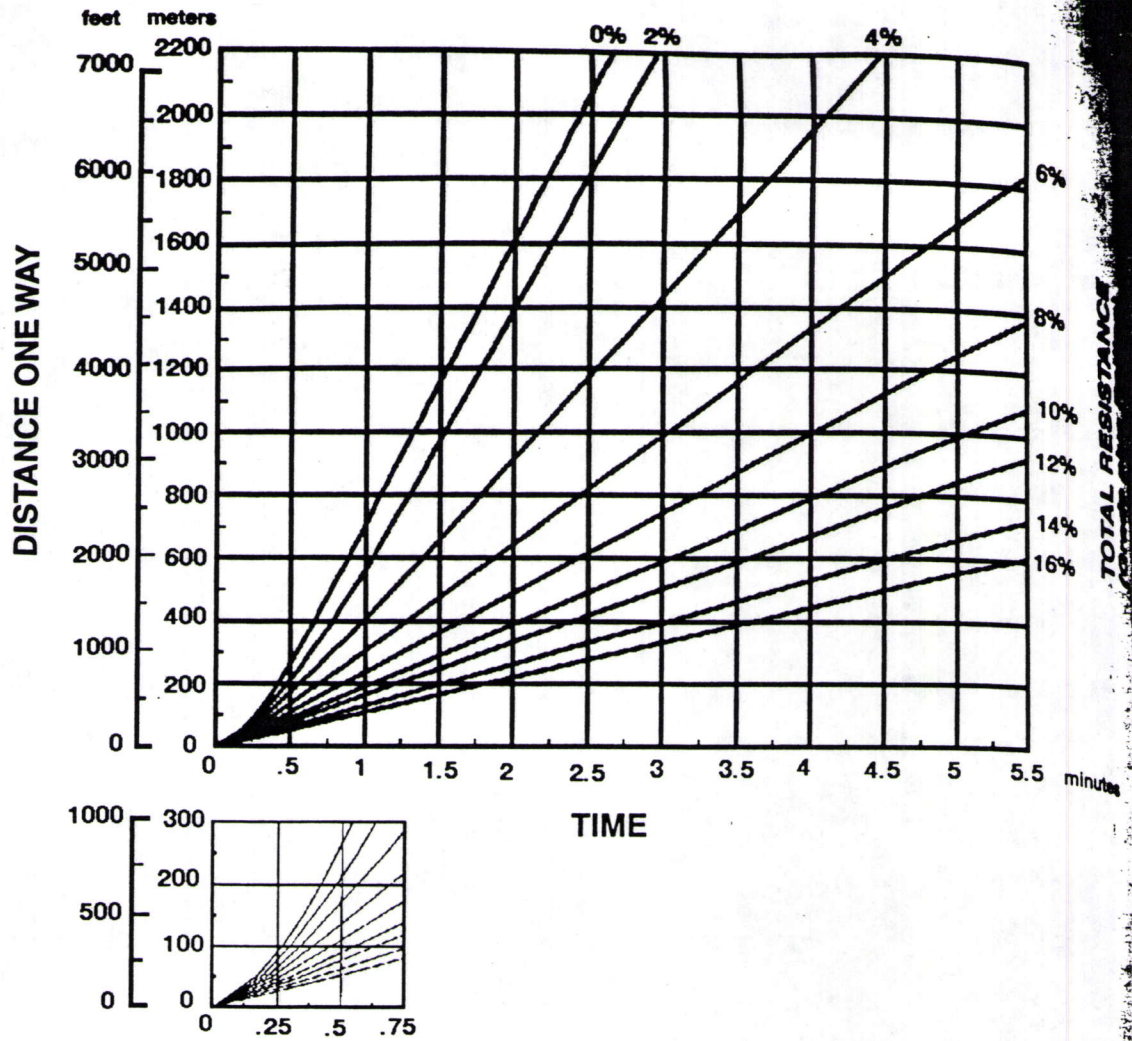
(In lieu of standard bucket.)

Capacity	Monthly \$	Weekly \$	Daily \$	Hourly \$	Estimated Operating Cost \$/Hr.
1-1/2 CY	480.00	135.00	34.00	5.00	.85
2 CY	740.00	205.00	51.00	8.00	1.15

## SINGLE ENGINE CONVENTIONAL SCRAPERS

Model (Yr.Disc.)	Scraper Capacity	Tractor HP	Operator Protection	Monthly \$	Weekly \$	Daily \$	Hourly \$	Estimated Operating Cost \$/Hr.
<b>DIESEL POWERED</b>								
<b>CATERPILLAR</b>								
611	11.0-15.0 CY	262.2	EROPS	9,770.00	2,735.00	685.00	105.00	39.40
611	11.0-15.0 CY	262.2	ROPS	9,650.00	2,700.00	675.00	100.00	39.10
621F	14.00-20.00 CY	327.0	EROPS	12,275.00	3,435.00	860.00	130.00	48.35
621F	14.00-20.00 CY	327.0	ROPS	12,155.00	3,405.00	850.00	130.00	48.05
631E SERIES II	21.00-31.00 CY	450.0	EROPS	19,075.00	5,340.00	1,335.00	200.00	72.35
631E SERIES II	21.00-31.00 CY	450.0	ROPS	18,980.00	5,315.00	1,330.00	200.00	72.10
651E	32.00-44.00 CY	550.0	EROPS	24,345.00	6,815.00	1,705.00	255.00	89.90
<b>TEREX</b>								
S-24C (1999)	24-34 CY	480.0	EROPS	15,265.00	4,275.00	1,070.00	160.00	68.20
S-24C (1999)	24-34 CY	480.0	ROPS	15,210.00	4,260.00	1,065.00	160.00	68.10

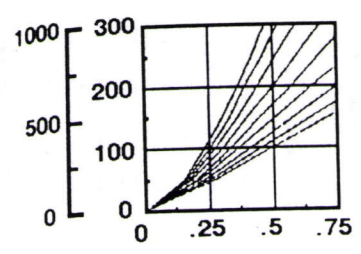
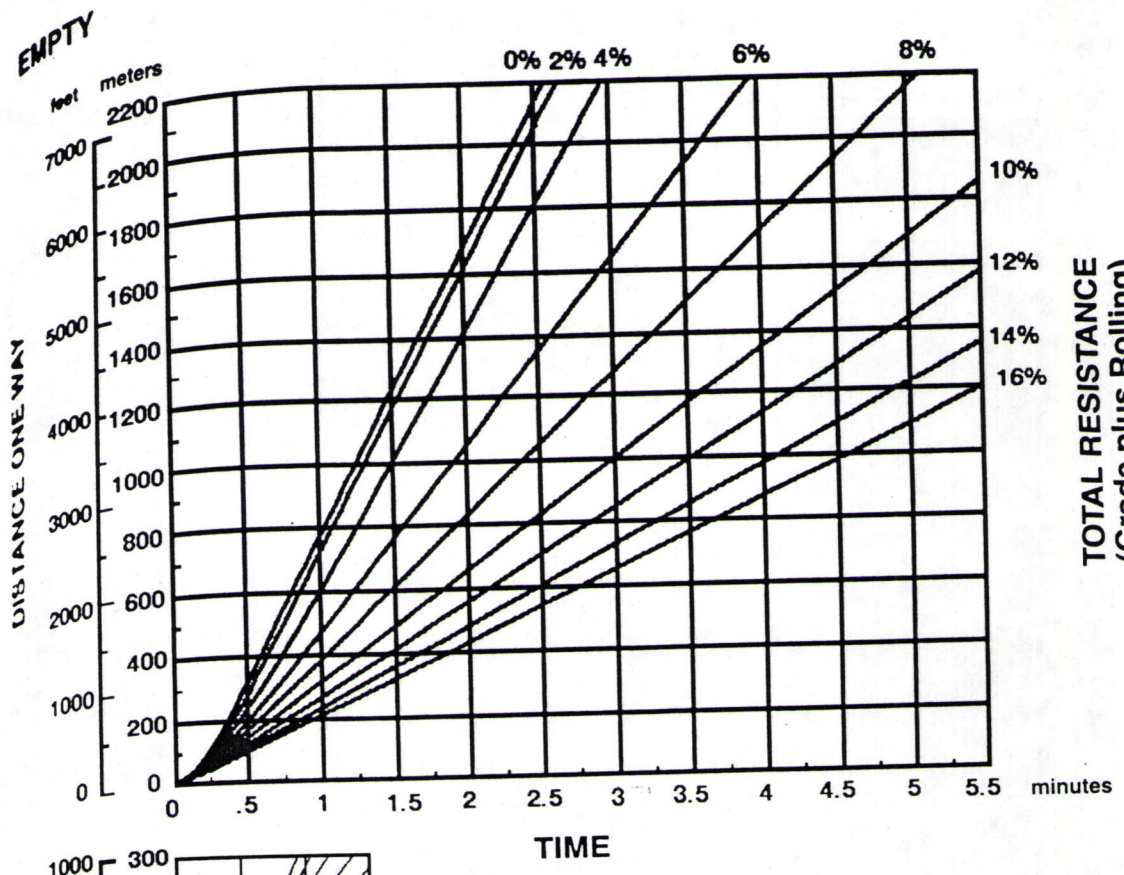
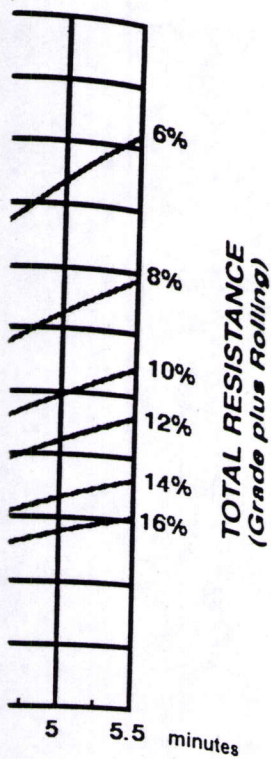




Empty weight: 45 980 kg (101,370 lb)  
 Payload: 34 020 kg (75,000 lb)



loaded



Empty weight: 45 980 kg (101,370 lb)

101,370 lb)  
lb)

000430



USED ON  
VS

ZONE C Severe
Heavy rock ripping. Pushloading and dozing in hard rock. Work on rock surfaces. Continuous high impact conditions.
8,000 Hr 25,000 Hr 30,000 Hr
Pulling layer scrapers, used in construction applications, ripping, dozing.
N/A 8,000 Hr 10,000 Hr
Maintenance of hard packed roads with embedded rock. Heavy fill spreading. Ripping-scarifying of asphalt or concrete. Continuous high load factor. High impact.
12,000 Hr 30,000 Hr
Continuous digging in rock/natural bed clay, high impact, using hammer, working in forests or quarries.
6,000 Hr 8,000 Hr
Continuous trenching or truck loading in rock or shot rock soils. Large amount of travel over rough ground. Machine continuously working on rock floor with constant high load factor and high impact.
10,000 Hr 10,000 Hr 15,000 Hr 40,000 Hr
Continuous loading in poorly-shot rock, virgin or lightly-blasted tight banks, e.g., shales, cemented gravels, caliches, etc. Adverse underfoot conditions: rough floors; high impact loading on undercarriage.
15,000 Hr 40,000 Hr

	ZONE A Moderate	ZONE B Average	ZONE C Severe
<b>FELLER BUNCHERS</b>	Continuous felling and stacking in good underfoot conditions. Flat ground uniform trees below 305 mm (12 inches).	Continuous cycling in good underfoot conditions. Rolling terrain, some trees up to 508 mm (20 inches) or some hardwoods.	Continuous cycling in steep terrain over stumps and fallen trees. Most trees 508 mm (20 inches) or larger hardwoods.
	18,000 Hr	15,000 Hr	10,000 Hr
<b>BACKHOE LOADERS</b>	Light duty utility applications in light to medium soil. Trenching depths less 1.83 m (6 ft.)	Utility applications in medium to heavy soil. Occasional use of constant flow implements. Dig depths to 3.05 m (10 ft.)	Production applications or digging in rock. Regular use of constant flow implements. Dig depths over 3.05 m (10 ft.)
	12,000 Hr	10,000 Hr	5,000 Hr
<b>SKIDDERS</b>	Intermittent skidding for short distances, no decking. Good underfoot conditions: level terrain, dry floor, few if any stumps.	Continuous turning, steady skidding for medium distances with moderate decking. Good underfooting: dry floor with few stumps and gradual rolling terrain.	Continuous turning, steady skidding for long distances with frequent decking. Poor underfoot conditions: wet floor, steep slopes and numerous stumps.
Wheel Track	10,000 Hr 12,000 Hr	8,000 Hr 10,000 Hr	7,200 Hr 8,000 Hr
<b>PIPELAYERS</b>	Little or no use in mud, water or on rock. Use on level, regular surfaces.	Typical pipelayer use in operating conditions ranging from very good to severe.	Continuous use in deep mud or water or on rock surfaces.
561M-572R 583R-589	20,000 Hr 25,000 Hr	15,000 Hr 20,000 Hr	10,000 Hr 15,000 Hr
<b>WHEEL TRACTOR-SCRAPERS</b>	Level or favorable hauls on good haul roads. No impact. Easy-loading materials.	Varying loading and haul road conditions. Long and short hauls. Adverse and favorable grades. Some impact. Typical road-building use on a variety of jobs.	High impact condition, such as loading ripped rock. Overloading. Continuous high total resistance conditions. Rough haul roads.
513C Series II, 611, 615C Series II 521F-627F, 631E-657E	12,000 Hr 22,000 Hr	10,000 Hr 17,000 Hr	8,000 Hr 12,000 Hr
<b>CONSTRUCTION &amp; MINING TRUCKS &amp; TRACTORS</b>	Continuous operation at an average gross weight less than recommended. Excellent haul roads. No overloading, low load factor. (See Hourly Fuel Consumption section for definition).	Continuous operation at an average gross weight approaching recommended. Minimal overloading, good haul roads, moderate load factor. (See Hourly Fuel Consumption section for definition).	Continuous operation at or above maximum recommended gross weight. Overloading, poor haul roads, high load factor. (See Hourly Fuel Consumption section for definition). Note — Continual loading beyond recommended maximum gross weight will further reduce Zone C hours.
769D-777D 784C-797	50,000 Hr 60,000 Hr	40,000 Hr 50,000 Hr	30,000 Hr 40,000 Hr

000431

## **APPENDIX 15**

(Production Rate of Wheeled Tractor-Scraper)



623F		633E Series II	
272 kW	365 hp	335/365 kW	450/490 hp
5 305 kg	77,830 lb	51 110 kg	112,400 lb
3.8 m³	18 yd³	17.7 m³	23.3 yd³
7.6 m³	23 yd³	26 m³	34 yd³
10 039 kg	55,200 lb	37 200 kg	82,000 lb
65%		64%	
35%		30%	
52%		51%	
48%		49%	
3406CTA		3406TA	
1900		2000	
4.6 L	893 in³	18 L	1088 in³
1 km/h	30 mph	53 km/h	33 mph
9 m	35'8"	13.16 m	43'2"
33.25R29**E2		37.25R35**E2	
33.25R29**E2		37.25R35**E2	
5 m	11'6"	3.5 m	11'6"
10 mm	13"	431 mm	17"
10 mm	20"	610 mm	24"
15		14	
3 m	5'0"	1.22 m	4'
1 mm	15"	578 mm	22 7/8"
6 L	160 U.S. gal	814 L	215 U.S. gal
8 m	12'1"	4.24 m	13'11"
8 m	26'2"	9.02 m	29'7"
11 m	43'4"	14.8 m	48'7"
5 m	11'8"	3.96 m	12'10"
—		3.64 m	11'10"
1 m	7'2"	2.5 m	8'2"
1 m	7'3"	2.5 m	8'2"

**6000SL**  
 Standard Power Tractor  
 Standard Operating Weight  
 Empty Weight  
 Power Capacity (Heaped)  
 Standard Load  
 Standard Operating Weight  
 (Loaded)  
 Auger ATTACHMENT  
 Auger Diameter  
 Auger RPM  
 Auger Power  
 Hydraulic Flow  
 Hydraulic Flow  
 System Pressure  
 System Control

Weight includes standard machine, coolant, lubricants, full fuel tank and operator.

The auger scraper is a self-loading system that offers an alternative to conventional, push-pull or elevating scrapers. An independent hydrostatic system powers the auger which is located near the center of the bowl. The rotating auger lifts and evenly distributes over 50% of the material that flows over the scraper cutting edge. This action reduces the cutting edge resistance allowing the wheel tractor-scraper to continue moving through the cut and quickly obtain full rated loads.

- Advantages:**
- Load in equal or less time
  - Requires shorter cut distance
  - Complete material ejection
  - Auger ejector pushes material
  - Auger ejector reduces dust problems
  - No material
  - Increased tire life

- Broader material appetite
- Better material retention on haul road (closed apron instead of open elevator)

621F		631E Series II		651E	
272 kW	365 hp	335/365 kW	450/490 hp	410/452 kW	550/605 hp
37 760 kg	83,250 lb	45 980 kg	101,370 lb	66 575 kg	146,770 lb
15.96 m³	21 yd³	23.7 m³	31 yd³	33.6 m³	44 yd³
21 775 kg	48,000 lb	34 020 kg	75,000 lb	47 175 kg	104,000 lb
57 950 kg	127,750 lb	80 000 kg	176,370 lb	113 750 kg	250,770 lb
1320 mm	4'4"	1524 mm	5'0"	1676 mm	5'6"
Variable 55 to 35 RPM		Variable 55 to 35 RPM		Variable 55 to 35 RPM	
149 kW	200 hp	201 kW	270 hp	354 kW	475 hp
273 L/min	72 gpm	378 L/min	100 gpm	549 L/min	145 gpm
—	—	—	—	132 L/min	35 gpm
41 370 kPa	6000 psi	37 895 kPa	5500 psi	41 370 kPa	5700 psi
electronic		electronic		electronic	

000433



Total Resistance

4%

*Cycle Time —*  
= load\* + haul + maneuver & spread\* + return  
= 0.6 + 1.4 + 0.7 + 1.0  
= 3.7 min.  
\*For fixed time (load, maneuver and spread)  
see the table below.  
When cycle time and payload are known, pro-  
ductivity can be calculated. For a more complex  
example see the Earthmoving Section.

### TYPICAL FIXED TIMES FOR SCRAPERS

(Times may vary depending on job conditions)

Model	Loaded By	Load Time (Min.)	Maneuver and Spread or Maneuver and Dump (Min.)
613C Series II	Self	0.9	0.7
615C Series II	Self	0.9	0.7
623F	Self	0.9	0.7
633E Series II	One D6R	0.5	0.7
611	One D8R	0.5	0.7
621F	One D8R	0.5	0.6
627F	One D9R	0.4	0.7
621F	One D9R	0.4	0.6
627F	Self	0.9*	0.6
627F/PP	One D9R	0.6	0.7
631E Series II	One D9R	0.6	0.6
637E Series II	One D10R	0.5	0.7
631E Series II	One D10R	0.5	0.6
637E Series II	Self	1.0*	0.6
637E/PP Series II	One D11R	0.6	0.7
651E	One D11R	0.6	0.6
657E	Push Pull	1.1*	0.6
	Self		
621F	Auger	0.9	0.7
627F	Auger	0.7	0.7
631E Series II	Auger	0.9	0.7
637E Series II	Auger	0.8	0.7
651E	Auger	1.3	0.7
657E	Auger	1.0	0.7

\*Load time per pair, including transfer time.

**NOTE:** Empty Weights shown on the Wheel Tractor-Scraper charts includes ROPS Canopy. The travel times will remain within acceptable limits when applied to a non-ROPS equipped machine. When calculating TMPH loadings any additional weight must be considered in establishing mean tire loads.

### USE OF RETARDER CURVES

The following explanation applies to retarder curves for Wheel Tractor-Scrapers and Articulated Trucks.

The speed that can be maintained (without use of service brake) when the machine is descending a grade with retarder fully on can be determined from the retarder curves in this section if gross machine weight and total effective grade are known.

**Total Effective Grade (or Total Resistance)** is grade assistance *minus* rolling resistance.

10 kg/metric ton (20 lb/U.S. ton) = 1% adverse grade.

#### Example

15% favorable grade with 5% rolling resistance. Find Total Effective Grade.

Total Effective Grade = 15% Grade Assistance — 5%

Rolling Resistance = 10% Total Effective Grade Assistance.

#### Example problem:

A 651E with an estimated payload of 47 175 kg (104,000 lb) descends a 10% total effective grade. Find constant speed and gear range with maximum retarder effort. Find travel time if the slope is 610 m (2000 ft) long.

Empty Weight + Payload = Gross Weight  
= 60 950 kg + 47 175 kg = 108 125 kg  
(134,370 lb + 104,000 lb = 238,370 lb)

000434



# 020 | Subsurface Investigation & Demolition

2 SITE WORK

020 550   Site Demolition		CREW	DAILY OUTPUT	LABOR-HOURS	UNIT	1998 BARE COSTS				TOTAL	
						MAT.	LABOR	EQUIP.	TOTAL	INCL O&P	
554	2200	Reinforced	B-38	24	1.667	C.Y.		40	41.50	81.50	108
	2300	With hand held air equipment, bituminous, to 6" thick	B-39	1,900	.025	S.F.		.56	.09	.65	.98
	2320	Concrete to 6" thick, no reinforcing		1,200	.040			.89	.14	1.03	1.56
	2340	Mesh reinforced		1,400	.034			.76	.12	.88	1.34
	2360	Rod reinforced		765	.063			1.40	.23	1.63	2.44
	2400	Curbs, concrete, plain	B-6	360	.067	L.F.		1.54	.59	2.13	3.03
	2500	Reinforced		275	.087			2.01	.78	2.79	3.98
	2600	Granite		360	.067			1.54	.59	2.13	3.03
	2700	Bituminous		528	.045			1.05	.40	1.45	2.08
	2900	Pipe removal, sewer/water, no excavation, 12" diameter		175	.137			3.16	1.22	4.38	6.25
	2930	15" diameter		150	.160			3.68	1.43	5.11	7.25
	2960	24" diameter		120	.200			4.61	1.78	6.39	9.10
	3000	36" diameter		90	.267			6.15	2.38	8.53	12.15
	3200	Steel, welded connections, 4" diameter		160	.150			3.45	1.34	4.79	6.80
	3300	10" diameter		80	.300			6.90	2.67	9.57	13.70
	3500	Railroad track removal, ties and track	B-13	330	.170			3.90	2.38	6.28	8.65
	3600	Ballast	B-14	500	.096	C.Y.		2.14	.43	2.57	3.82
	3700	Remove and re-install, ties & track using new bolts & spikes		50	.960	L.F.		21.50	4.27	25.77	38
	3800	Turnouts using new bolts and spikes		1	.48	Ea.		1,075	214	1,289	1,900
	4000	Sidewalk removal, bituminous, 2-1/2" thick	B-6	325	.074	S.Y.		1.70	.66	2.36	3.36
	4050	Brick, set in mortar		185	.130			2.99	1.16	4.15	5.90
	4100	Concrete, plain, 4"		160	.150			3.45	1.34	4.79	6.80
	4200	Mesh reinforced		150	.160			3.68	1.43	5.11	7.25
	5000	Slab on grade removal, plain	B-5	45	1.244	C.Y.		29	22.50	51.50	69.50
	5100	Mesh reinforced		33	1.697			39.50	30.50	70	94.50
	5200	Rod reinforced		25	2.240			52	40.50	92.50	126
	5500	For congested sites or small quantities, add up to								200%	200%
5550	For disposal on site, add	B-11A	232	.069			1.68	3.59	5.27	6.55	
5600	To 5 miles, add	B-34D	76	.105			2.56	7.20	9.76	11.80	
020 600   Building Demolition											
604	0010	BUILDING DEMOLITION Large urban projects, incl. 20 Mi. haul									
	0012	Excludes dump fee, C.F. is volume of building standing, steel	B-8	21,500	.003	C.F.		.07	.10	.17	.22
	0050	Concrete		15,300	.004			.10	.15	.25	.32
	0080	Masonry		20,100	.003			.08	.11	.19	.24
	0100	Mixture of types, average		20,100	.003			.08	.11	.19	.24
	0500	Small bldgs, or single bldgs, no salvage included, steel	B-3	14,800	.003			.08	.11	.19	.25
	0600	Concrete		11,300	.004			.10	.15	.25	.32
	0650	Masonry		14,800	.003			.08	.11	.19	.25
	0700	Wood		14,800	.003			.08	.11	.19	.25
	1000	Single family, one story house, wood, minimum				Ea.				2,300	2,700
	1020	Maximum								4,000	4,800
	1200	Two family, two story house, wood, minimum								3,000	3,600
	1220	Maximum								5,800	7,000
	1300	Three family, three story house, wood, minimum								4,000	4,800
1320	Maximum								7,000	8,400	
608	0010	DISPOSAL ONLY Urban buildings with salvage value allowed									
	0020	Including loading and 5 mile haul to dump									
	0200	Steel frame	B-3	430	.112	C.Y.		2.63	3.96	6.59	8.40
	0300	Concrete frame		365	.132			3.10	4.66	7.76	9.95
	0400	Masonry construction		445	.108			2.54	3.82	6.36	8.15
0500	Wood frame		247	.194			4.58	6.90	11.48	14.70	
612	0010	DUMP CHARGES Typical urban city, tipping fees only									
	0100	Building construction materials				Ton					60



# 020 | Subsurface Investigation & Demolition

## 020 700 | Selective Demolition

	CREW	DAILY OUTPUT	LABOR-HOURS	UNIT	1950 TAKE COSTS				TOTAL INCL O&P
					MAT.	LABOR	EQUIP.	TOTAL	
On metal lath	1 Clab	300	.027	S.F.		.56		.56	.88
Plywood, one side	B-1	1,500	.016			.35		.35	.54
Terra cotta block and plaster, to 6" thick	"	175	.137	↓		2.96		2.96	4.66
Toilet partitions, slate or marble	1 Clab	5	1.600	Ea.		33.50		33.50	52.50
Hollow metal	"	8	1	"		21		21	33
<b>WINDOW DEMOLITION</b>									
Aluminum, including trim, to 12 S.F.	1 Clab	16	.500	Ea.		10.45		10.45	16.50
To 25 S.F.		11	.727			15.20		15.20	24
To 50 S.F.		5	1.600			33.50		33.50	52.50
Storm windows, to 12 S.F.		27	.296			6.20		6.20	9.75
To 25 S.F.		21	.381			7.95		7.95	12.55
To 50 S.F.		16	.500	↓		10.45		10.45	16.50
Glass, minimum		200	.040	S.F.		.84		.84	1.32
Maximum		150	.053	"		1.11		1.11	1.76
Steel, including trim, to 12 S.F.		13	.615	Ea.		12.85		12.85	20.50
To 25 S.F.		9	.889			18.60		18.60	29.50
To 50 S.F.		4	2			42		42	66
Wood, including trim, to 12 S.F.		22	.364			7.60		7.60	12
To 25 S.F.		18	.444			9.30		9.30	14.65
To 50 S.F.	↓	13	.615			12.85		12.85	20.50
Remove and reset window, minimum	1 Carp	6	1.333			34		34	54
Average		4	2	↓		51		51	80.50
Maximum	↓	2	4	↓		102		102	161

## 020 750 | Concrete Removal

<b>FOOTINGS AND FOUNDATIONS DEMOLITION</b>									
Floors, concrete slab on grade,									
4" thick, plain concrete	B-9C	500	.080	S.F.		1.70	.35	2.05	3.07
Reinforced, wire mesh	↓	470	.085			1.81	.37	2.18	3.27
Rods		400	.100			2.13	.43	2.56	3.84
6" thick, plain concrete		375	.107			2.27	.46	2.73	4.09
Reinforced, wire mesh	↓	340	.118			2.51	.51	3.02	4.51
Rods	↓	300	.133	↓		2.84	.58	3.42	5.10
Footings, concrete, 1' thick, 2' wide	B-5	300	.187	L.F.		4.33	3.37	7.70	10.45
1'-6" thick, 2' wide	↓	250	.224			5.20	4.05	9.25	12.55
3' wide	↓	200	.280			6.50	5.05	11.55	15.65
2' thick, 3' wide	↓	175	.320			7.40	5.80	13.20	17.90
Average reinforcing, add				↓				10%	10%
Heavy reinforcing, add				↓				20%	20%
Walls, block, 4" thick	A-1	200	.040	S.F.		.84	.34	1.18	1.69
6" thick	↓	190	.042			.88	.35	1.23	1.78
8" thick	↓	180	.044			.93	.37	1.30	1.87
12" thick	↓	175	.046			.96	.38	1.34	1.93
For horizontal reinforcing, add								10%	10%
For vertical reinforcing, add								20%	20%
Concrete, plain concrete, 6" thick	B-9	160	.250			5.30	1.08	6.38	9.60
8" thick	↓	140	.286			6.10	1.24	7.34	10.95
10" thick	↓	120	.333			7.10	1.45	8.55	12.80
12" thick	↓	100	.400			8.50	1.74	10.24	15.35
For average reinforcing, add								10%	10%
For heavy reinforcing, add								20%	20%
For congested sites or small quantities, add up to				↓				200%	200%
Add for disposal, on site	B-11A	232	.069	C.Y.		1.68	3.59	5.27	6.55
To five miles	B-30	220	.109			2.79	7.15	9.94	12.10

SITE WORK 2



# 020 | Subsurface Investigation & Demolition

## 020 800 | Haz. Mat'l Abatement

### DECONTAMINATION CONTAINMENT AREA DEMOLITION and clean-up

0100	Spray exposed substrate with surfactant (bridging)								
0100	Flat surfaces	A-9	6,000	.011	S.F.	.30	.33	.63	.86
0200	Irregular surfaces		4,000	.016	*	.35	.49	.84	1.18
0250	Pipes, beams, and columns		2,000	.032	L.F.	.60	.98	1.58	2.24
0300	Spray encapsulate polyethylene sheeting		8,000	.008	S.F.	.25	.25	.50	.68
1000	Roll down polyethylene sheeting		8,000	.008	*		.25	.25	.40
1100	Bag polyethylene sheeting		400	.160	Ea.	.70	4.91	5.61	8.65
1500	Fine clean exposed substrate, with nylon brush		2,400	.027	S.F.		.82	.82	1.32
2000	Wet wipe substrate		4,800	.013			.41	.41	.66
2500	Vacuum surfaces, fine brush	▼	6,400	.010	▼		.31	.31	.49
2600	Structural demolition								
3000	Wood stud walls	A-9	2,800	.023	S.F.		.70	.70	1.13
3100	Window manifolds, not incl. window replacement		4,200	.015			.47	.47	.75
3500	Plywood carpet protection	▼	2,000	.032	▼		.98	.98	1.58
3600	Remove custom decontamination facility	A-10A	8	3	Ea.	15.65	92.50	108.15	166
4000	Remove portable decontamination facility	3 Asbe	12	2	*	11.50	61	72.50	111
4100	HEPA vacuum, shampoo carpeting	A-9	4,800	.013	S.F.	.05	.41	.46	.72
5000	Final cleaning of protected surfaces	A-10A	8,000	.003	*		.09	.09	.15

### ENCAPSULATION WITH SEALANTS

0100	Ceilings and walls, minimum	A-9	21,000	.003	S.F.	.25	.09	.34	.43
0100	Maximum		10,600	.006		.35	.19	.54	.69
0200	Columns and beams, minimum		13,300	.005		.25	.15	.40	.52
0210	Maximum		5,325	.012	▼	.35	.37	.72	.98
0300	Pipes to 12" diameter including minor repairs, minimum		800	.080	L.F.	.35	2.45	2.80	4.35
0310	Maximum	▼	400	.160	*	1	4.91	5.91	9

### REMOVAL OF UNDERGROUND STORAGE TANKS

0010	Petroleum storage tanks, non-leaking								
0100	Excavate & load onto trailer								
0110	3000 gal. to 5000 gal. tank	B-14	4	12	Ea		268	53.50	321.50
0120	6000 gal to 8000 gal tank	B-3A	3	13.333	▼		297	235	532
0130	9000 gal to 12000 gal tank	*	2	20	▼		445	355	800
0190	Known leaking tank add				%				100%
0200	Remove sludge, water and remaining product from bottom of tank with vacuum truck								
0300	3000 gal to 5000 gal tank	A-13	5	1.600	Ea		43.50	102	145.50
0310	6000 gal to 8000 gal tank	▼	4	2	▼		54.50	128	182.50
0320	9000 gal to 12000 gal tank	▼	3	2.667	▼		73	171	244
0390	Dispose of sludge off-site, average				Gal				3.50
0400	Insert solid carbon dioxide "dry ice" to produce inert gas								
0401	For cleaning & transporting tanks (1.5 lbs./100 gal. capacity)	1 Clab	500	.016	Lb	1.10	.33	1.43	1.74
1020	Haul tank to certified salvage dump, 100 miles round trip								
1023	3000 gal. to 5000 gal. tank				Ea			525	600
1026	6000 gal. to 8000 gal. tank				▼			625	690
1029	9,000 gal. to 12,000 gal. tank				▼			850	935
1100	Disposal of contaminated soil to landfill								
1110	Minimum				C.Y.				110
1111	Maximum				*				310
1120	Disposal of contaminated soil to bituminous concrete batch plant								
1121	Minimum				C.Y.				50
1131	Maximum				*				100
2010	Decontamination of soil on site incl poly tarp on top/bottom								
2011	Soil containment berm, and chemical treatment								

000438



# 022 | Earthwork

## 022 300 | Pavement Base

	CREW	DAILY OUTPUT	LABOR HOURS	UNIT	1998 BARE COSTS				TOTAL INCL O&P	
					MAT.	LABOR	EQUIP.	TOTAL		
0010 BASE Prepare and roll sub-base, small areas to 2500 S.Y.	B-32A	1,500	.016	S.Y.		.41	.64	1.05	1.34	304
0100 Large areas over 2500 S.Y.	B-32	3,700	.009	"		.23	.44	.67	.83	
0010 BASE COURSE For roadways and large paved areas	B-36B	4,600	.014	S.Y.	5.40	.35	.69	6.44	7.25	308
0050 Crushed 3/4" stone base, compacted, 3" deep		4,500	.014		7.70	.36	.71	8.77	9.80	
0100 6" deep		3,300	.019		11.55	.49	.97	13.01	14.50	
0100 9" deep		2,700	.024		15.40	.59	1.18	17.17	19.15	
0200 12" deep		6,000	.011		5.05	.27	.53	5.85	6.60	
0300 Crushed 1-1/2" stone base, compacted to 4" deep		4,500	.014		7.70	.36	.71	8.77	9.80	
0301 6" deep		3,500	.018		10.30	.46	.91	11.67	13.05	
0302 8" deep		2,000	.032		15.35	.80	1.60	17.75	19.90	
0303 12" deep										
0304 Bank run gravel, spread and compacted	B-32	6,000	.005	S.Y.	2.45	.14	.27	2.86	3.21	
0350 6" deep		4,900	.007		3.68	.17	.33	4.18	4.67	
0370 9" deep		3,600	.009		4.90	.23	.45	5.58	6.25	
0390 12" deep	B-45	6,000	.003	Gal.	1.45	.07	.12	1.64	1.84	
0400 Liquid application to gravel base, asphalt emulsion		6,000	.003	"	1.71	.07	.12	1.90	2.12	
0500 Prime and seal, cut back asphalt		6,000	.003	S.Y.	2.90	.07	.12	3.09	3.43	
0600 Macadam penetration crushed stone, 2 gal. per S.Y., 4" thick		4,000	.004		4.35	.10	.18	4.63	5.15	
0700 6" thick, 3 gal. per S.Y.		3,000	.005		5.80	.14	.24	6.18	6.85	
0800 8" thick, 4 gal. per S.Y.	B-6	10,000	.002		1.25	.06	.02	1.33	1.49	
0900 Stabilization fabric, polypropylene, 6 oz./S.Y.						50%	50%			
0920 For small and irregular areas, add										

## 022 400 | Soil Stabilization

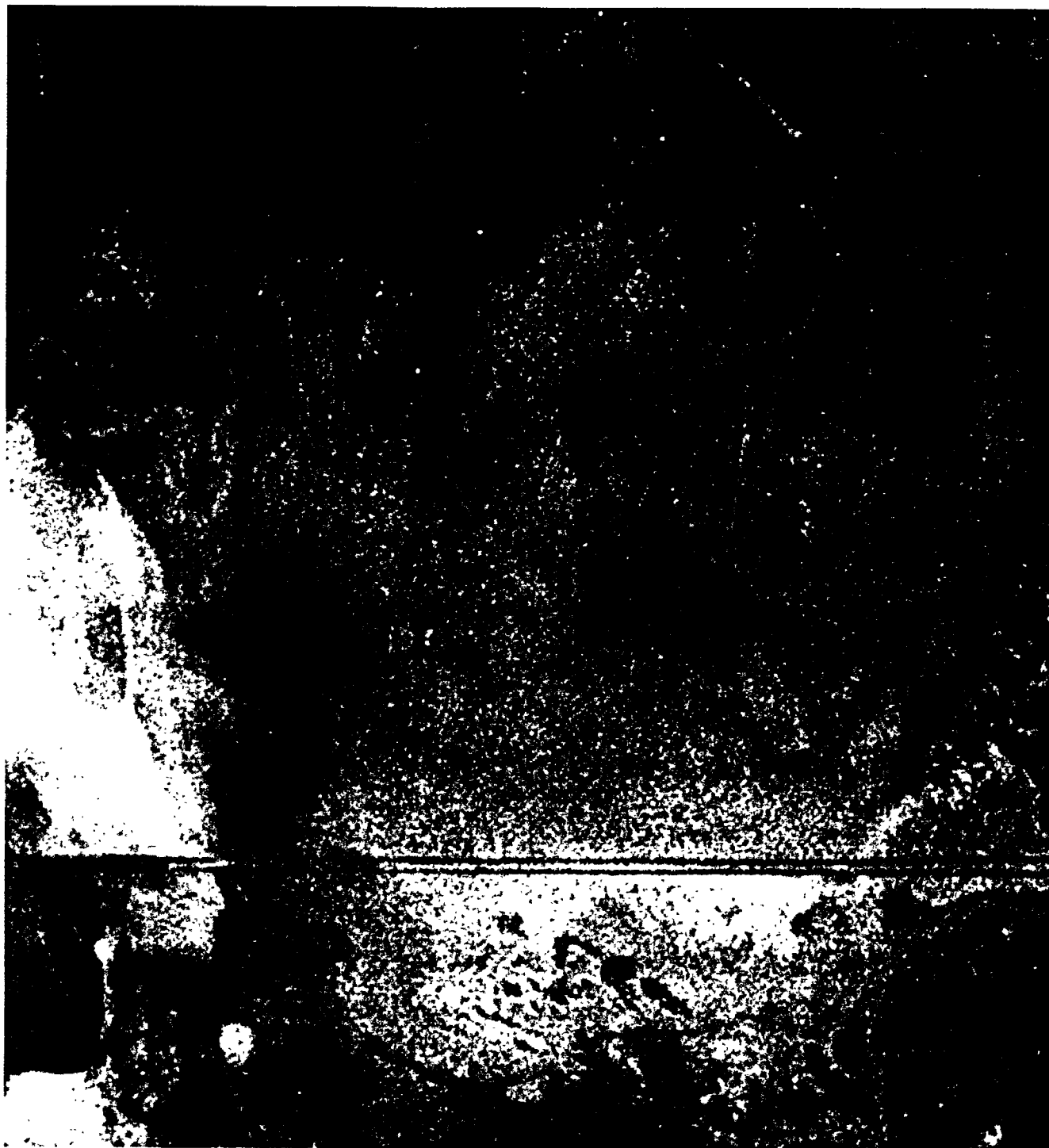
0010 GROUTING, PRESSURE Cement and sand, 1:1 mix, minimum	B-61	124	.323	Bag	8.25	7.30	2.84	18.39	23.50	408
0100 Maximum		51	.784	"	8.25	17.70	6.90	32.85	44	
0200 Cement and sand, 1:1 mix, minimum		250	.160	C.F.	16.55	3.61	1.41	21.57	25.50	
0300 Maximum		100	.400		25	9.05	3.52	37.57	45.50	
0400 Epoxy cement grout, minimum		137	.292		100	6.60	2.57	109.17	123	
0500 Maximum		57	.702		100	15.85	6.20	122.05	141	
0600 Structural epoxy grout				Gal.	45			45	49.50	
0700 Alternate pricing method: (Add for materials)										
0710 5 person crew and equipment	B-61	1	40	Day		905	350	1,255	1,800	

## 022 500 | Vibroflotation

0010 VIBROFLOTATION	R022-510	B-60	750	.075	V.L.F.		1.85	1.40	3.25	4.39	504
0900 Vibroflotation compacted sand cylinder, minimum			325	.172			4.27	3.23	7.50	10.10	
0950 Maximum			500	.112			2.78	2.10	4.88	6.60	
1100 Vibro replacement compacted stone cylinder, minimum			250	.224			5.55	4.20	9.75	13.15	
1150 Maximum			.47	.119	Total		2,950	2,225	5,175	7,000	
1300 Mobilization and demobilization, minimum			.14	.400	"		9,925	7,500	17,425	23,600	
1400 Maximum											

## 022 700 | Slope/Erosion Control

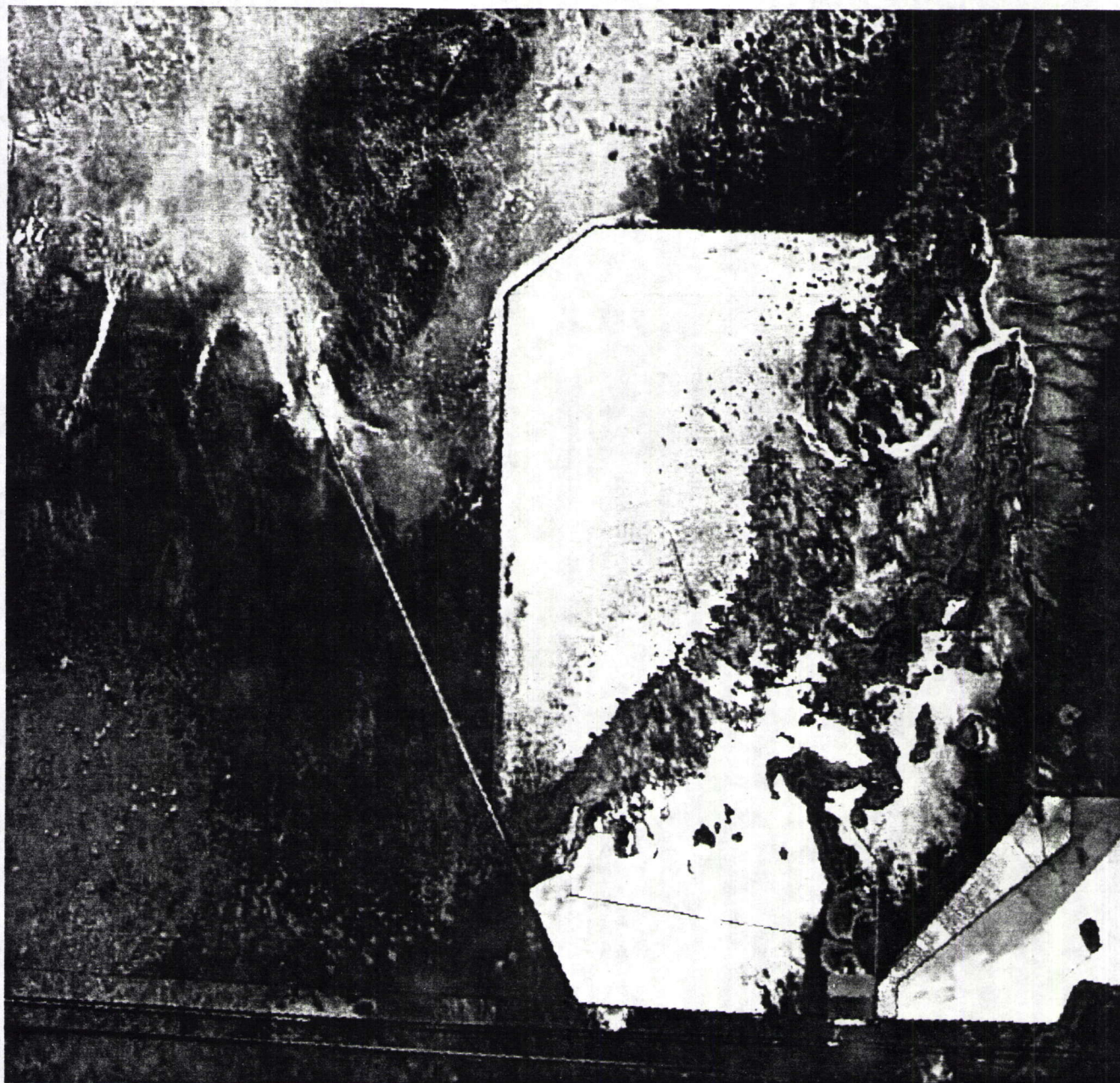
0010 EROSION CONTROL Jute mesh, 100 S.Y. per roll, 4' wide, stapled	B-80A	2,400	.010	S.Y.	.78	.21	.07	1.06	1.27	704
0060 Nylon, 3 dimensional	"	700	.034		3.50	.72	.25	4.47	5.25	
0070 Paper biodegradable mesh	B-1	2,500	.010		.06	.21		.27	.40	
0080 Paper mulch	B-64	20,000	.001		.04	.02	.01	.07	.09	
0100 Plastic netting, stapled, 2" x 1" mesh, 20 mil	B-1	2,500	.010		.40	.21		.61	.77	
0200 Polypropylene mesh, stapled, 6.5 oz./S.Y.		2,500	.010		1.75	.21		1.96	2.26	
0300 Tobacco netting, or jute mesh #2, stapled		2,500	.010		.06	.21		.27	.40	
1000 Silt fence, polypropylene, ideal conditions	2 Clab	1,600	.010	L.F.	.45	.21		.66	.83	
1100 Adverse conditions	"	950	.017	"	.50	.35		.85	1.10	
1200 Place and remove hay bales	A-2	3	8	Ton	50	175	56	281	390	



MAG CORP Area MAY 1985

000441

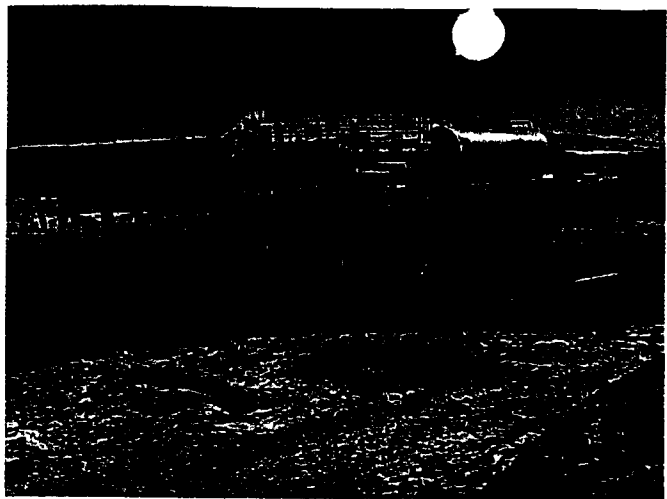




MAGCORP AUG 1998

000442





P1 Pump Station



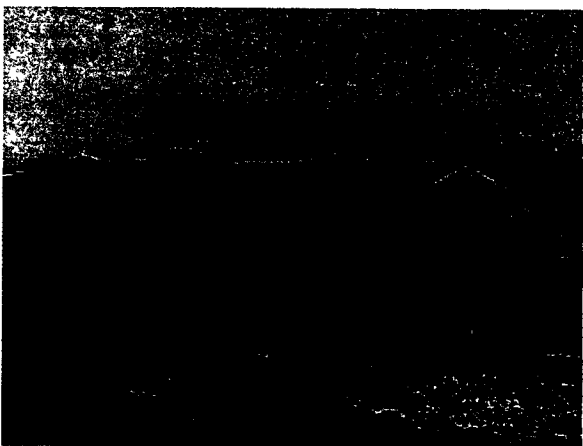
Ditch Interior to Pond 0 & Dike - North Side



Magnesium Chloride Pond West Berm North Pond



South Magnesium Chloride Pond East Berm



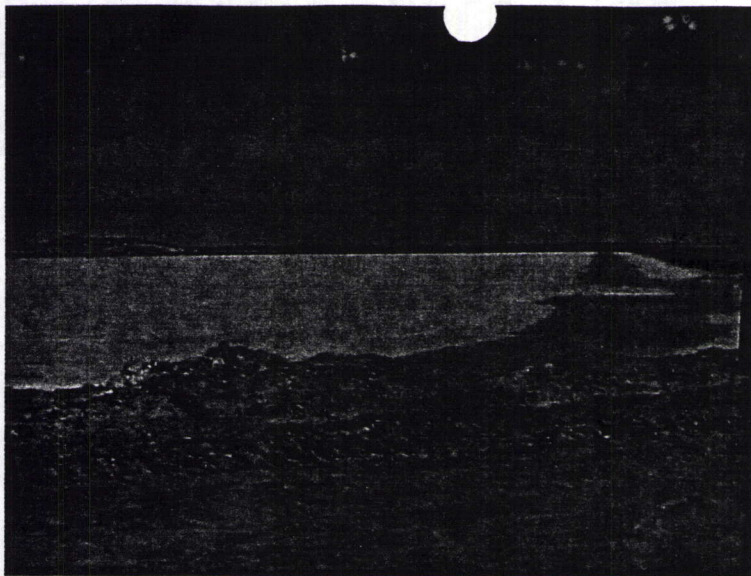
P-2 Feed Canal



Bi-Pass Canal

000443

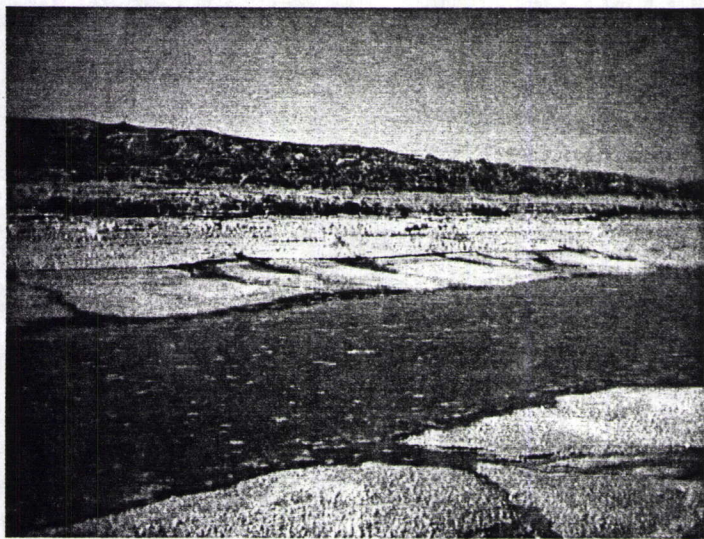




North Brine Storage Pond



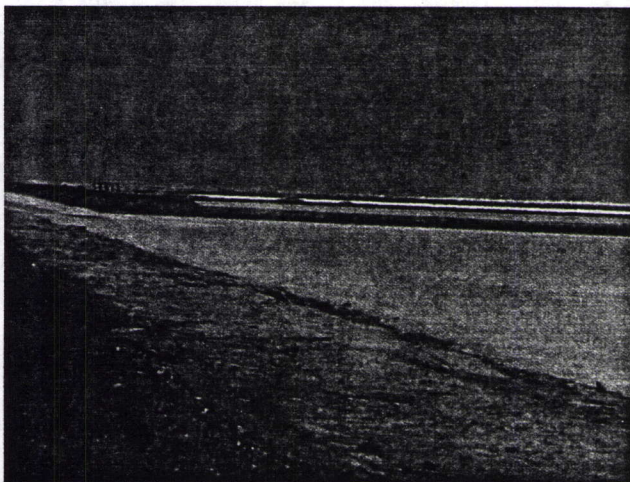
P-1 Feed Canal



Cross Section P-1 Feed Canal



Interior Dikes



Interior Dikes at 7 Inlet Canal



P2 Pump Station

000444





P3 Pump Station (background)



P4 Pump Stations



P5 Pump Station with Sump



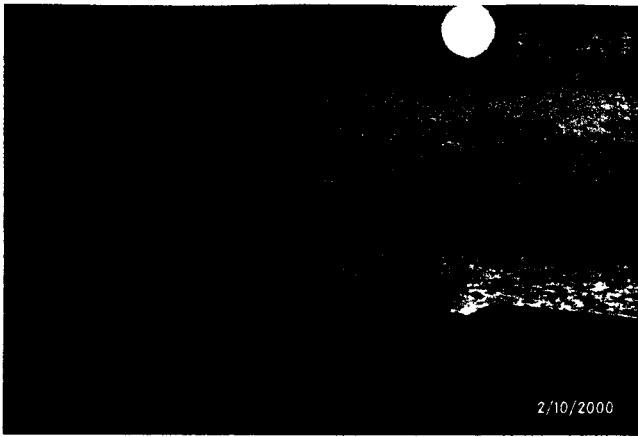
Pond 0 Gate Structure



Shop and Warehouse with Tanks



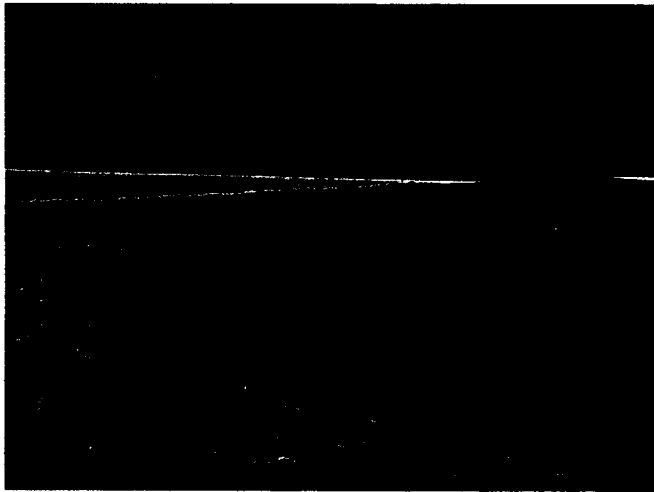
Road through the Dune Area



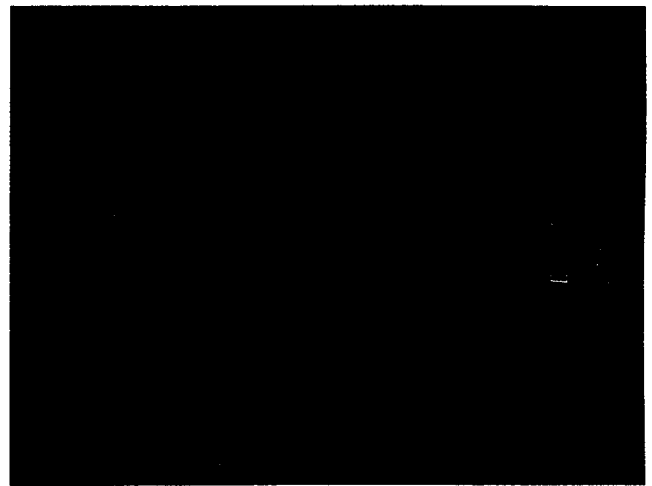
Dike Between Pond 0 and Pond 1



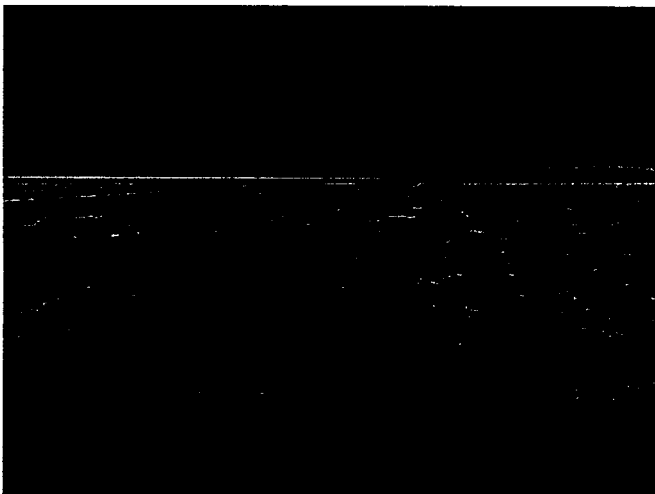
Pond 0 Ditch and North Roads



Pond 5 SW Dike



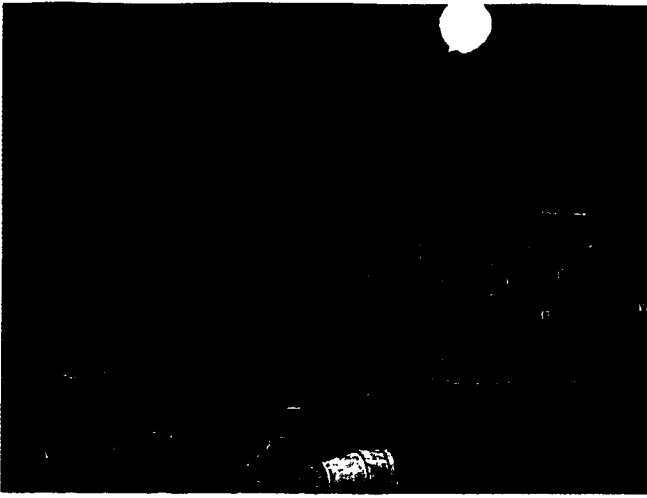
Pond 5 Top Soil Area



Pond 7D



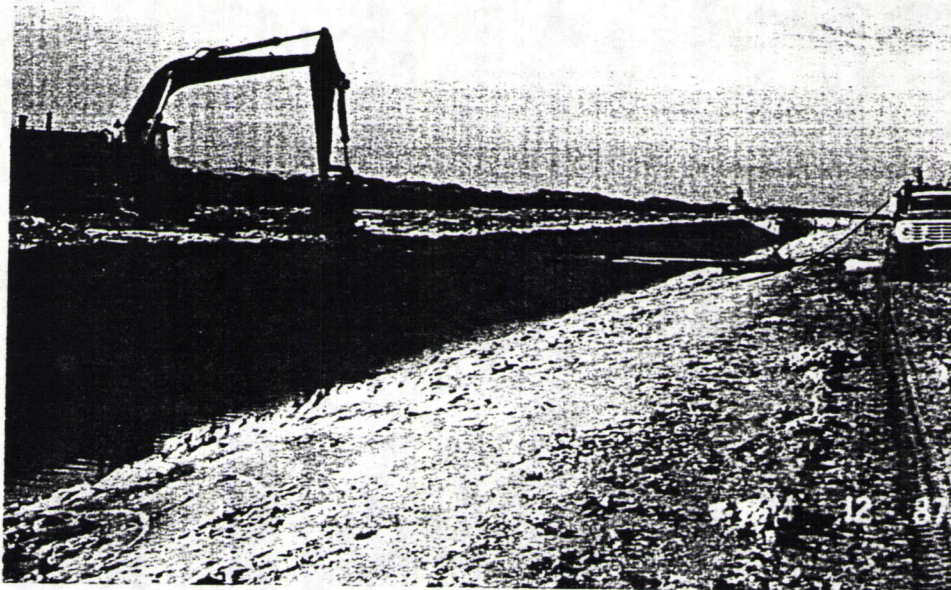
Pond 7D Ditch



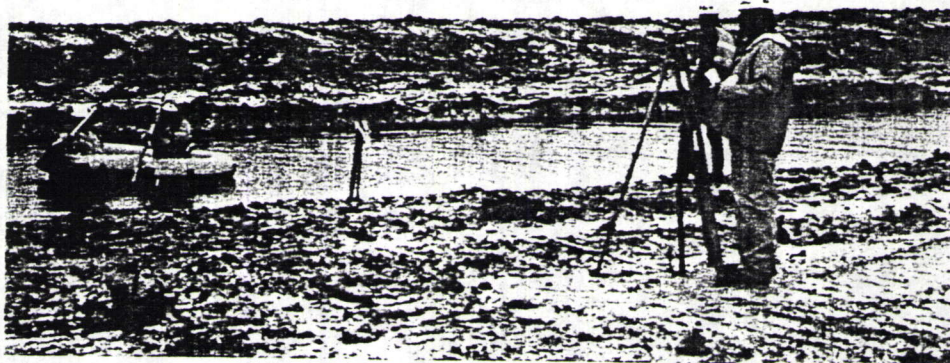
Diesel Tank at P1 Pump Station



Pond 0 West Dike

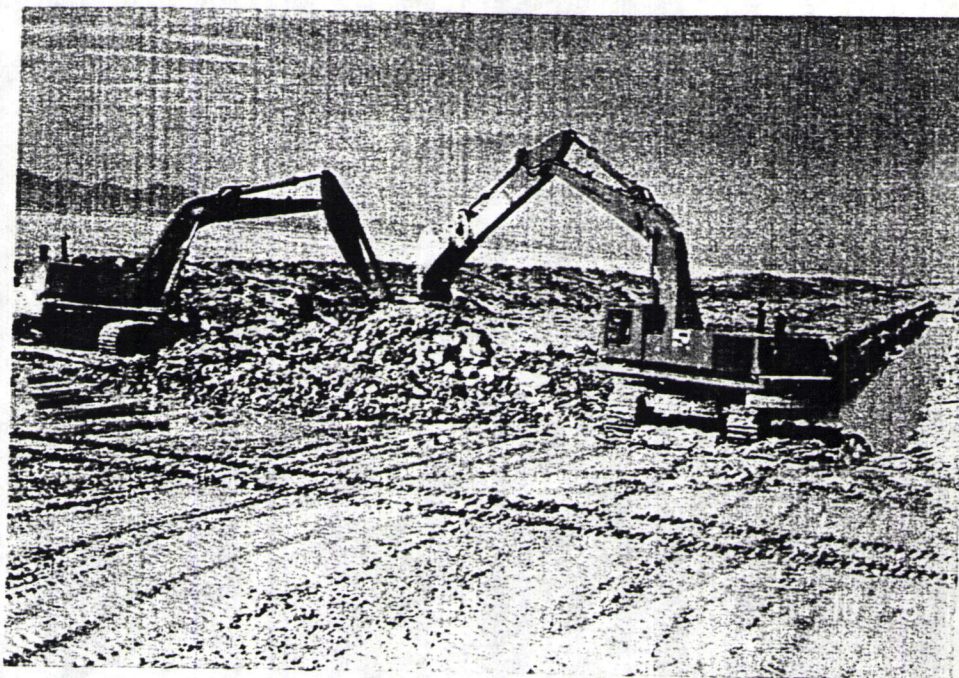


P-1 inlet canal service access bridge.

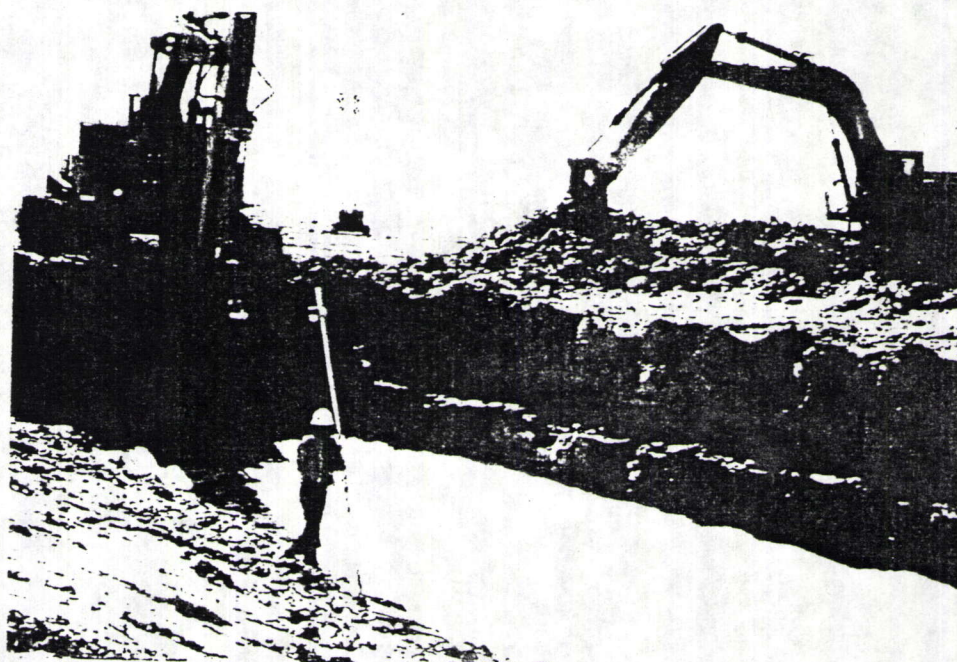


Checking final grade on flooded section of P-1 inlet canal.



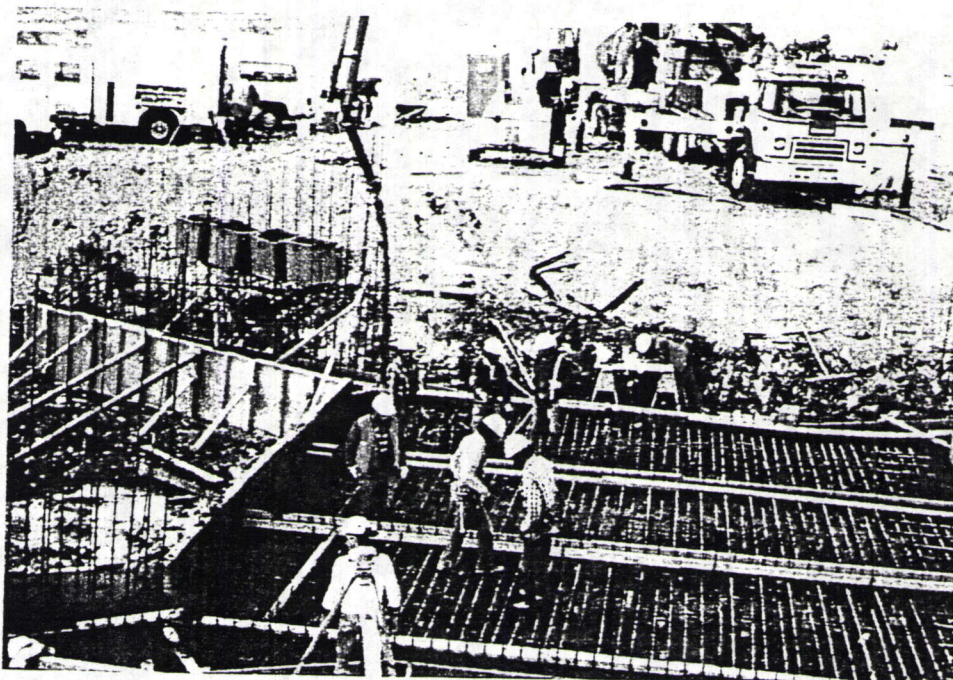


P-1 inlet canal half width excavation. Material required double handling to move to final location.

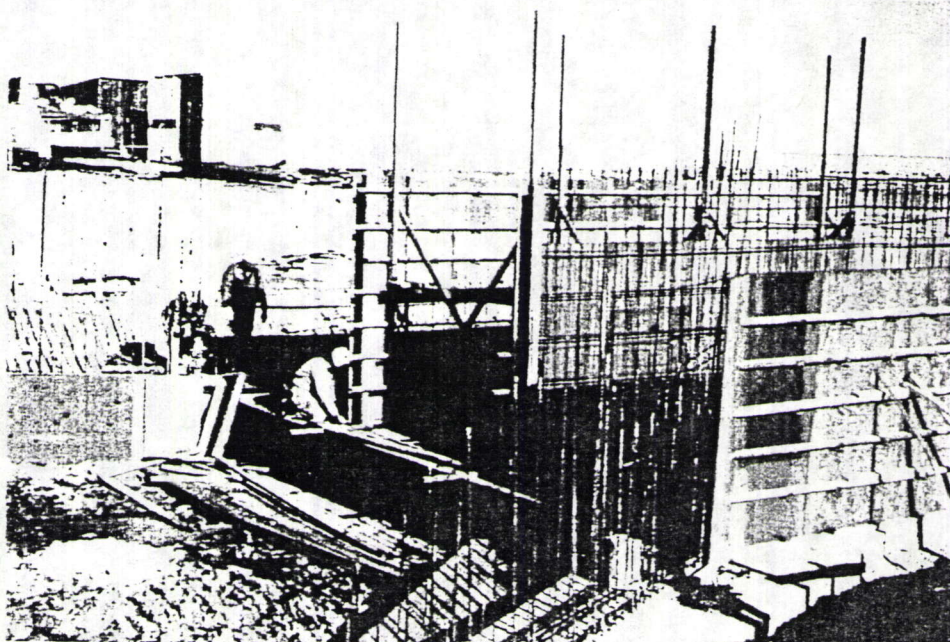


P-1 inlet canal half width excavation.



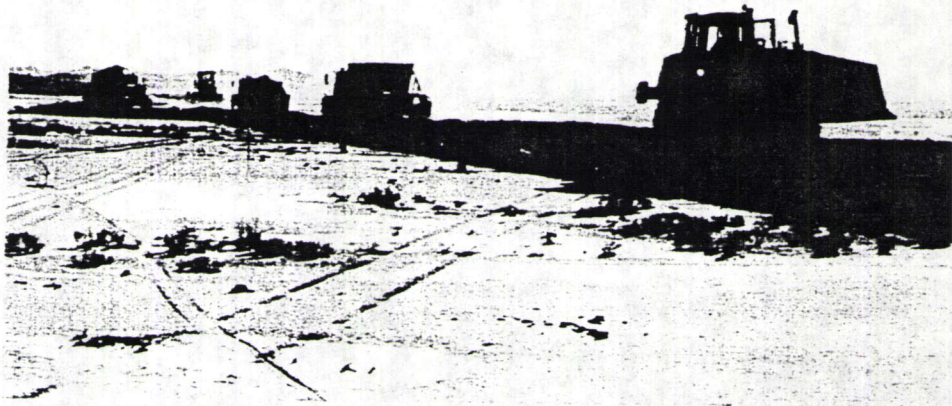


Footing construction for P-1 pumpstation outlet structure.



Wall construction for P-1 pumpstation outlet structure.

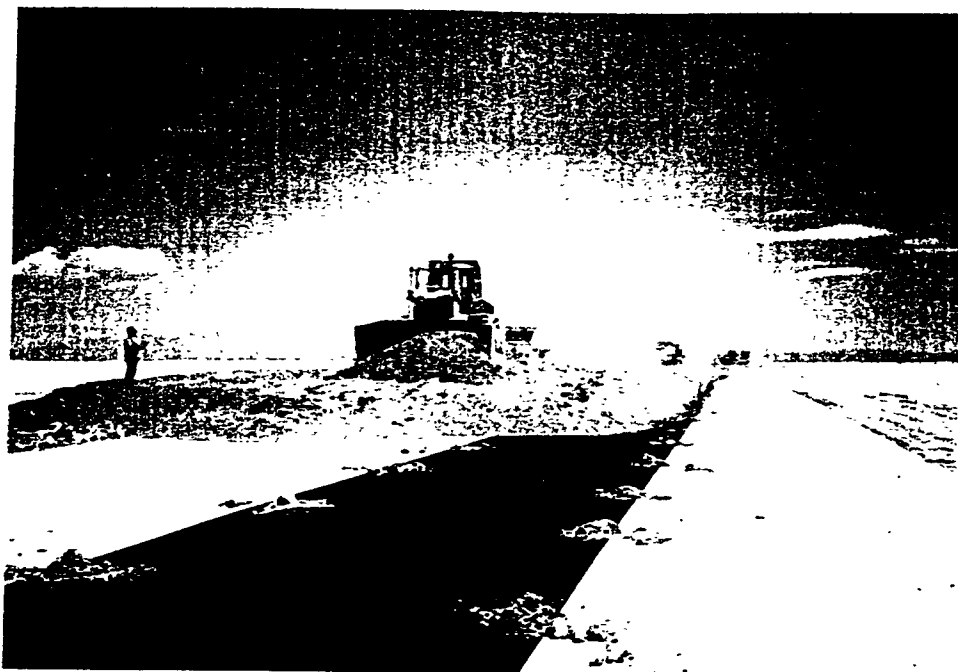




Haul units turning trucks around at turn outs then backing to leading edge of fill on first lift.



Trucks dumping and dozer advancing loading edge of fill on first lift.



Advancing fill over filter fabric for return load.

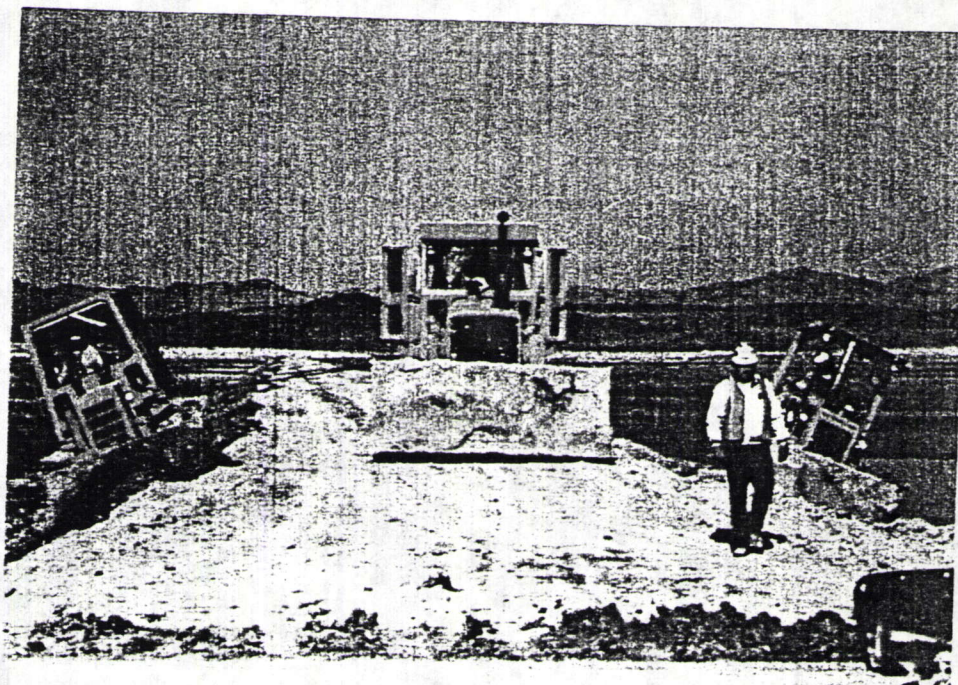


Trucks hauling on dike and return road.



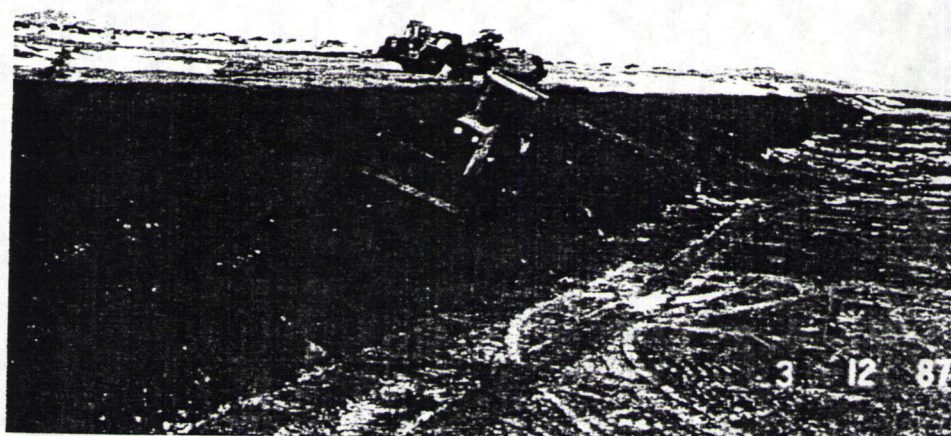


Slope finishing with blade tied off to 623 paddlewheel.

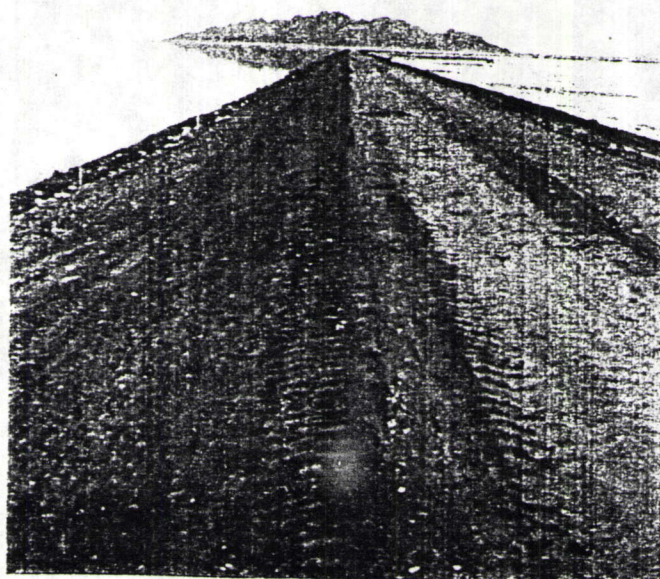


Finishing Pond 7 dikes with D3 and D4 dozers tied off to D6.



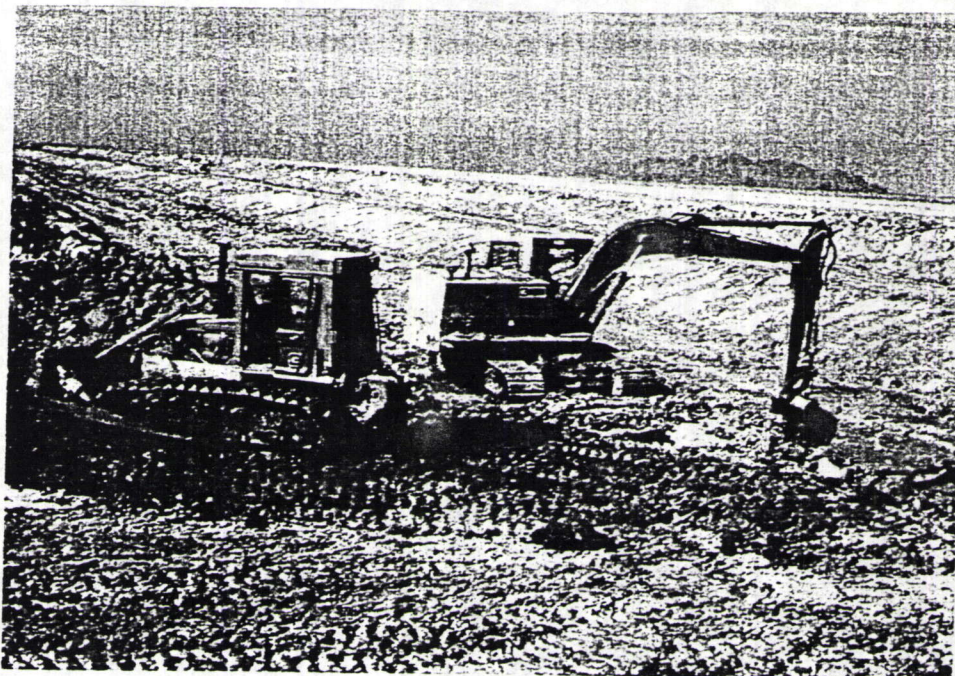


Dozer finishing 250 million gallon reservoir dikes.

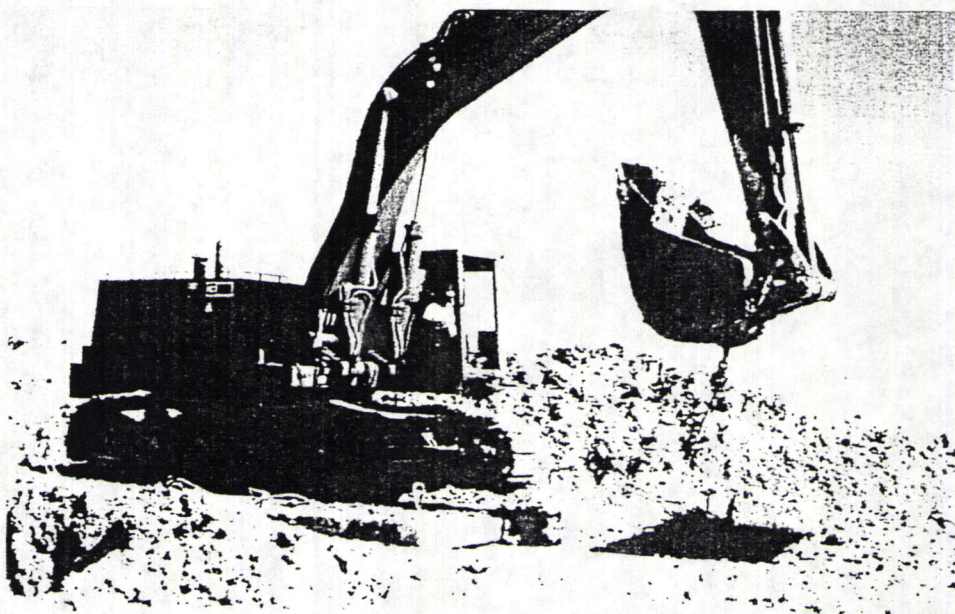


Finished and sold dike section.



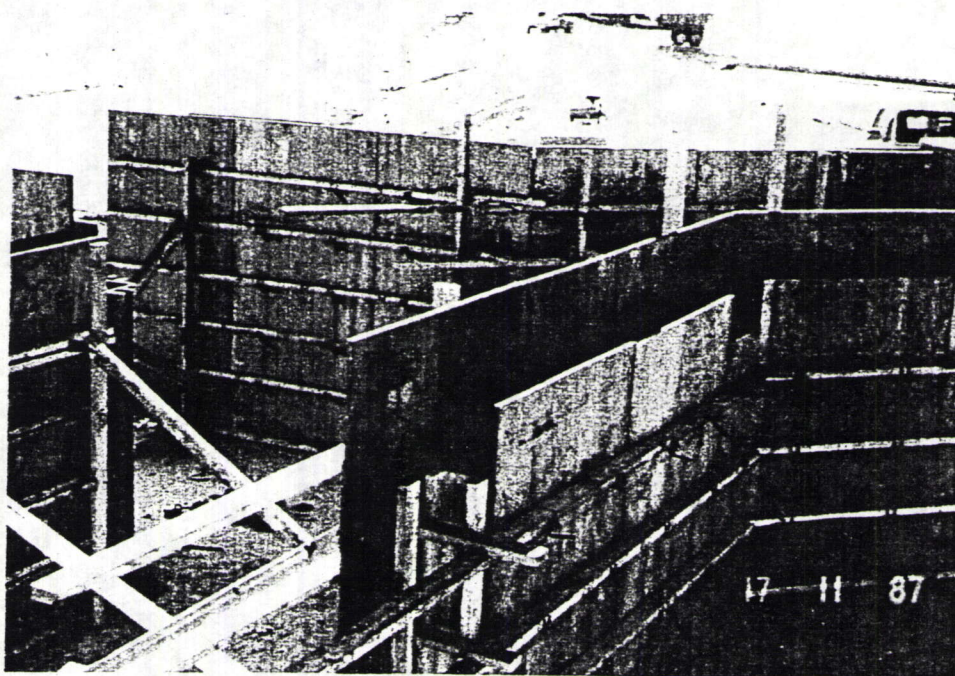


245 hoe excavation, with L.G.P. D6 dozer rehandle, on P-1 inlet canal.

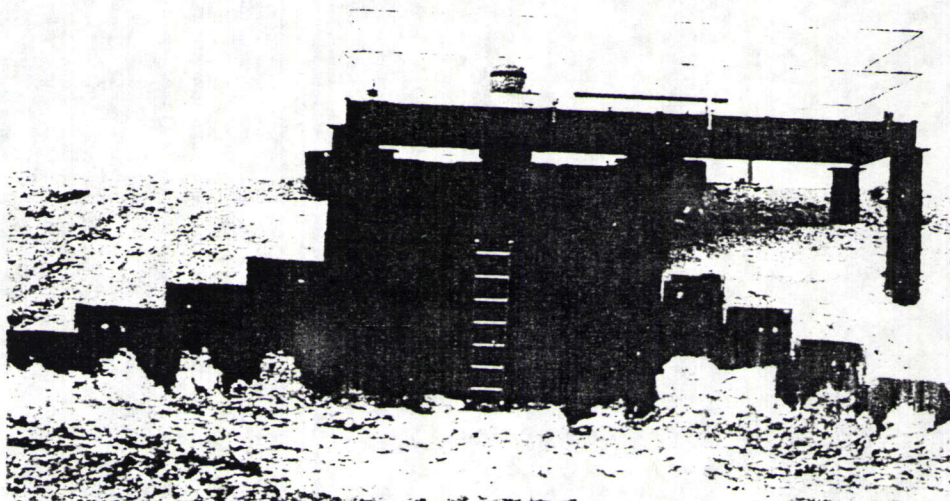


245 hoe shuffling mats. The hoe was required to work off of mats for all inlet canal excavations.





Wall construction for P-1 pumpstation outlet structure.

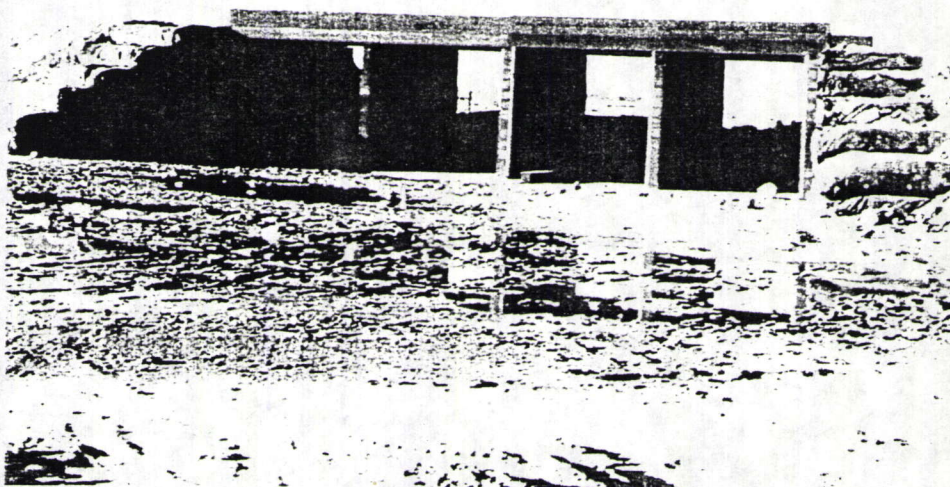


Completed P-4 pumpstation.





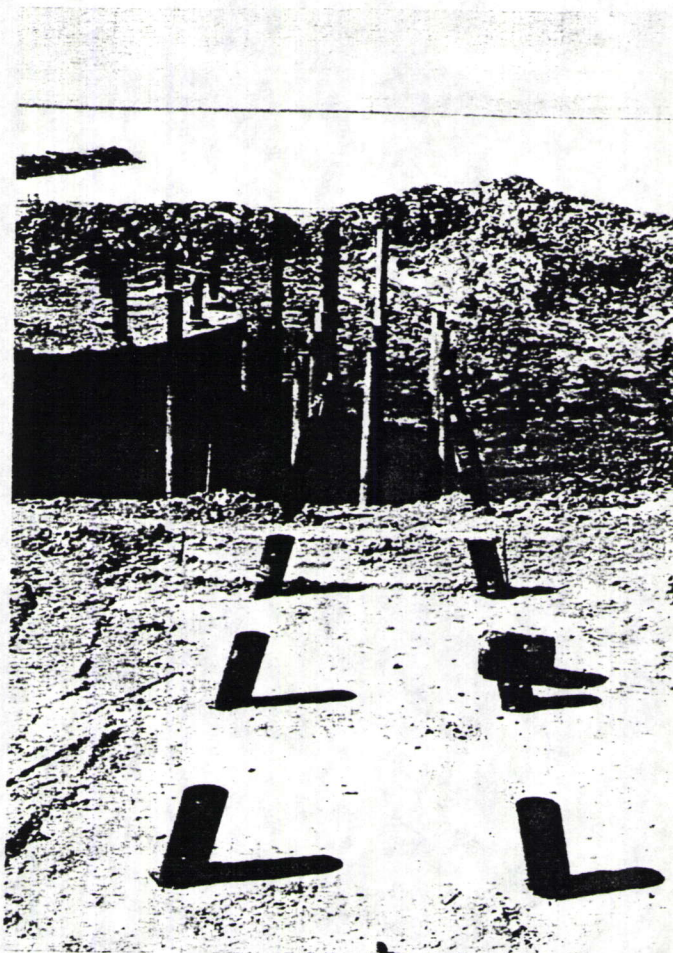
P-1 pumpstation outlet structure rip rap.



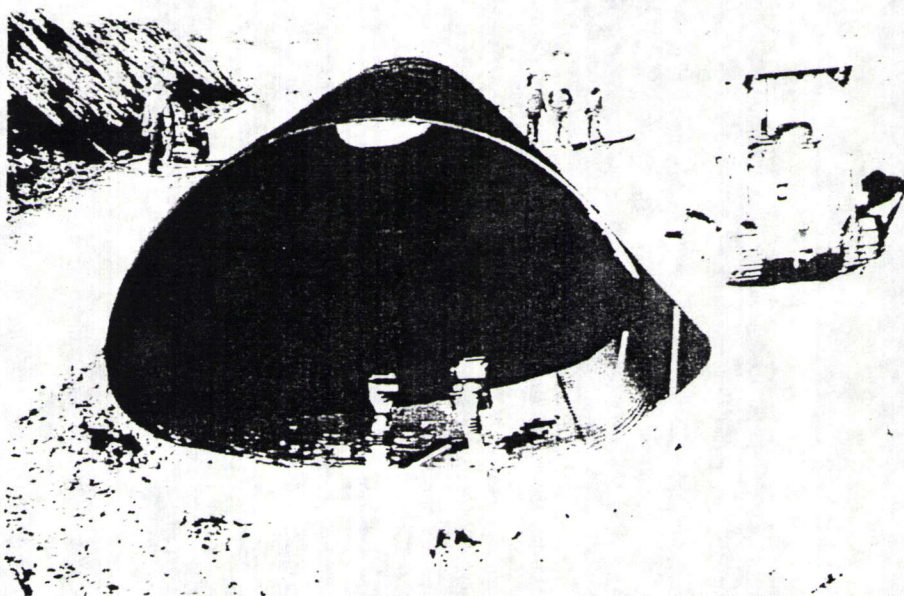
Pond 7 area flow control gates.

000457





Sheet and pipe pile installation for P-1 pumpstation and flume.



Corrugated metal arch pipe installation.



# Weighted Averages for Push Distance Determination

Push					
Area	Length	yds	Push Dist	yds	Dist * Yds
102	528	1995	45	1995	89760
73	1056	2855	45	2855	128480
476	5000	88148	128.5	88148	11327037
265	6400	62815	103	62815	6469926
222	21000	172667	85	172667	14676667
240	38500	342222	201	342222	68786667
218	2500	20185	171	20185	3451667
327	13300	161078	122	161078	19651489
189	8300	58100	150	58100	8715000
220	4900	39926	147	39926	5869111
929	7500	258056	466	258056	120253889
348	11500	148222	230	148222	34091111
175	7500	48611	138	48611	6708333
73	4000	10815	167	10815	1806074
333	1300	16033	140	16033	2244667
		1431728	2338	1431728	304269877
Wt Avg.		212.519397183			



## **APPENDIX 19**

(Utah State Department of Highways and Bureau of Public Roads)



SALT FLAT INVESTIGATIONS

Progress Report

Parts VI - XIII

In Cooperation with  
Utah State Department of Highways  
and Bureau of Public Roads

Engineering Experiment Station  
College of Engineering

Utah State University  
Logan, Utah

January 1962

Property of  
UTAH GEOLOGICAL & MINERAL SURVEY

000462

1. The car's weight is supported only instantaneously and does not allow sufficient time for the salt to deform by creep nor for the confined soil to consolidate.

2. The tire load causes a three-dimensional rather than a two-dimensional stress pattern and additional support of the tire is developed by the salt to the front and the rear as well as to the sides of the tire. This is not true of the two-dimensional highway stress pattern.

3. It must be recognized that a car is very small in comparison with the road bed, and the loads which might be distributed through the blocks of salt provide a major assist in transferring tire loads to the soil. On the other hand, the blocks of salt are so small in comparison with the size of the roadbed that they may be thought of more in terms of bricks floating in a matrix of mud.

4. Actually the soil beneath the salt has a higher bearing capacity than anticipated. Unconfined compression tests indicate that the bearing capacity of the clay is greater than 10 psi. (Refer to Part VI.) Certainly a strength of 10 psi is adequate to support a highway weighing about 700 pounds per square foot, or about 5 psi. Some unconfined compression tests show bearing capacities less than 10 psi; but in every case the material is not clay, but silt or sand. Loose silt or sand in a saturated state can become quick (liquified) if load is applied instantaneously, but the construction of a highway is not an instantaneous process, and the silt and sand layers will have time to consolidate, and if confined, will certainly carry the load.

### Conclusions

1. The salt crust cannot be depended upon to contribute flexural support for the proposed interstate highway. It can serve no better purpose than fill material and a possible temporary means of distributing loads of equipment and highway fill until consolidation of the soil can be accomplished.

2. If the salt must be used as fill, then it is desirable that it be sealed against groundwater flow. A serious limitation of salt is its instability in the presence of groundwater flow and its tendency to dissolve and re-crystallize thus relieving stresses and reducing the load-carrying capacity. It may be advisable to place a short section of fill on the salt after preliminary soil tests are made. By observing it for a year, the amount of dissolution and recrystallization of the salt may be noted. However, the Western Pacific Railway line has been placed on fill directly on the salt crust. The railroad company's experience and tests on this fill may reveal the necessary information.



## APPENDIX 20

(Utah Division of Oil Gas and Mining Reclamation Costs)



## RECLAMATION COST BASIS

last revision

12/1/2000

## RIPPING D7R

Parameters Used in Calculations for File No.

## DETAILS/ASSUMPTIONS

- CAT D7R dozer, 230 hp, semi-U blade, multishank ripper, fixed parallelogram (3 tips)
- shank gauge 6' 6" (tip to tip), pocket spacing 3' 3" (between shanks)
- ASSUME width between passes ~2' 6" => overall pass width =9.0'
- ASSUME ripping to 12" depth MINIMUM; 1 MPH=88 FPM or 1.5 ft per second
- ASSUME: mtl with seismic velocity of 6,000 fps => ripping at 0.25 MPH
- one acre = 43,560 SF; use ~400' x 110' block
- ASSUME every 400' requires 0.30 min to raise, pivot, turn & lower
- ASSUME work efficiency of 50 minutes/hour => 83%

	D7R	DIST	SPEED	ADD	MIN/PASS
Time/Pass =(dist/speed)+add on		400.00	1.00	0.30	4.85
NOTE: SPEED IN MPH			TIME		PASS/HR
#Pass/Hour = time/(MIN/PASS)			50.00		10.32
			FT/PASS		SF/PASS
Sq-ft Ripped/Pass =(length/pass)*(FT/PASS)			9.00		3600.00
					ACRE/PASS
Acre Ripped/Pass = (SF/PASS)/(SF/acre)			CY/Pass		0.08
			133		ACRE/HR
Acre Ripped/Hr =(ACRE/PASS)*(PASS/HR)			CY/HR		0.85
			1,376		HRS/ACRE
Hrs to Rip one acre = 1 /(ACRE/HR)					1.17
				6.8	ACRE/8HR-DAY

## FROM RENTAL RATE BLUE BOOK 3Q/00

	EQUIP	OPER
Hourly Cost, D7R, EROPS, semi-U blade, (pg 9-41)	115.00	30.30
Multi-shank rippers, 3 parallelogram, 230 hp (pg 9-47)	15.00	2.80
Sub-totals	130.00	33.10
Multi by regional factor (page 9-vii)	0.87	1.00
Sub-totals	112.45	33.10

Sub-total Equipment &amp; Operating Cost

145.55 (\$/HR)

## FROM MEANS HEAVY CONSTRUCTION COST DATA 2000

Crew B-10B, 1-Equip Operator (med), hourly cost 40.87 (\$/HR)

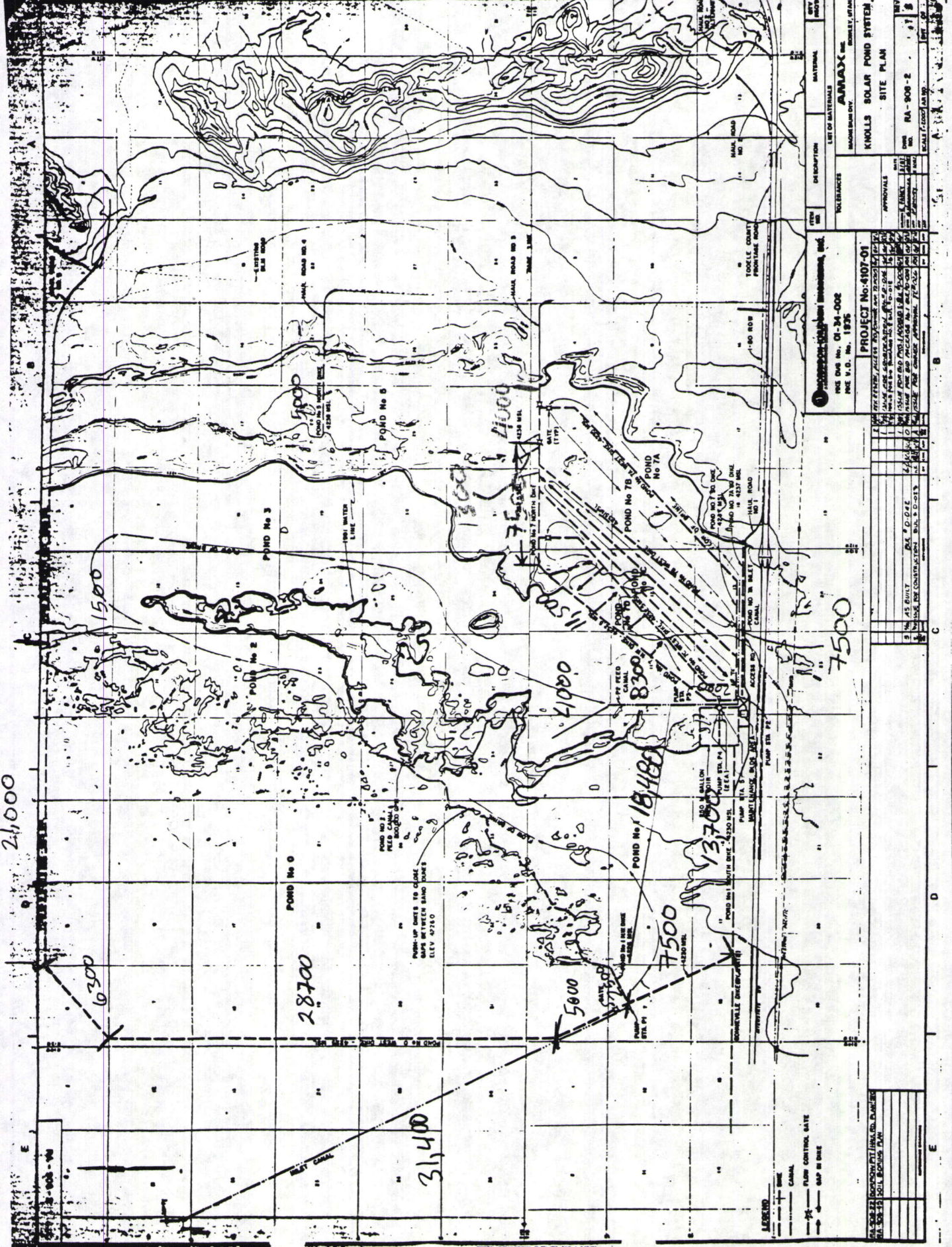
TOTAL COST PER HOUR		186.42 (\$/HR)
COST PER CUBIC YARD	\$/CY	0.14
TOTAL RIPPING COST PER ACRE (rounded)		\$219 (\$/ACRE)
current speed used =	1.00 mph	
RIPPING D7R 230hp		

000465





24000



PROJECT No. 4107-01  
PDS No. 01-34-002  
PDS No. 1975

AMAX, INC.  
ENGINEER, MAP  
MAJOR BUREAU

KNOLLS SOLAR POND SYSTEM  
SITE PLAN

DATE: RA-908-2  
SCALE: 1" = 2000' (AS SHOWN)

NO.	DESCRIPTION	MATERIAL	QTY	UNIT
1	GRAVEL			
2	SAND			
3	ROCK			
4	CONCRETE			
5	STEEL			
6	PIPE			
7	WIRE			
8	PAINT			
9	GLASS			
10	BRICK			
11	CEMENT			
12	WOOD			
13	PLASTER			
14	ROOFING			
15	INSULATION			
16	GLAZING			
17	SEALANT			
18	FASTENERS			
19	WELDING			
20	PAINTING			
21	CONCRETE			
22	STEEL			
23	PIPE			
24	WIRE			
25	PAINT			
26	GLASS			
27	BRICK			
28	CEMENT			
29	WOOD			
30	PLASTER			
31	ROOFING			
32	INSULATION			
33	GLAZING			
34	SEALANT			
35	FASTENERS			
36	WELDING			
37	PAINTING			
38	CONCRETE			
39	STEEL			
40	PIPE			
41	WIRE			
42	PAINT			
43	GLASS			
44	BRICK			
45	CEMENT			
46	WOOD			
47	PLASTER			
48	ROOFING			
49	INSULATION			
50	GLAZING			
51	SEALANT			
52	FASTENERS			
53	WELDING			
54	PAINTING			
55	CONCRETE			
56	STEEL			
57	PIPE			
58	WIRE			
59	PAINT			
60	GLASS			
61	BRICK			
62	CEMENT			
63	WOOD			
64	PLASTER			
65	ROOFING			
66	INSULATION			
67	GLAZING			
68	SEALANT			
69	FASTENERS			
70	WELDING			
71	PAINTING			
72	CONCRETE			
73	STEEL			
74	PIPE			
75	WIRE			
76	PAINT			
77	GLASS			
78	BRICK			
79	CEMENT			
80	WOOD			
81	PLASTER			
82	ROOFING			
83	INSULATION			
84	GLAZING			
85	SEALANT			
86	FASTENERS			
87	WELDING			
88	PAINTING			
89	CONCRETE			
90	STEEL			
91	PIPE			
92	WIRE			
93	PAINT			
94	GLASS			
95	BRICK			
96	CEMENT			
97	WOOD			
98	PLASTER			
99	ROOFING			
100	INSULATION			

000467



Independent Statistics Consultant.

Very good experiences with Utah DOGM and Federal OSM.

Skillful in statistics but still good at maintaining reality and actual, in-the-field application.

**John W. Kern**  
**Spectrum Consulting Services**  
**415 NW Robert**  
**Pullman, WA 99163**

(509) 339-2489

johnk1@gte.net





## StatAdvisor

Welcome to the StatAdvisor. The StatAdvisor is designed to assist in interpreting the results of statistical procedures. It will explain the results of statistical tests, warn you about any critical assumptions which may be violated by your data, and suggest other procedures which might be applied.

You can access this window at any time by pressing the StatAdvisor button on the main toolbar. You can also have StatAdvisor output added automatically to the bottom of all text panes by checking StatAdvisor under View on the main menu.

000469

17		3.0	15	07/11/99
18	10	4	16.4	10/30/99
19	11	3.3	33.3	11/15/99
20	12	2.9	17.4	12/25/99





QuakeDat2.sf3

	Location	Magnitude	Distance	Date	Col 5	Col 6
1	1	3.2	4.5	01/01/98		
2	1	4	3	01/01/98		
3	2	3	17	02/15/98		
4	2	4.1	22	04/22/98		
5	2	5	15.2	04/23/98		
6	3	2.4	10	06/13/98		
7	3	7.2	15	06/30/98		
8	4	4.4	30.2	08/12/98		
9	5	2.6	6.5	09/24/98		
10	5	2.4	12	11/26/98		
11	5	3	8.5	01/29/99		
12	5	4.5	10	03/03/99		
13	6	3.1	22	04/20/99		
14	7	2.8	18	05/01/99		
15	8	2	4.4	06/26/99		
16	8	2.6	10.2	08/22/99		
17	9	3.6	19	09/21/99		
18	10	4	16.4	10/30/99		
19	11	3.3	33.3	11/15/99		
20	12	2.9	17.4	12/25/99		

MultBoxWhi... ☐ ☐ ☐ 
 Mag/Box... ☐ ☐ ☐ 
 Mag/Loc Si... ☐ ☐ ☐ 
 Mag/Dist Si... ☐ ☐ ☐ 
 Mag/Proba... ☐ ☐ ☐ 
 Mag/Proba... ☐ ☐ ☐ 
 QuakeDem... ☐ ☐ ☐ 
 StatAdvisor ☐ ☐ ☐ 
 StatGallery ☐ ☐ ☐ 
 StatReporter ☐ ☐ ☐ 
 Mag/Loc ☐ ☐ ☐ 
 Date/Loc ☐ ☐ ☐

Ready

Start

Novell-delivered Applicatio...

STATGRAPHICS Plus...

NOV 11 11:13 AM





Mag/Loc



## Analysis Summary

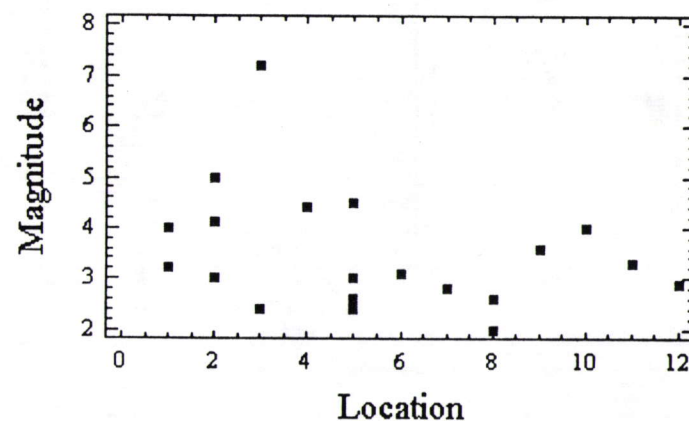
X variable: Location  
Y variable: Magnitude

20 values

## The StatAdvisor

-----  
This procedure creates a scatterplot of Magnitude versus Location.  
To fit a curve to this data, select Relate - Simple Regression from  
the main menu.

Plot of Magnitude vs Location



Row	Location	Magnitude	Date
1	1	2.6	09/24/98
10	5	2.4	11/26/98
11	5	3	01/29/99
12	5	4.5	03/03/99
13	6	3.1	04/20/99
14	7	2.8	05/01/99
15	8	2	06/26/99
16	8	2.6	08/22/99
17	9	3.6	09/21/99
18	10	4	10/30/99
19	11	3.3	11/15/99
20	12	2.9	12/25/99







Date/Loc

File Edit View Options Help



## Analysis Summary

X variable: Location

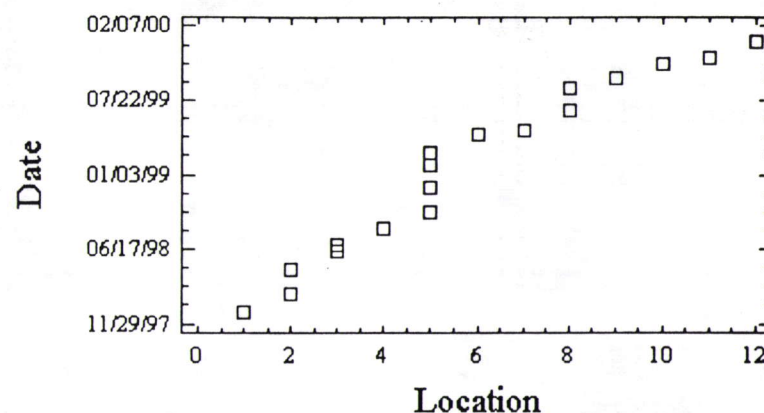
Y variable: Date

20 values

## The StatAdvisor

-----  
This procedure creates a scatterplot of Date versus Location. To fit a curve to this data, select Relate - Simple Regression from the main menu.

Plot of Date vs Location



9	5	2.8	8.5	09/24/98
10	5	2.4	12	11/26/98
11	5	3	8.5	01/29/99
12	5	4.5	10	03/03/99
13	6	3.1	22	04/20/99
14	7	2.8	18	05/01/99
15	8	2	4.4	06/26/99
16	8	2.6	10.2	08/22/99
17	9	3.6	19	09/21/99
18	10	4	16.4	10/30/99
19	11	3.3	33.3	11/15/99
20	12	2.9	17.4	12/25/99

000472



Ready

NUM1





MultBoxWhisk



## Analysis Summary

Dependent variable: Magnitude

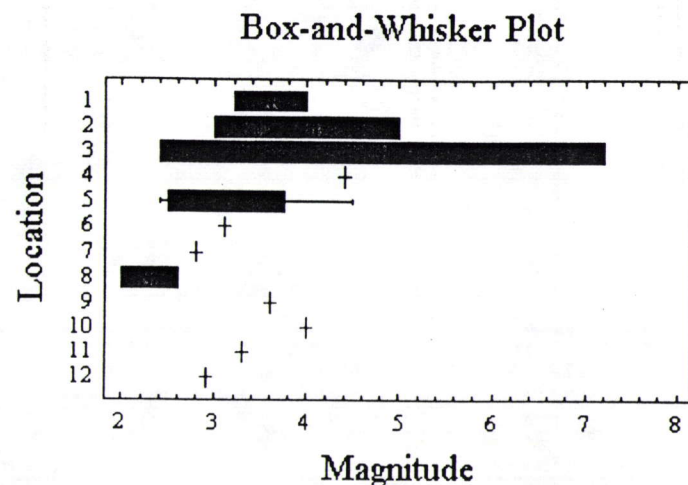
Factor: Location

Number of observations: 20

Number of levels: 12

## The StatAdvisor

This procedure constructs box-and-whisker plots to compare the 12 samples of Magnitude. For a detailed statistical analysis of this data, select Compare - Analysis of Variance - One-Way ANOVA from the main menu.



9	5	2.6	6.3	09/24/96
10	5	2.4	12	11/26/98
11	5	3	8.5	01/29/99
12	5	4.5	10	03/03/99
13	6	3.1	22	04/20/99
14	7	2.8	18	05/01/99
15	8	2	4.4	06/26/99
16	8	2.6	10.2	08/22/99
17	9	3.6	19	09/21/99
18	10	4	16.4	10/30/99
19	11	3.3	33.3	11/15/99
20	12	2.9	17.4	12/25/99





Mag/Box&amp;Whisk



Lbf

Row

## Analysis Summary

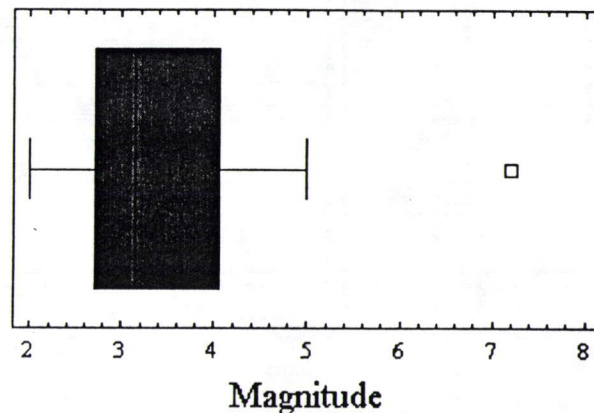
Data variable: Magnitude

20 values ranging from 2.0 to 7.2

## The StatAdvisor

This procedure displays a box-and-whisker plot of a single column of data. You can create many other graphs and statistics for the data by selecting Describe - Numeric Data - One-Variable Analysis from the main menu.

Box-and-Whisker Plot



1	5	2.0	6.5	09/24/96
10	5	2.4	12	11/26/98
11	5	3	8.5	01/29/99
12	5	4.5	10	03/03/99
13	6	3.1	22	04/20/99
14	7	2.8	18	05/01/99
15	8	2	4.4	06/26/99
16	8	2.6	10.2	08/22/99
17	9	3.6	19	09/21/99
18	10	4	16.4	10/30/99
19	11	3.3	33.3	11/15/99
20	12	2.9	17.4	12/25/99

MultBox&amp;Whisk

Mag/Loc Si

Mag/Dist Si

Mag/Proba

Mag/Proba...

QuakeDem...

StatAdvisor

StatGallery

StatReporter

Mag/Loc

Date/Loc

Ready

Start

Novell-delivered Applicatio...

STATGRAPHICS Plus...

NUM 11:14 AM





## Mag/Loc Simple Regression



Lb:

Row:

Regression Analysis - Linear model:  $Y = a + b \cdot X$ 

Dependent variable: Magnitude

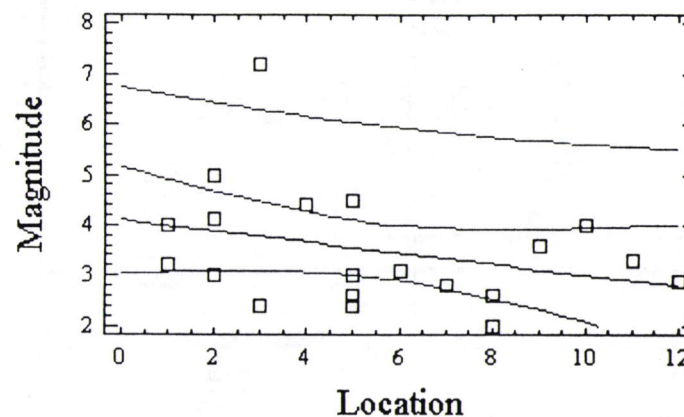
Independent variable: Location

Parameter	Estimate	Standard Error	T Statistic	P-Value
Intercept	4.09991	0.502762	8.15477	0.0000
Slope	-0.109157	0.0791481	-1.37915	0.1847

## Analysis of Variance

Source	Sum of Squares	Df	Mean Square	F-Ratio
--------	----------------	----	-------------	---------

Plot of Fitted Model



9	5	2.6	6.3	09/24/98
10	5	2.4	12	11/26/98
11	5	3	8.5	01/29/99
12	5	4.5	10	03/03/99
13	6	3.1	22	04/20/99
14	7	2.8	18	05/01/99
15	8	2	4.4	06/26/99
16	8	2.6	10.2	08/22/99
17	9	3.6	19	09/21/99
18	10	4	16.4	10/30/99
19	11	3.3	33.3	11/15/99
20	12	2.9	17.4	12/25/99





## Mag/Dist Simple Regression

Regression Analysis - Linear model:  $Y = a + b \cdot X$ 

Dependent variable: Magnitude

Independent variable: Distance

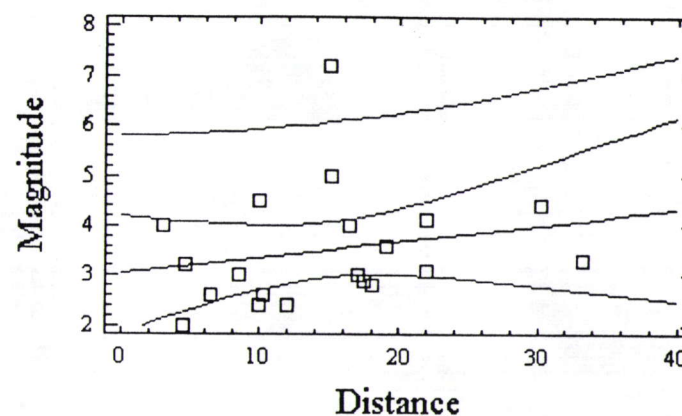
Parameter	Estimate	Standard Error	T Statistic	P-Value
Intercept	3.03386	0.55798	5.43723	0.0000
Slope	0.0319848	0.0333402	0.959345	0.3501

## Analysis of Variance

Source	Sum of Squares	Df	Mean Square	F-Ratio
--------	----------------	----	-------------	---------

9	5	2.0	8.5	09/24/98
10	5	2.4	12	11/26/98
11	5	3	8.5	01/29/99
12	5	4.5	10	03/03/99
13	6	3.1	22	04/20/99
14	7	2.8	18	05/01/99
15	8	2	4.4	06/26/99
16	8	2.6	10.2	08/22/99
17	9	3.6	19	09/21/99
18	10	4	16.4	10/30/99
19	11	3.3	33.3	11/15/99
20	12	2.9	17.4	12/25/99

Plot of Fitted Model







## Mag/Probability Plots



## Probability Plots

Data variable: Magnitude

Number of observations: 20

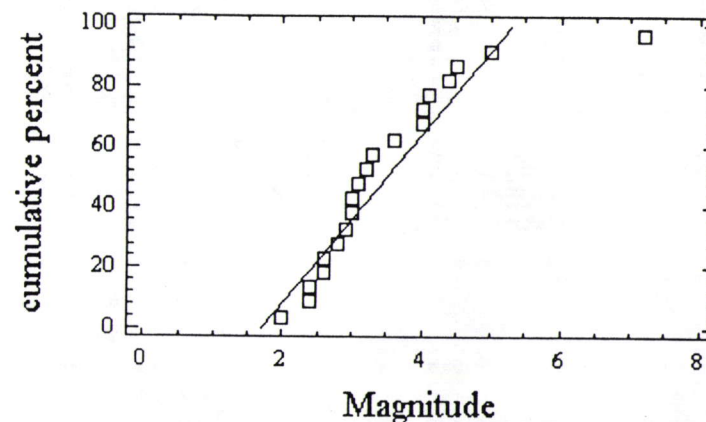
Number of values below minimum: 0

Number of values above maximum: 0

## The StatAdvisor

This procedure creates seven different types of probability plots to help you determine whether Magnitude comes from a particular type of distribution. After examining these plots, you may fit a distribution to the data by selecting the Distribution Fitting procedure.

Uniform Probability Plot



9	5	2.0	6.5	09/24/98
10	5	2.4	12	11/26/98
11	5	3	8.5	01/29/99
12	5	4.5	10	03/03/99
13	6	3.1	22	04/20/99
14	7	2.8	18	05/01/99
15	8	2	4.4	06/26/99
16	8	2.6	10.2	08/22/99
17	9	3.6	19	09/21/99
18	10	4	16.4	10/30/99
19	11	3.3	33.3	11/15/99
20	12	2.9	17.4	12/25/99





## Mag/Probability Plot



## Analysis Summary

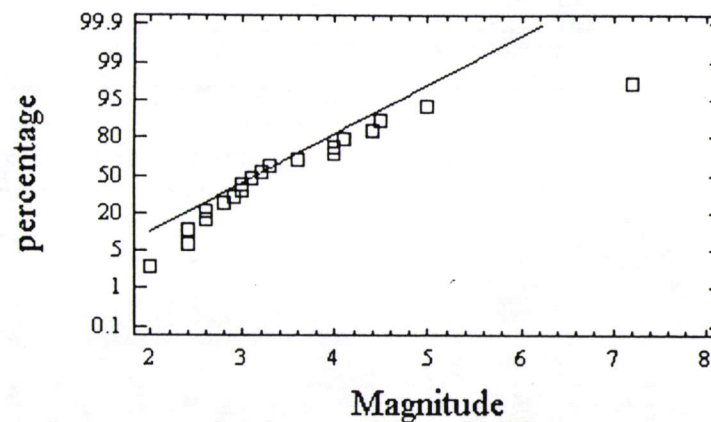
Data variable: Magnitude

20 values ranging from 2.0 to 7.2

## The StatAdvisor

This procedure displays a normal probability plot of a single column of data. You can create many other graphs and statistics for the data by selecting Describe - Numeric Data - One-Variable Analysis from the main menu.

Normal Probability Plot for Magnitude



14	7	2.8	18	05/01/99
15	8	2	4.4	06/26/99
16	8	2.6	10.2	08/22/99
17	9	3.6	19	09/21/99
18	10	4	16.4	10/30/99
19	11	3.3	33.3	11/15/99
20	12	2.9	17.4	12/25/99





QuakeDat2.s13

	Location	Magnitude	Distance	Date	Col 5	Col 6
1		3.2	4.5	01/01/98		
2		4	3	01/01/98		
3		3	17	02/15/98		
4		4.1	22	04/22/98		
5		5	15.2	04/23/98		
6		2.4	10	06/13/98		
7		7.2	15	06/30/98		
8		4.4	30.2	08/12/98		
9		2.6	6.5	09/24/98		
10		2.4	12	11/26/98		
11		3	8.5	01/29/99		
12		4.5	10	03/03/99		
13		3.1	22	04/20/99		
14		2.8	18	05/01/99		
15		2	4.4	06/26/99		
16		2.6	10.2	08/22/99		
17		3.6	19	09/21/99		
18		4	16.4	10/30/99		
19		3.3	33.3	11/15/99		
20		2.9	17.4	12/25/99		

000479





Mag/Loc



Lbt

Row

## Analysis Summary

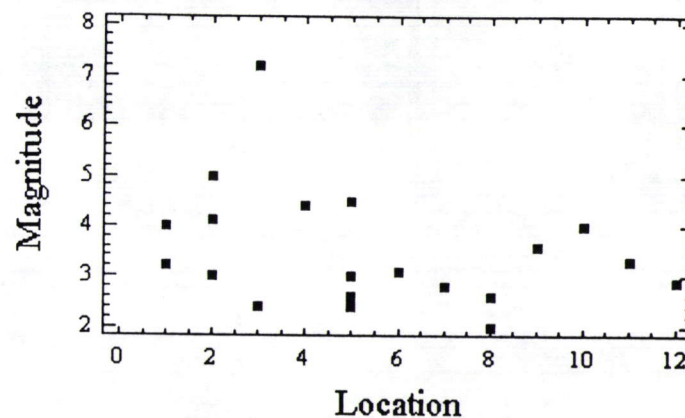
X variable: Location  
Y variable: Magnitude

20 values

## The StatAdvisor

This procedure creates a scatterplot of Magnitude versus Location. To fit a curve to this data, select Relate - Simple Regression from the main menu.

Plot of Magnitude vs Location



9	5	2.6	8.5	09/24/96
10	5	2.4	12	11/26/98
11	5	3	8.5	01/29/99
12	5	4.5	10	03/03/99
13	6	3.1	22	04/20/99
14	7	2.8	18	05/01/99
15	8	2	4.4	06/26/99
16	8	2.6	10.2	08/22/99
17	9	3.6	19	09/21/99
18	10	4	16.4	10/30/99
19	11	3.3	33.3	11/15/99
20	12	2.9	17.4	12/25/99

MultiBox/Whi...	Mag/Box&...	Mag/Loc Si...	Mag/Dist Si...	Mag/Proba...	Mag/Proba...
QuakeDem...	StatAdvisor	StatGallery	StatReporter	Date/Loc	





Date/Loc



Lbl

Row

## Analysis Summary

X variable: Location

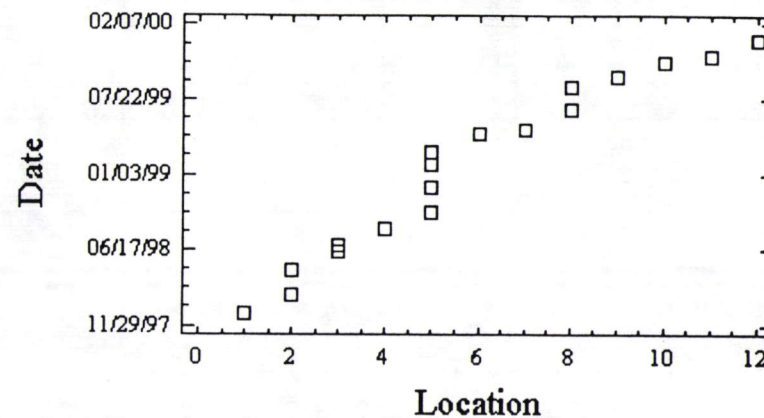
Y variable: Date

20 values

## The StatAdvisor

This procedure creates a scatterplot of Date versus Location. To fit a curve to this data, select Relate - Simple Regression from the main menu.

Plot of Date vs Location



1	5	2.0	8.5	09/24/98
10	5	2.4	12	11/26/98
11	5	3	8.5	01/29/99
12	5	4.5	10	03/03/99
13	6	3.1	22	04/20/99
14	7	2.8	18	05/01/99
15	8	2	4.4	06/26/99
16	8	2.6	10.2	08/22/99
17	9	3.6	19	09/21/99
18	10	4	16.4	10/30/99
19	11	3.3	33.3	11/15/99
20	12	2.9	17.4	12/25/99





MultBoxWhisk



## Analysis Summary

Dependent variable: Magnitude

Factor: Location

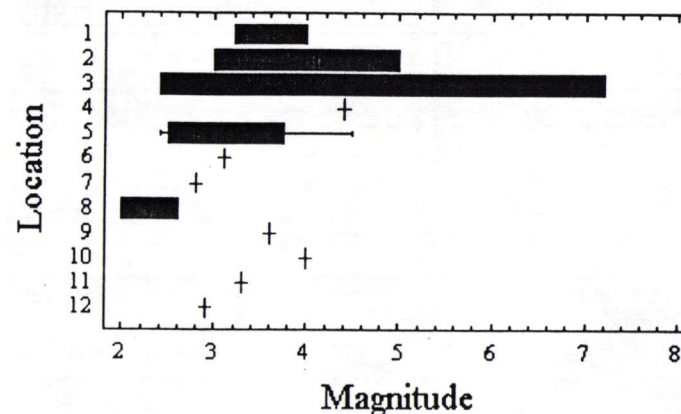
Number of observations: 20

Number of levels: 12

## The StatAdvisor

This procedure constructs box-and-whisker plots to compare the 12 samples of Magnitude. For a detailed statistical analysis of this data, select Compare - Analysis of Variance - One-Way ANOVA from the main menu.

Box-and-Whisker Plot



9	5	2.6	6.3	09/24/98
10	5	2.4	12	11/26/98
11	5	3	8.5	01/29/99
12	5	4.5	10	03/03/99
13	6	3.1	22	04/20/99
14	7	2.8	18	05/01/99
15	8	2	4.4	06/26/99
16	8	2.6	10.2	08/22/99
17	9	3.6	19	09/21/99
18	10	4	16.4	10/30/99
19	11	3.3	33.3	11/15/99
20	12	2.9	17.4	12/25/99

Mag/Box... Mag/Loc St... Mag/Dist St... Mag/Proba... Mag/Proba...

QuakeDem... StatAdvisor StatGallery StatReporter Mag/Loc Date/Loc

Ready

Novell-delivered Application...

STATGRAPHICS Plus...

NUM... 11:14AM





Mag/Box&amp;Whisk



Lbt

Row

## Analysis Summary

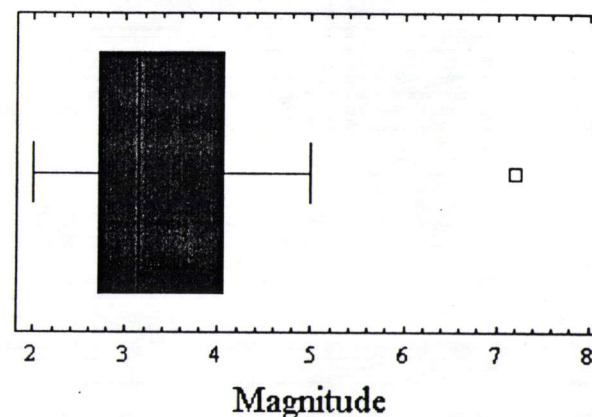
Data variable: Magnitude

20 values ranging from 2.0 to 7.2

## The StatAdvisor

This procedure displays a box-and-whisker plot of a single column of data. You can create many other graphs and statistics for the data by selecting Describe - Numeric Data - One-Variable Analysis from the main menu.

Box-and-Whisker Plot



9	5	2.0	0.5	09/24/90
10	5	2.4	12	11/26/98
11	5	3	8.5	01/29/99
12	5	4.5	10	03/03/99
13	6	3.1	22	04/20/99
14	7	2.8	18	05/01/99
15	8	2	4.4	06/26/99
16	8	2.6	10.2	08/22/99
17	9	3.6	19	09/21/99
18	10	4	16.4	10/30/99
19	11	3.3	33.3	11/15/99
20	12	2.9	17.4	12/25/99

MultBox&amp;Whi...

Mag/Loc Si...

Mag/Dist Si...

Mag/Proba...

Mag/Proba...

QuakeDem...

StatAdvisor

StatGallery

StatReporter

Mag/Loc

Date/Loc

16880

Start

Novell-delivered Applicatio...

STATGRAPHICS Plus...

NUM 11:14 AM





## Mag/Loc Simple Regression



Lbf

Row

Regression Analysis - Linear model:  $Y = a + b \cdot X$ 

Dependent variable: Magnitude

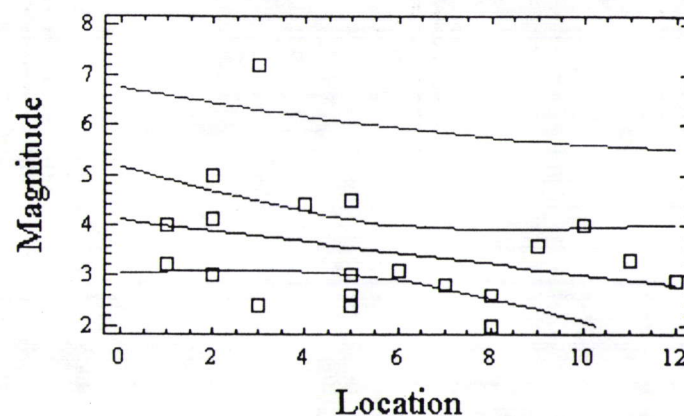
Independent variable: Location

Parameter	Estimate	Standard Error	T Statistic	P-Value
Intercept	4.09991	0.502762	8.15477	0.0000
Slope	-0.109157	0.0791481	-1.37915	0.1847

## Analysis of Variance

Source	Sum of Squares	Df	Mean Square	F-Ratio
--------	----------------	----	-------------	---------

Plot of Fitted Model



9	2.6	6.3	09/24/98
10	2.4	12	11/26/98
11	3	8.5	01/29/99
12	4.5	10	03/03/99
13	3.1	22	04/20/99
14	2.8	18	05/01/99
15	2	4.4	06/26/99
16	2.6	10.2	08/22/99
17	3.6	19	09/21/99
18	4	16.4	10/30/99
19	3.3	33.3	11/15/99
20	2.9	17.4	12/25/99



Dependent variable: Magnitude  
Independent variable: Distance

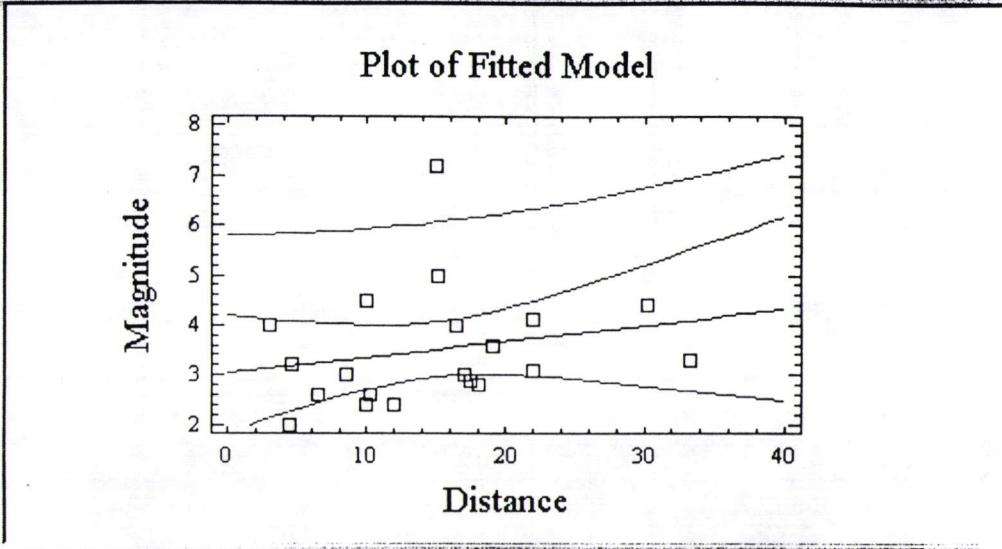
Parameter	Estimate	Standard Error	T Statistic	P-Value
Intercept	3.03386	0.55798	5.43723	0.0000
Slope	0.0319848	0.0333402	0.959345	0.3501

Analysis of Variance

Source	Sum of Squares	Df	Mean Square	F-Ratio
--------	----------------	----	-------------	---------

1				
---	--	--	--	--

9	5	2.6	8.3	09/24/98
10	5	2.4	12	11/26/98
11	5	3	8.5	01/29/99
12	5	4.5	10	03/03/99
13	6	3.1	22	04/20/99
14	7	2.8	18	05/01/99
15	8	2	4.4	06/26/99
16	8	2.6	10.2	08/22/99
17	9	3.6	19	09/21/99
18	10	4	16.4	10/30/99
19	11	3.3	33.3	11/15/99
20	12	2.9	17.4	12/25/99







## Mag/Probability Plots



## Probability Plots

Data variable: Magnitude

Number of observations: 20

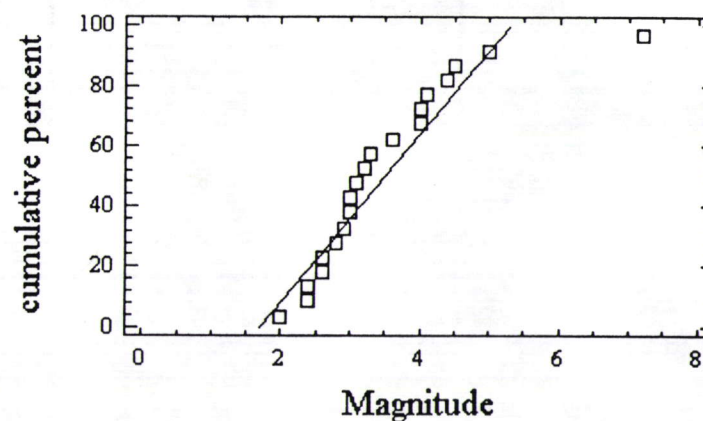
Number of values below minimum: 0

Number of values above maximum: 0

## The StatAdvisor

This procedure creates seven different types of probability plots to help you determine whether Magnitude comes from a particular type of distribution. After examining these plots, you may fit a distribution to the data by selecting the Distribution Fitting procedure.

Uniform Probability Plot



5	5	2.0	0.5	09/24/98
10	5	2.4	12	11/26/98
11	5	3	8.5	01/29/99
12	5	4.5	10	03/03/99
13	6	3.1	22	04/20/99
14	7	2.8	18	05/01/99
15	8	2	4.4	06/26/99
16	8	2.6	10.2	08/22/99
17	9	3.6	19	09/21/99
18	10	4	16.4	10/30/99
19	11	3.3	33.3	11/15/99
20	12	2.9	17.4	12/25/99



Ready

Start

Novell-delivered Applicatio...

STATGRAPHICS Plus...

NUM1 11:15 AM





## Mag/Probability Plot



Lbt

Row

## Analysis Summary

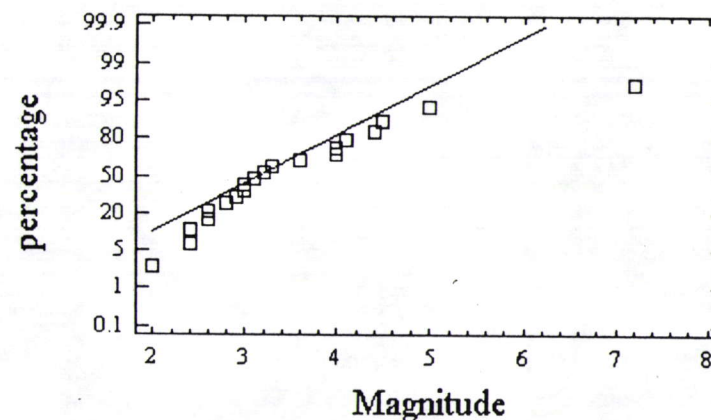
Data variable: Magnitude

20 values ranging from 2.0 to 7.2

## The StatAdvisor

This procedure displays a normal probability plot of a single column of data. You can create many other graphs and statistics for the data by selecting Describe - Numeric Data - One-Variable Analysis from the main menu.

Normal Probability Plot for Magnitude



14	7	2.8	18	05/01/99
15	8	2	4.4	06/26/99
16	8	2.6	10.2	08/22/99
17	9	3.6	19	09/21/99
18	10	4	16.4	10/30/99
19	11	3.3	33.3	11/15/99
20	12	2.9	17.4	12/25/99